Planning Commission



Minutes for the Wednesday, August 17, 2022, Regular Meeting

Members of the Planning Commission

Dr. Christine Crawford

Chair

Bob Bigger Jesse Elliott Leonard Carter, Jr.

Rett Harbeson

Timothy V. Key, Vice Chair

JoAnn McKie

CITIZEN ASSISTANCE: Individuals requiring special assistance or a sign interpreter to participate in the meeting are asked to please notify the Department of Planning and Development 48 hours prior to the meeting at 803-441-4221.

- 1. <u>Call to Order</u> 7:00 p.m.
- 2. <u>Roll Call</u> Members present were Chairman Dr. Christine Crawford, Commissioners JoAnn McKie, Rett Harbeson, Bob Bigger, and Len Carter.
- **3.** Approval of Minutes July 20, 2022 Regular Meeting were approved with the correction of the name of commissioners present.
- 4. Confirmation of Agenda There were no changes to the agenda.
- 5. <u>Application RZM22-003 West Five Notch Apartments</u> Rezoning A request by Glynn Bruker to rezone approximately 0.52 acres located along West Five Notch Road, TPN 005-19-06-006 from PD, Planned Development to R-5, Mixed Residential to develop 5 apartment units.

Mr. Paradise stated this is a request of rezoning of the .52 acres which was an old carwash. This development will have 5 units. It backs up to R-5 zoning which is already

approved for a development plan and it will share existing 28' driveway. This will take it from Planned development to R-5 zoning.

Mr. Bo Slater with James Swift & Associates is present representing Mr. Bruker. This will have 5 units and will share the existing driveway with the development that is already approved.

- a. Public Hearing No comments from the public.
- **b.** Consideration of the Rezoning request by the Planning Commission Mr. Harbeson made first motion and Mr. Bigger seconded it. Approved unanimously.
- Recommendation to City Council
 Unanimously approved to go to City Council.
- **6.** Application RWN22-002 Compassion Way Street Naming A request by the City of North Augusta to give the name Compassion Way to a portion of right of way currently referred to as the Frontage Road adjacent to I-20 at Exit 1 and West Martintown Road.

Mr. Paradises stated this come up due to E911. There are lot of frontage roads already in Aiken County. The area is beginning to be developed so we need to change this road name so that River Falls Apartments can start getting their addresses. So after contacting a business on that road but got no response the road name fell back on the staff at the city. The mayor came up with the name Compassion Way due to having the pain management center on this road.

- a. Public Hearing No comments from the public.
- **b.** Consideration of the Street Naming request by the Planning Commission Mr. Carter made the first motion and Mr. Bigger made the second motion. It was approved unanimously.
- 7. Application PP22-003 Wrenfield at Chanticleer Major Subdivision Preliminary Plat A request by Merit Commercial Holdings for approval of 127 single-family detached homes located on approximately 66.67 ac zoned R-10, Medium Lot, Single-Family Residential. The property is located at the end of Big Pine Road, TPN 002-12-01-002.

Mr. Paradise stated the Mr. Harbeson has recused himself because he works for the firm working on this project.

Mr. Paradise state back in October of 2021 Planning Commission reviewed a concept plan for this subdivision but it was called Big Tree Subdivision. There were a few comments then by Planning Commission. The development went forward but it changed the name to Wrenfield at Chanticleer and it is directly behind Chanticleer and will be accessed thru that neighborhood. It is 66.9 acres zoned R-10 and will have 127 single family detached homes with a density of .52 dwelling units per acre. They are

requesting a waiver for the block length increase from 650 to 1000 ft. The traffic study has been done. Apportion has been annexed of Chanticleer subdivision on March 18, 1991 and at that time property was zoned R-2 which is equivalent to the current R-10.

Ms. Alexander Reynolds with Cranston Engineering came forward to speak about this development. She stated that the sketch plan presented in 2021 is similar to this one. This would be first conservation subdivision in North Augusta and they would make sure they hit all the perimeters. Mr. Bigger is concerned about the entrance being only one. Mrs. McKie discussed the traffic on Martintown Rd. and how we need some red lights. Mr. Paradise stated he had some things that staff are recommending such as the road names. The approval includes certification of the us of the road names Whooping Crane Cove, Warbler Court, Wilton Place, and Wrenfield Way. Also any outstanding comments will be addressed to the satisfaction of City Staff. There are still some outstanding comments related to landscaping, parking, elevations and others.

Mr. Bigger and Mr. Carter are concerned about the traffic and entrance to the development.

Dan Holloway is speaking on the development. It is zoned for R-10 which allows 50ft lots. He discussed that a traffic study was done and that bot everyone is going to come and go at the same time. They also talked to the county at lengths about this property and traffic. Michael Bradham representing JLA who is working on the plan for this property. The plan is very dense. He went to another subdivision with over 300 residents with just one entrance and it does work for them.

- **a.** Consideration of the Major Subdivision Preliminary Plat application by the Planning Commission
 - Mr. Carter made the first motion for the wavier and conditions and Mrs. McKie made the second motion. But the vote was 2 opposed & 2 approved. Due to the conflict of votes they looked at Roberts Rules of Order and the procedures of how to handle this type of situation. Mr. Carter made the motion to reconsider the previous motion and Mrs. McKie made the second motion which was approved unanimously. Mr. Bigger then made a motion to table the item until the next meeting and that was seconded by Mr. Carter and approved unanimously.
- 8. <u>Application SP22-001 Hamrick Farms Multifamily</u> Major Site Plan A request by Panther Residential Management, LLC for approval of a 340-unit apartment complex located in the Hamrick Farms Planned Development, a portion of TPN 005-17-01-012, approximately 25.3 ac.

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Mr. Paradise stated this if for a major site plan improvement. It is part of Hamrick Farms which is Development 754 acres at exit 1 at Martintown Rd. The City authorized a traffic study in this area. The area is zoned mixed use. This is appropriate use for this development. The plans show 681 parking spaces and some using garages to account for those. They did get a variance for the height of the buildings. They are using the wetlands for buffers on undeveloped land. Stormwater must approve all sediment erosion control. The approval of road names of Repose Loop, Patriarch Place, Founders Lane and Envisioner Path for internal roads for the development. There is proposed connection at Exit 1 at the red light and Knobcone Ave. That is one of the things the traffic consultant is working on because all the traffic was coming out on Exit 1. The roads should be sufficient for the apartment complex and other developments coming later.

Sean Smith with Cranston Engineering group. To answer some of your questions they are having ongoing conversations and meetings about the Martintown Corridor. The main road for Hamrick Farms is directly off the off ramp. The two main roads going in the development they are trying to approve and construction all of this at the same time.

These are 340 proposed units. They also have two entrances being constructed. The 3 developers are splitting the cost of roads for the projects.

a. Consideration of the Major Site Plan application by the Planning Commission Mr. Bigger made the first motion to approve with condition to have connectivity to both Knobcone and Martintown Rd. and approval of road names. Mr. Carter seconded the motion. It was approved unanimously.

9. Staff Report

a. July Performance Report

Mr. Paradise stated still working on the development code. The next phase is to get printed and let everyone look it over and get feedback. The kickoff meeting for the Georgia Ave. traffic calming study took place this week.

10. Adjourn Meeting is adjourned at 8:40pm.

Respectfully yours,

The Pa

Tommy Paradise

Director of Planning and Development

Department of Planning and Development



Project Staff Report

Major Subdivision (Preliminary Plat) PP22-003 Wrenfield at Chanticleer

Prepared by: Kuleigh Baker

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SECTION 1: PROJECT SUMMARY

Project Name	Wrenfield at Chanticleer	
Applicant	Merit Commercial Holdings	
Engineer	JLA	
Address/Location	Termini of Southwood Drive, Big Pine Road, and	
	Greenwood Drive	
Parcel Number	002-12-01-002	
Total Project Acreage	± 66.9 acres	
Zoning	R-10, Medium Lot, Single-Family Residential	
Development Pattern	Conservation Subdivision	
Traffic Impact Tier	Tier 2	
Proposed Use	127 Single-family detached homes	
Density	.52 du/ac	
Future Land Use	Residential Single Family	

SECTION 2: PLANNING COMMISSION CONSIDERATION

The North Augusta Development Code (NADC) § 5.8.3 specifies the procedures for Planning Commission approval of major subdivisions (preliminary plats) that exceed the minor plat threshold requirements of §5.8.3.1.

NADC 5.8.3.1 Applicability

An application is considered a major subdivision (preliminary plat) if:

- a. The application does not meet the tests for a minor subdivision as set forth in §5.8.2.1;
- b. The application is for property located in a PD District;
- c. The application would otherwise require minor subdivision approval, but a waiver is requested pursuant to §5.9; or

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- d. The application proposes development in two (2) or more phases. In addition, the code states:
 - **5.8.3.4.4** At the conclusion of the staff review stage, the Department shall report its findings to the Planning Commission as to:
 - a. Type of subdivision proposed, physical characteristics of the land, relation of the proposed development to surrounding areas and existing and probable future development;
 - b. Relation to major roads, utilities and other facilities and services;
 - c. Any proposed agreements, contracts, deed restrictions, sureties, dedications, contributions, guarantees, or other instruments, or the need for such instruments, or for amendments in those proposed; and
 - d. Compliance of the subdivision application with the provisions of this Chapter, the suitability of plans proposed, and the desirability of conditions on the approval, waivers, or amendments, if any.
 - **5.8.3.4.5** Based on such findings, the report to the Planning Commission on the application shall include a recommendation for approval or denial and any recommended waivers, conditions of approval or modifications to the major subdivision application as submitted, if any, with reasons therefore.
 - **5.8.3.4.6** A majority vote is required for the Planning Commission to approve, approve with conditions, if applicable, or deny a major subdivision application. The decision of the Planning Commission provides the final approval of the application.
- **5.8.3.5** Scope of Major Subdivision Approval Preliminary approval of a major subdivision development application shall confer upon the applicant the following rights:
 - a. The approval of the major subdivision application constitutes approval of the subdivision or land development as to its character, intensity of development, general layout, and the approximate dimensions of streets, lots, and other planned features. Such approval binds the developer to the general scheme of the subdivision or land development and permits the developer to proceed with the installation of site improvements, subject to obtaining other necessary permits.
 - b. The approval of the major subdivision application does not constitute approval of a final subdivision plat, and accordingly, does not authorize the sale of lots or the occupancy or use of a parcel of land.
 - c. The applicant may request final approval for the whole, or a section, or sections of the major subdivision application upon completion of the subdivision and approval of the development by the city and state agencies with jurisdiction.
 - d. A major subdivision application, a site specific development plan for the purposes of this section, approval or conditional approval shall expire two (2) years from said approval unless

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a grading permit has been issued and construction has commenced. The applicant may apply for and the Planning Commission may grant extensions on such preliminary approval for additional periods up to one (1) year each but not to exceed five (5) extensions. If an amendment to this Chapter is adopted by the City Council subsequent to the major subdivision development approval that would preclude the initial approval, a request for an extension may not be granted. (Rev. 12-1-08; Ord. 2008-18) (Rev. 8-16-10; Ord. 2010-12)

Planning Commission Action:

Per §5.8.3.4.6, a majority vote is required for the Planning Commission to approve, approve with conditions, if applicable, or deny a major subdivision application.

SECTION 3: PUBLIC NOTICE

A notice of the major subdivision application and scheduled date of the Planning Commission meeting was posted on www.northaugustasc.gov on September 15, 2022.

SECTION 4: SITE HISTORY

A portion of the subject property adjacent to the existing Chanticleer subdivision was annexed on March 18, 1991 by Ordinance No. 91-05. At that time, the property was zoned R-2, Single-Family Residential in conformance with the City's Land Use and Development Plan. The equivalent R-10, Medium Lot, Single-Family Residential zoning district was adopted with the Official Zoning Map of the 2008 North Augusta Development Code.

On October 21, 2021, the Planning Commission reviewed a Concept Plan for the proposed subdivision.

On August 17, 2022 the Planning Commission reviewed the Major Subdivision (Preliminary Plat) for the proposed subdivision. Additional information was requested which will be presented by the applicant to the board.

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SECTION 5: EXISTING SITE CONDITIONS

	Existing Land Use	Future Land Use	Zoning	
Subject	Vacant	Residential Single Family	R-10, Medium Lot, Single-Family	
Parcel			Residential	
North	Residential	Residential Single Family	Outside City Limits/R-10,	
			Medium Lot, Single-Family	
			Residential	
South	Residential	Residential Single Family	R-14, Large Lot, Single-Family	
			Residential	
East	Residential	Residential Single Family	R-10, Medium Lot, Single-Family	
			Residential/ R-14, Large Lot,	
			Single-Family Residential	
West	Vacant/Residential	Residential Single Family	Outside City Limits	

<u>Access</u> – The site currently has access to West Martintown Road from Shawnee Drive, Southwood Drive, Big Pine Road, and Greenwood Drive.

<u>Topography</u> – The subject site has variable topography with multiple streams on site.

<u>Utilities</u> – Water and wastewater connections would have to be brought in from neighboring developments.

<u>Floodplain and Environmental Conditions</u> – A small portion of the site is located in Flood Zone X and AE with a 0.2% annual chance of flood hazard. Site located on FEMA FIRM panel 45003C0313F.

<u>Drainage Basin</u> – The proposed development is located in the Pretty Run/Rapids Basin. Pretty Run basin is located in a highly dense residential part of North Augusta. The preliminary physical stream assessments at two reaches of the stream indicate that this stream channel is currently not effective at transporting current loads of stormwater during heavy storm events. A main sewer line runs along and in the stream channel and some of its tributaries. Overtopping of banks is obvious in several locations and manholes present in those locations may overflow if surcharging occurs. High nutrient concentrations have been detected in two samples during the period. The results indicate that urban runoff is impacting the stream channel. Many homes back up to the creek along its way through the city. The high density residential area contains well-maintained lawns in many instances. In addition, animals are

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penned at or near the creek along most of its reach. The city will continue to reach out to residents in the area to provide information that may help reduce pollutant loads.

SECTION 6: STAFF EVALUATION AND ANALYSIS

Section §5.8.3.4.4 asks that the Department shall report its findings to the Planning Commission as to:

a. Type of subdivision proposed, physical characteristics of the land, relation of the proposed development to surrounding areas and existing and probable future development;

The applicant is proposing construction of 127 single-family detached homes in a one access subdivision. Single-family detached homes are permitted in the R-10, Medium Lot, Single-Family Residential Zoning District. The proposed development is situated at the rear of the existing Chanticleer subdivision and the proposed development is comparable to the surrounding neighborhoods.

b. Relation to major roads, utilities and other facilities and services;

The proposed utility and infrastructure improvements have been reviewed by the Director of Engineering and Public Works. There are outstanding comments that must be addressed prior to final Staff approval.

West Martintown Road is maintained by SCDOT and will require encroachment and driveway permits issued by SCDOT for any improvements required by the TIA.

The applicant must receive approval for a Stormwater Management Permit and satisfactorily address review comments and modify plans in response to any outstanding Stormwater, Engineering, and Planning comments.

The applicant has proposed the road names Whooping Crane Cove, Warbler Court, Wilton Place, and Wrenfield Way. The names have been reserved by Aiken County E911 Addressing for one year. Final approval of the proposed road names is subject to Planning Commission approval of this application. Road suffixes are subject to the final road layout. The entrance road will remain Big Pine Road.

Per NADC Section 2.3.7, the connectivity ratio does not apply to local streets within a Conservation Subdivision. The applicant is requesting a waiver to the maximum block length.

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c. Any proposed agreements, contracts, deed restrictions, sureties, dedications, contributions, guarantees, or other instruments, or the need for such instruments, or for amendments in those proposed; and;

As part of the Final Plat process required for the issuance of individual building permits and Certificates of Occupancy for residential lots, the developer shall submit a Deed of Dedication, Maintenance Guarantee and required guarantees for the acceptance of infrastructure. If needed, the Planning Department will also require a Performance Guarantee with a Letter of Credit for sidewalks and street trees and any other incomplete infrastructure to allow the applicant to construct homes prior to completion of all site improvements. Riparian buffer areas platted on individual lots are to be deed restricted.

d. Compliance of the subdivision application with the provisions of this Chapter, the suitability of plans proposed, and the desirability of conditions on the approval, waivers, or amendments, if any.

Waiver Request

The applicant has requested a waiver from Table 14-2, Maximum Block Length for a Local Street. The request is to increase the maximum block length from 650 ft to 1000 ft in two locations:

- 1. From the intersection of Road 1 and Road 1A to the terminus of Road 1
- 2. From the intersection of Road 2 and Road 2A to the terminus of Road 2.

The request is pursuant to NADC Section 14.19.2 which states "the permissible length of a cul-de-sac or close may be increased to a maximum of 1000 ft where the Planning Commission finds that natural features, including topography, environmental constraints, or other natural conditions, or parcel dimensions or configuration preclude a connecting street".

Per §5.9.1 Planning Commission Waivers, the Planning Commission may waive such standards where:

 After obtaining the recommendation of the Director, the Planning Commission determines that the proposed waiver does not conflict with the goals and policies of the Comprehensive Plan or the purposes underlying the standard; and

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The applicant state the waiver does not conflict with the goals and policies of the Comprehensive Plan or the purpose of the standard and that roads were laid out to utilize the existing stream crossing location, minimize grading, and avoid development in steep slopes and sensitive areas. Connection of Road 1 and Road 2 would require additional stream crossings. Shawnee Drive cannot be connected to the site due to topography issues.

Staff notes that Section 6.2.3 of the 2021 Comprehensive Plan states that the use of cul-de-sacs and dead-end streets should be minimized except in cases where sites are physically restrained by natural resources such as bodies of water, elevation changes, or to conserve other natural areas.

2) The applicant demonstrates, through documentation and/or studies, based on generally accepted engineering principles, that adherence to the standard provided by this Chapter would pose a threat to health and safety or would undermine a policy set forth in the Comprehensive Plan or the purposes underlying the standard; and

The applicant states that the street design is necessitated by the topography, grading, and storm detention requirements. Adherence to the 650 ft block length would result in an increase of conservation area and unusable land for development.

- 3) The applicant consents to an alternative standard, and the Planning Commission finds that such standard is consistent with the Comprehensive Plan, will protect the public health, safety and general welfare, and is consistent with the purposes underlying the standard; and
 - The applicant requests the Planning Commission evoke NADC Section 14.19.12 to allow the maximum block length for cul-de-sacs due to topographic challenges.
- 4) The economic burden imposed on the applicant to comply with the generally applicable standard outweighs the public purpose for such standard; and

The applicant states that any alternative would not result in a cohesive design of the site. Staff notes that the economic burden is not the primary purpose of this application through strict adherence to the standard reduces the amount of land that may be profitably developed.

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5) Compliance with the generally applicable standard is impracticable due to unique topographical or other site conditions.

The applicant states that the topography and streams on the site restrict the street layout. The proposed layout considers the topography while avoiding unnecessary impacts to surrounding properties.

SECTION 7: STAFF RECOMMENDATION

Based on the analysis and evaluation of each review criteria outlined above, the Department has determined the application is complete.

A recommendation by the Planning Commission for the approval of the major subdivision preliminary plat for Wrenfield at Chanticleer is appropriate subject to the following waiver and conditions:

Waiver

1) A waiver is granted to allow for cul-de-sacs that exceed the maximum of 650 ft allowed by Table 14-2. A maximum cul-de-sac length of 1000 ft is granted for Road 1 and Road 2.

Conditions

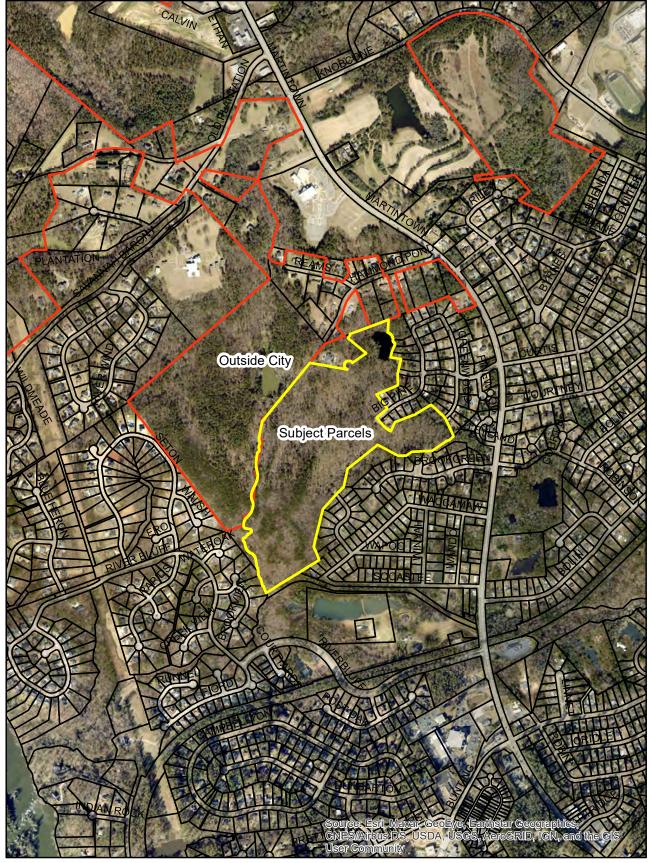
- 1) This approval includes certification of the use of the road names Whooping Crane Cove, Warbler Court, Wilton Place, and Wrenfield Way.
- 2) Any outstanding comments will be addressed to the satisfaction of City staff.

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SECTION 8: ATTACHMENTS

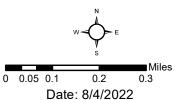
- 1. Site/Aerial Map
- 2. Topography Map
- 3. Current Zoning Map
- 4. Future Land Use Map
- 5. Application Documents and Waiver Request
- 6. Site Plan
- 7. Traffic Impact Analysis
- 8. ANX91-05
- 9. Critical Areas Study Ph II Assessment No. 47
- 10. FEMA FIRM panel 45003C0313F
- 11. Signage Plan
- 12. Shawnee Extension Profile
- 13. Signal Warrant Assessment
- 14. CONPL21-002 Staff Report
- 15. Minutes of the October 21, 2021 Regular Planning Commission Meeting
- cc. JLA, via email

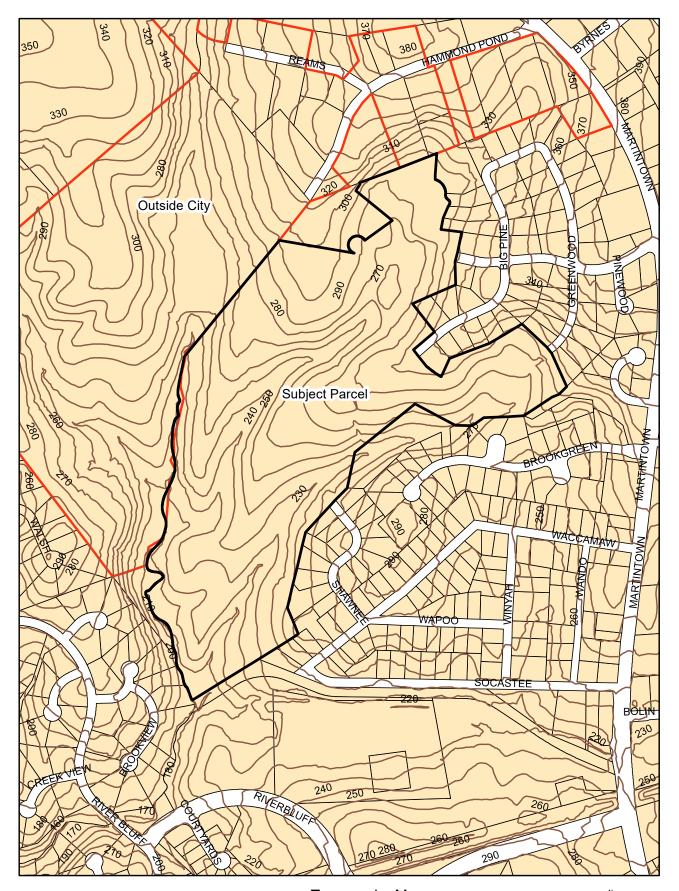
Merit Commercial Holdings, via email





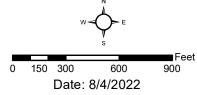
Aerial Map
PP22-003 Wrenfield at Chanticleer
Approx. 66.7 ac
zoned R-10, Medium Lot,
Single-Family Residential

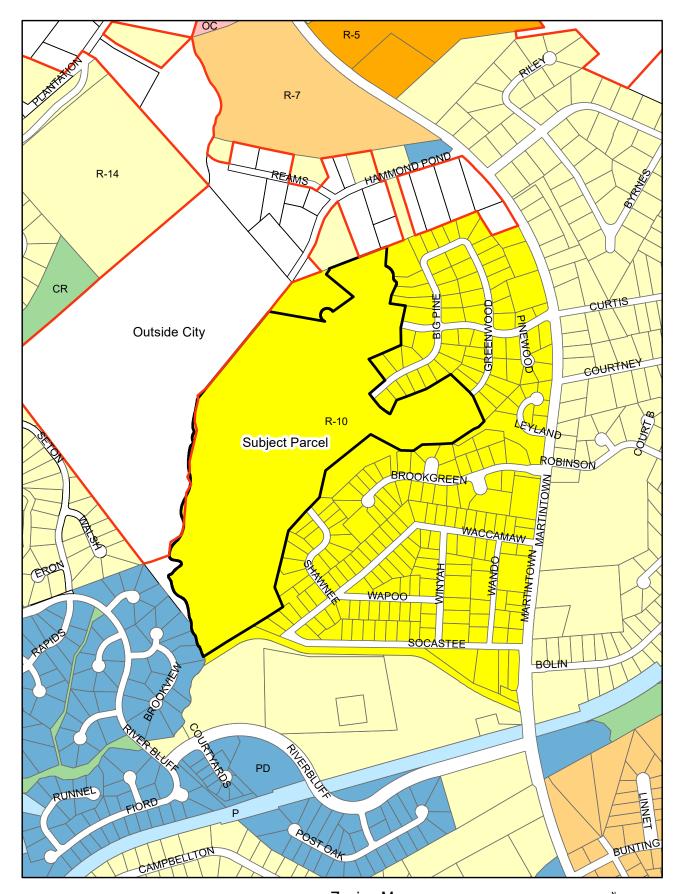






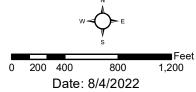
Topography Map
PP22-003 Wrenfield at Chanticleer
Approx. 66.7 ac
zoned R-10, Medium Lot,
Single-Family Residential

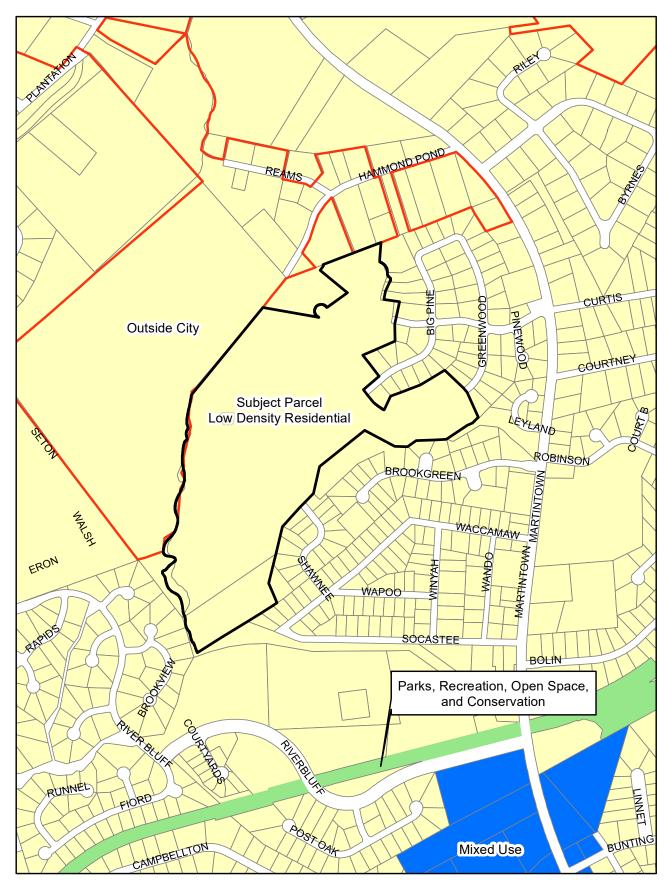






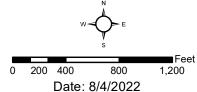
Zoning Map
PP22-003 Wrenfield at Chanticleer
Approx. 66.7 ac
zoned R-10, Medium Lot,
Single-Family Residential



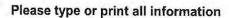




Future Land Use Map
PP22-003 Wrenfield at Chanticleer
Approx. 66.7 ac
Low Density Residential



Application for Development Approval





	Staff Use
Application Number	Date Received
Review Fee	Date Paid
. Project Name WRENFIELD AT CHAN	TICLEER (FORMERLY CALLED BIG PINE)
Project Address/Location BIG PINE	ROAD (PARCEL BOUNDARY IS WHERE BIG PINE RD. EN
Total Project Acreage 66.67 ACRES	Current Zoning R-10
Tax Parcel Number(s) 002-12-01-0	202
	JER Applicant Phone <u>706-83/-8/57</u>
Mailing Address P.O. Box 1	lele 7
City EVALS ST CA	Zip 30809 Email KHEFNER@ MERIT FLOOR.COM
. Is there a Designated Agent for this proj If Yes, attach a notarized Designation of	ect? Yes No Agent form. (required if Applicant is not property owner)
Engineer/Architect/Surveyor WILLTA	M BUCHANAN License No. 28610
Firm Name JOHNSON LASCHOBER+	SSOCIATES Firm Phone 706-724-5756
Firm Mailing Address 1296 8 ROAD 3	
	Zip 30901 Email WBOCHANANCTHE JLA GROUP.
	when Date 6/13/2022
Is there any recorded restricted covenant of prohibits the use or activity on the property (Check one.)	or other private agreement that is contrary to, conflicts with or that is the subject of the application? yes no
In accordance with Section 5.1.2.3 of the	North Augusta Development Code, I hereby request the City oject plans. The documents required by the City of North
Augusta, as outlined in Appendix B of the	North Augusta Development Code, are attached for the City's
complete to initiate the compliance review	cknowledges that all required documents must be correct and process.
Carl Hefen	6 13 7622
Applicant or Designated Agent Signatur	
Kevin R. Hefner	
Print Applicant or Agent Name	

Designation of Agent





This form is required if the property owner is not the applicant.

Staff Use Only					
Ap	pplication Number Date Received				
1.	Project Name WRENFZELD AT CHANTZCLEER (FORMERLY CALLED 814 PZNE)				
	Project Address/Location BIG PINE ROAD (PARCEL BOUNDARY IS WHERE BIG PINE RO. END				
	Project Parcel Number(s) 002-12-01-002				
2.	Property Owner Name MARZA S. DZTTY Owner Phone 706-829-5553				
	Mailing Address 804 BIG PINE ROAD City NORTH AUGUSTA ST SC Zip 2984! Email DOOWAN 2 @ CONCAST. NET				
3.	Designated Agent KEUZN HEFNER				
	Relationship to Owner Managing Partner of development group				
	Relationship to Owner Managing Partner of development group Firm Name Merit Commercial Holdings Phone 706-831-8157				
	Agent's Mailing Address P.U Box 1667				
	City Coans I ST GA ZIP 30809 Email KHEFNER@MERZTFLOOR.COM				
	Agent's Signature for Child Date 6/15/22				
4.	I hereby designate the above-named person (Line 3) to serve as my agent and represent me in the referenced application. 6/14/22				
	Owner Signature Date				
5.	Sworn and subscribed to before me on this day of				
	Notary Public NOTARY NOTARY				
	Notary Public 05 · 24 · 2026 Commission Expiration Date EXPIRES GEORGIA MAY 24, 2026 MAN DIAGONATION MAY 24, 2026 MAY 24				
	MBIA COUNTRIES				

Wrenfield at Chanticleer- Waiver Request Letter

Waiver Request

NADC Table 14-2 lists the maximum block length of a local street as 650'.

NADC Sec 14.19.2 states: The permissible length of a cul-de-sac or close may be increased to a maximum of 1,000' where the Planning Commission finds that natural features, including topography, environmental constraints, or other natural conditions, or parcel dimensions or configuration preclude a connecting street design.

A waiver is requested to evoke Sec. 14.19.2 and increase the maximum block length from 650' to 1,000 in two locations:

- 1. From the intersection of Road 1 and Road 1A to the terminus of Road 1
- 2. From the intersection of Road 2 and Road 2A to the terminus of Road 2

Waiver Request Justification

- 5.9.1.1 After obtaining the recommendation of the Director, the Planning Commission determines that the proposed waiver does not conflict with the goals and policies of the Comprehensive Plan or the purposes underlying the standard; and
- Response to 5.9.1.1: The proposed waiver does not conflict with the goals and policies of the Comprehensive Plan or the purposes underlying the standard. Roads were laid out to utilize the existing stream crossing location, minimize grading and avoid steep slopes and sensitive areas. This resulted in Road 1 and Road 2 ending in cul-de-sacs. These two streets cannot be connected together because it would necessitate another stream crossing. The existing Shawnee Drive cannot be connected to the proposed extension of Big Pine Road (Road 1) because of the significant steep topography at the end of Shawnee Drive.
- 5.9.1.2 The applicant demonstrates, through documentation and/or studies, based on generally accepted engineering principles, that adherence to the standard provided by this Chapter would pose a threat to health and safety or would undermine a policy set forth in the Comprehensive Plan or the purposes underlying the standard; and
- Response to 5.9.1.2: Strict adherence to the 650' block length instead of being granted the 1,000' block length for the cul-de-sac would result in increased conservation area. This may sound like a good thing but the site is already 49.75% open space, 9.75% more than is required to qualify for a conservation subdivision. This number will unnecessarily increase if the block length waiver is not granted.

- 5.9.1.3 The applicant consents to an alternative standard, and the Planning Commission finds that such standard is consistent with the Comprehensive Plan, will protect the public health, safety and general welfare, and is consistent with the purposes underlying the standard; and
- Response to 5.9.1.3: Consenting to an alternate standard is not necessary since evoking the permission of the Planning Commission per Sec. 14.19.12 is sought.
- 5.9.1.4 The economic burden imposed on the applicant to comply with the generally applicable standard outweighs the public purpose for such standard; and
- Response to 5.9.1.4: If the roads cannot be extended from 650 'to 1,000' development of an additional 1,400' (350' x 2 roads x 2 sides of each road) of frontage will not be possible and the property cannot be profitably developed.
- 5.9.1.5 Compliance with the generally applicable standard is impracticable due to unique topographical or other site conditions.

Response to 5.9.1.5: Same response as to 5.9.1.1. Roads were laid out to utilize the existing stream crossing location, minimize grading and avoid steep slopes and sensitive areas. This resulted in Road 1 and Road 2 ending in cul-de-sacs. These two streets cannot be connected together because it would necessitate another stream crossing. The existing Shawnee Drive cannot be connected to the proposed extension of Big Pine Road (Road 1) because of the significant steep topography at the end of Shawnee Drive.

Supporting Justification Enclosures

Included photographs:

- o Picture 1_Existing Stream Crossing
- o Picture 2_Existing Stream Crossing
- o Picture 3_Slopes near Shawnee Drive

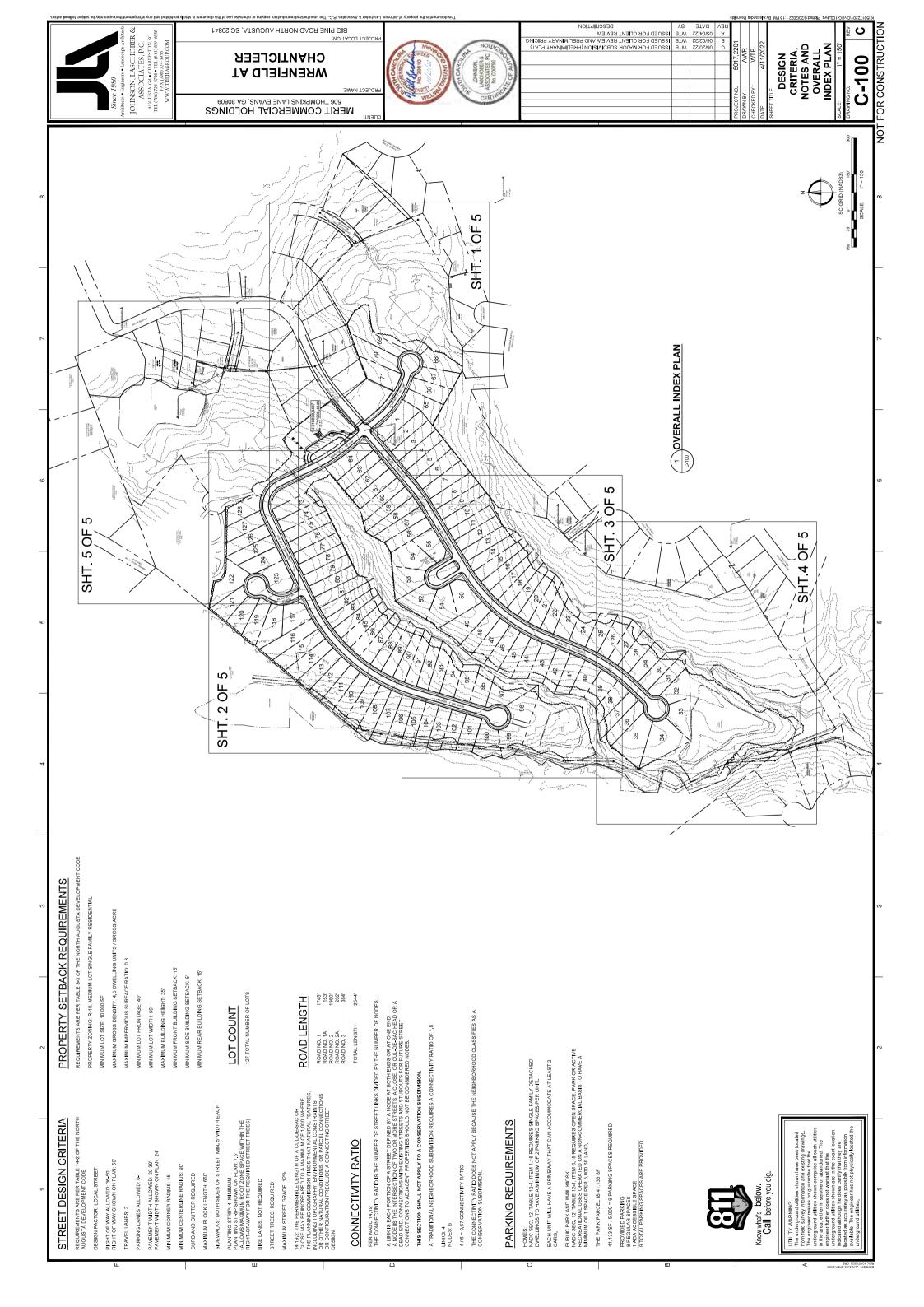
Included plans:

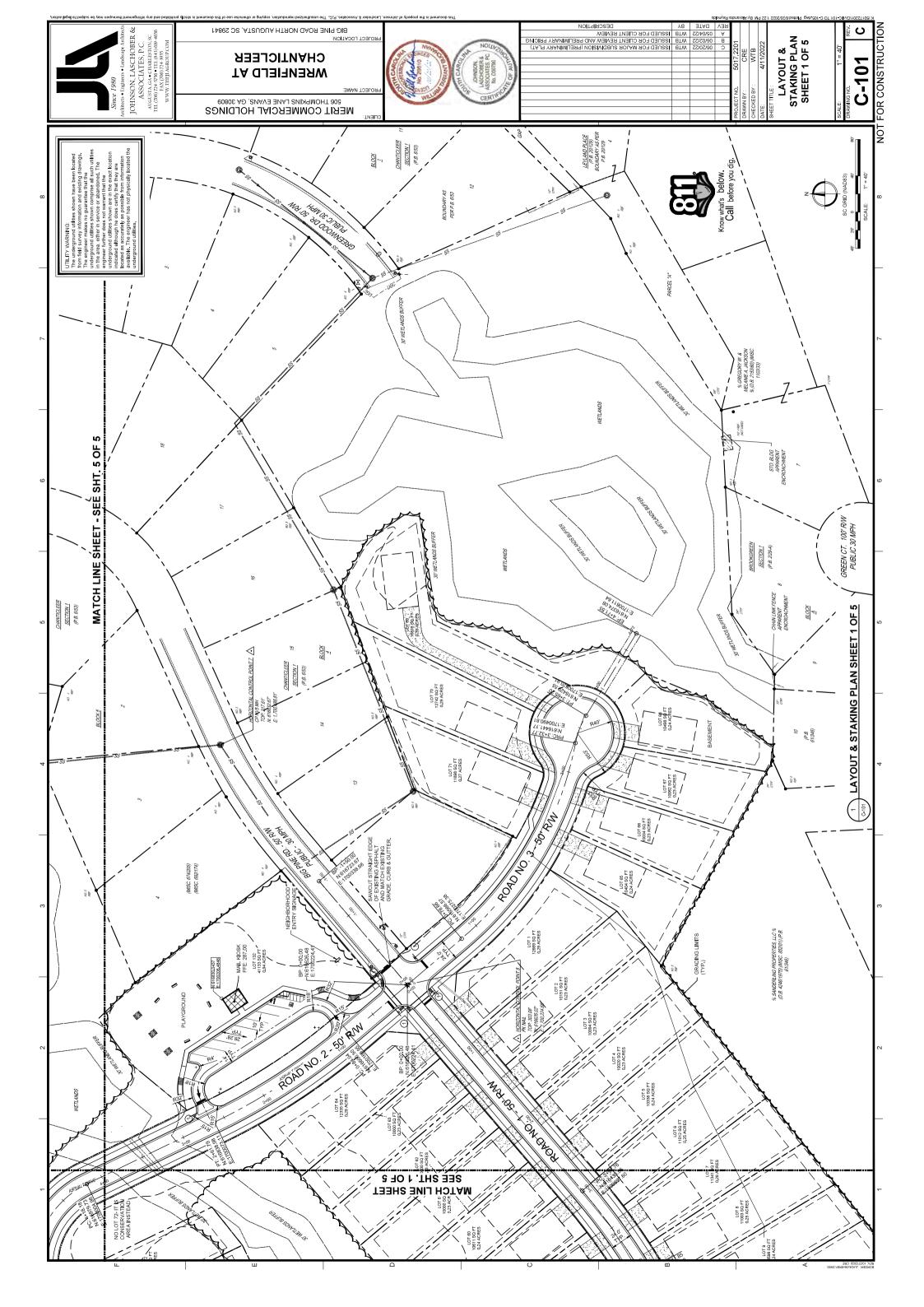
- o C-100_RC shows the layout of the roads
- o C-101_RC to C-105_RC show the road layout and site topography
- C-106_RC shows the amount of open space provided

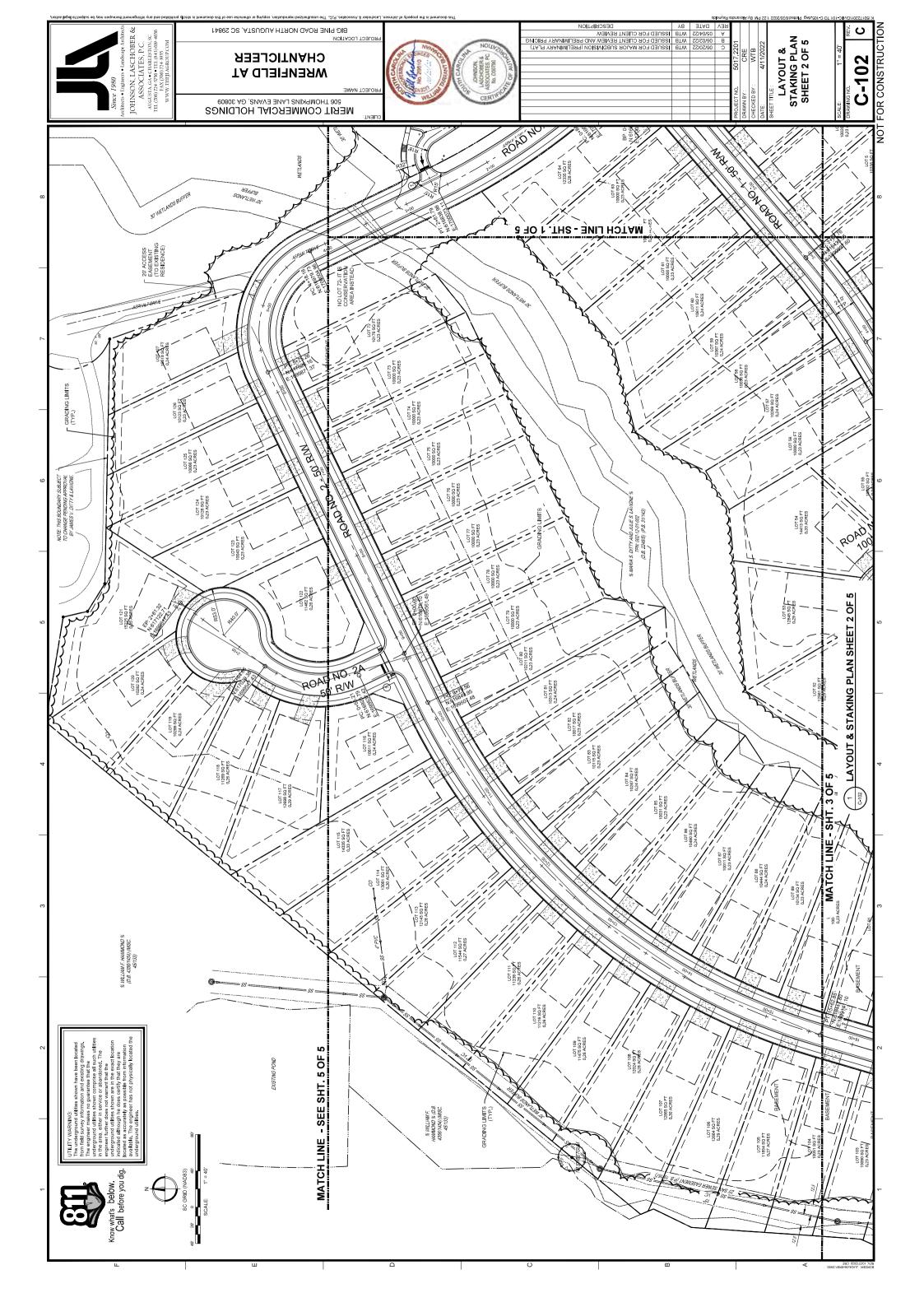


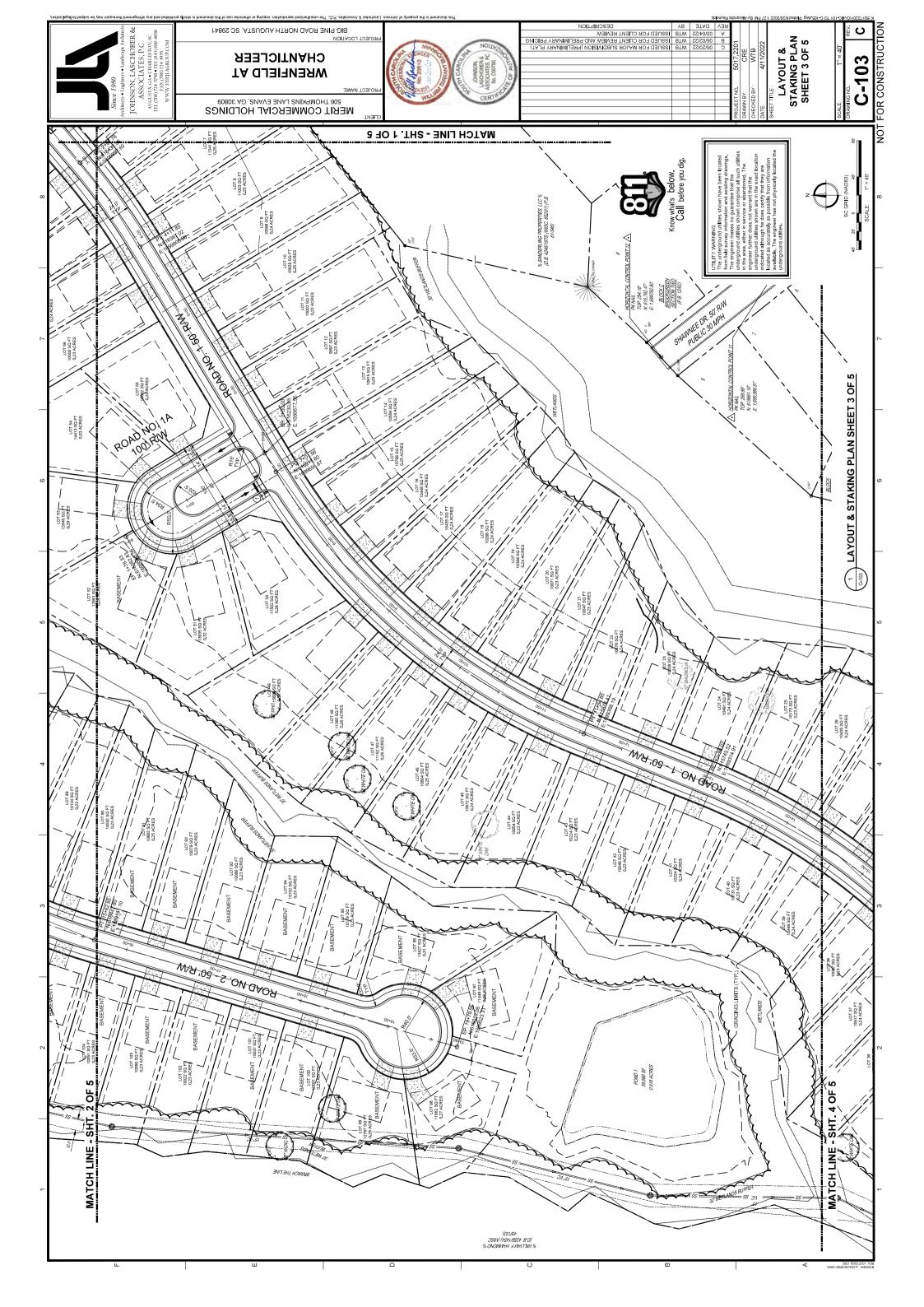


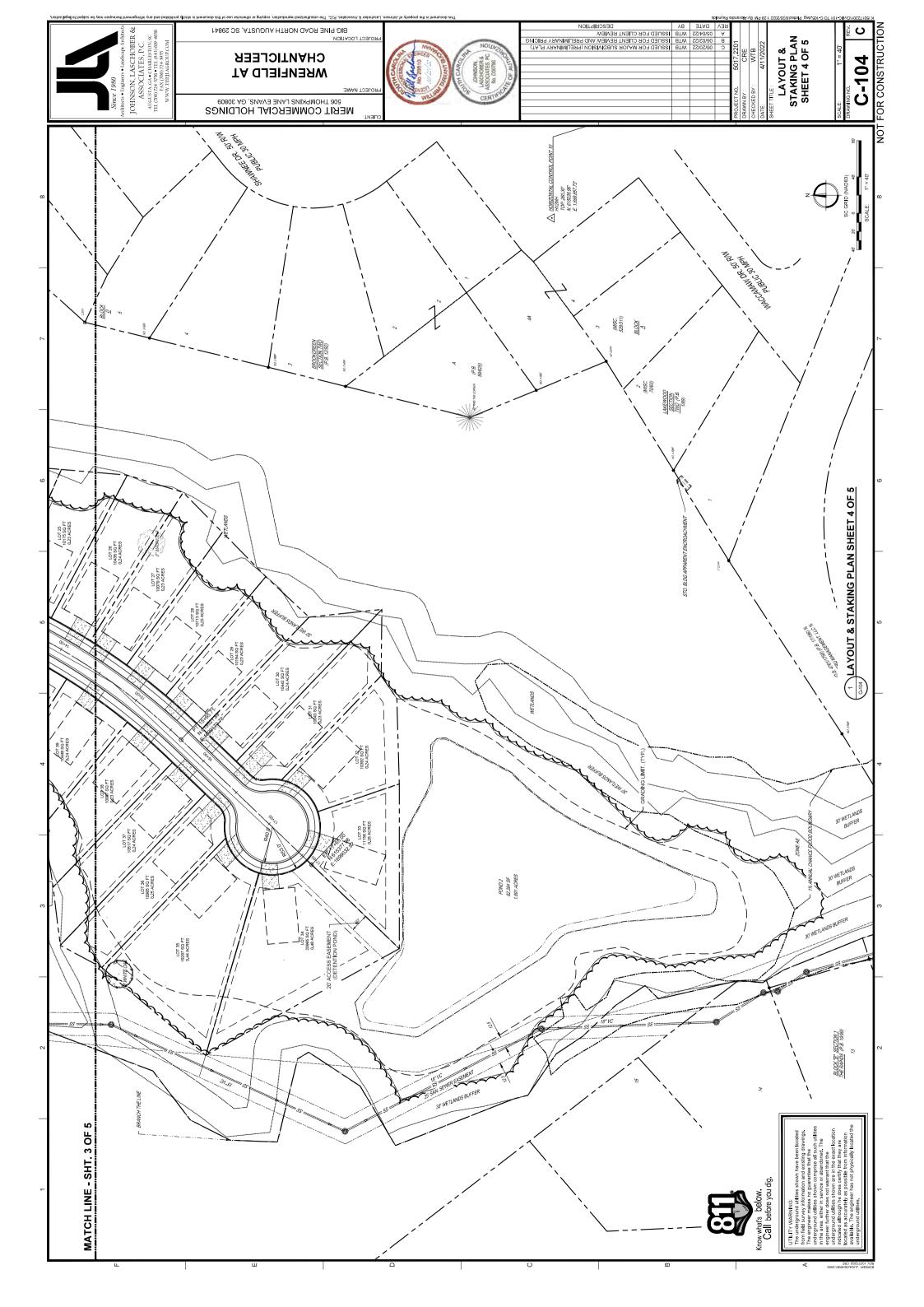


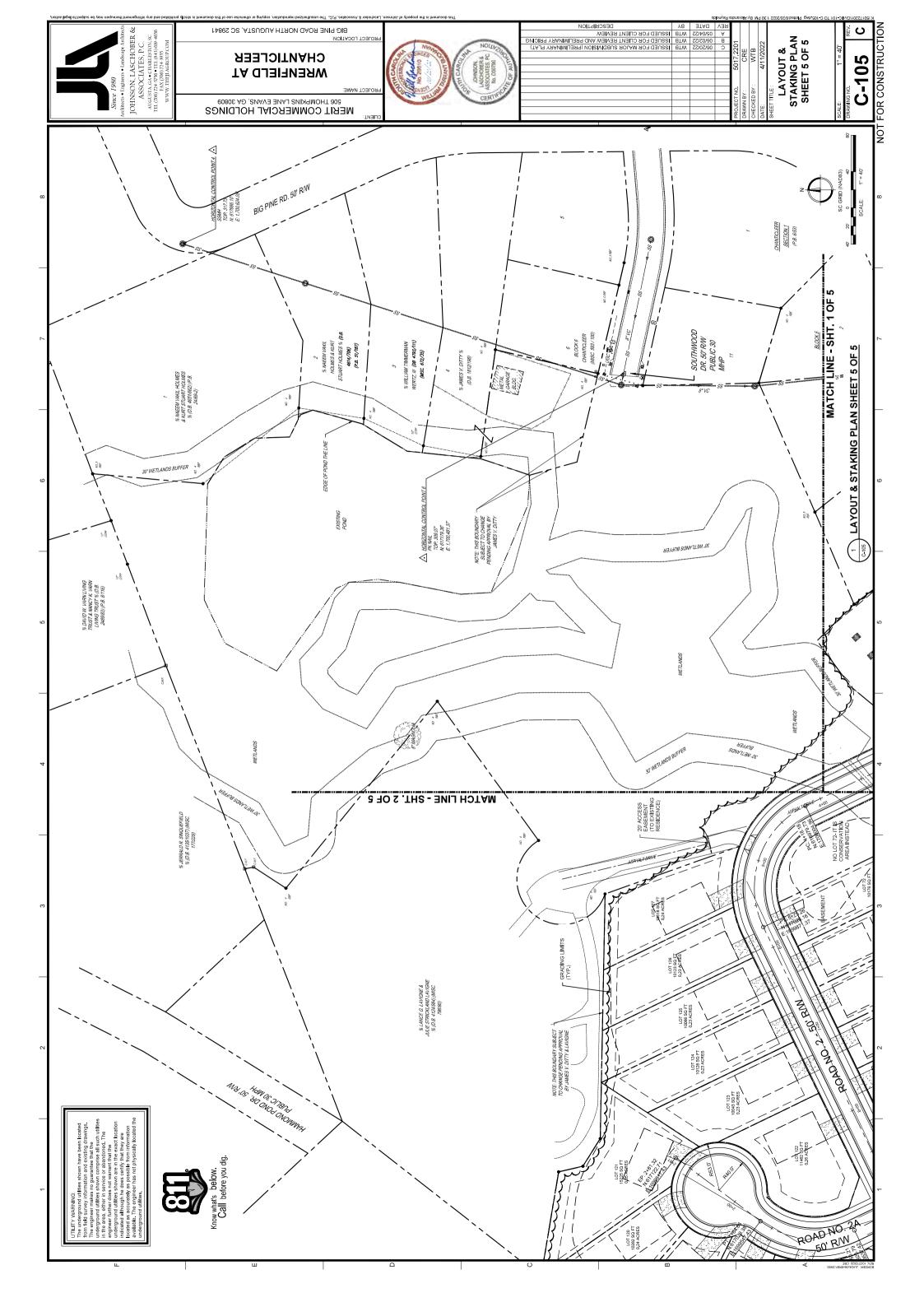


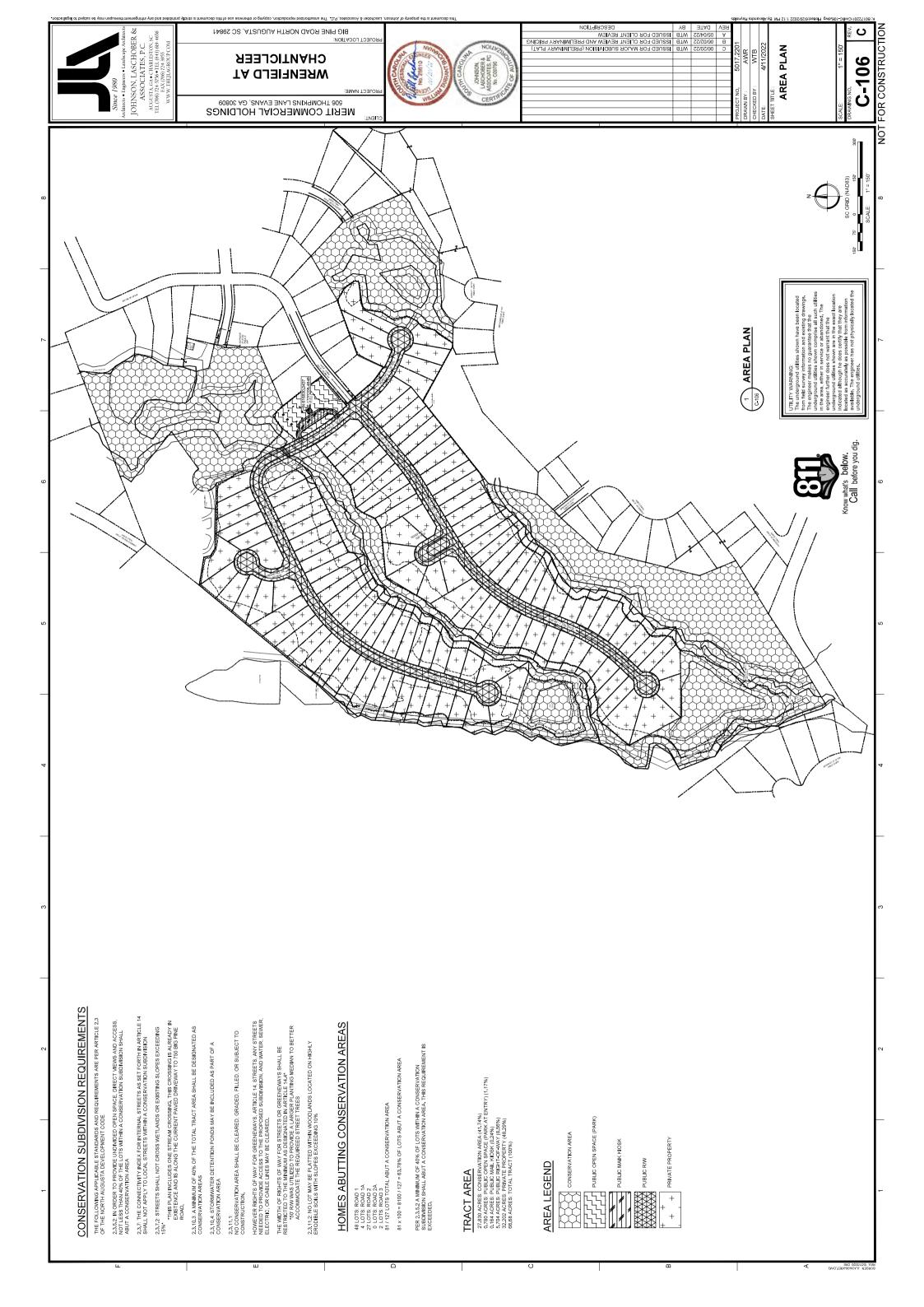












Site Analysis and Protection Recommendations Per NADC Sec. 6.1.1

Site Location:

The site is located at the dead end of Big Pine Road in North Augusta's Chanticleer neighborhood.

Geology and Soils:



According to the above Aiken County GIS soils map there are three types of soils present on the property: Hiawassee (pink), Troup (green), and Vaucluse (blue). USDA Soil classifications are as follows: Hiawassee soils are well drained with medium to rapid surface run off and moderate permeability. Troup soils are very deep somewhat excessively drained and have moderate to rapid permeability. Vaucluse soils are well drained with high to very high surface runoff and moderate to slow permeability.

Topography:

Slopes on the site range from 0-24%. The steepest slopes have been avoided as much as is practical in accordance with Sec. 6.1.3.2.

Wetland and Water Features:

Two wetlands and three streams are present on the site. A 30' buffer is shown surrounding each wetland and on each side of each stream. No land disturbance will occur within this

buffer. The FEMA firmette maps (below) show a floodplain at the south of the property. There are no homes planned to be near the flood plain. The only development near the floodplain is the 1.891 acre detention pond which is located outside of the limits of the floodplain.

You can choose a new flood map or move the location pin by selecting a different location on the locator map below or by entering a new location in the search field above. It may take a minute or more during peak hours to generate a dynamic FIRMette. If you are a

AFIREN (County)

Ominor promises boston based on over input and found from the first of the firs

Existing Vegetation:

OTHER AREAS CONSTELL CONSTELL FRENCH SYSTEM AVE

The site is wooded with a mix of pine and hardwoods.

Structures:

No existing structures are present on the property. Planned structures are 127 single family homes around $2{,}100$ sf $(35' \times 60')$ each.

Visual and View Features:

The neighborhood will be a conservation subdivision. 81 of the 127 the properties (63.78%) abut a conservation area and have direct views and access. All residents have access to the public park near the entrance that abuts a conservation area and has direct views into it.

Other Environmental Characteristics:

There are none known.

Road Networks:

Existing Roads- the property currently has an existing driveway from the end of existing Big Pine Road to parcel 002-12-01-032. This driveway crosses one of the streams. The location of this stream crossing is planned to be improved and used as the crossing location for the proposed Road 2.

Proposed Roads- Roads were laid out to minimize grading and avoid steep slopes and sensitive areas. This resulted in Road 1 and Road 2 ending in cul-de-sacs. These two streets cannot be connected together because it would necessitate another stream crossing. The existing Shawnee Drive cannot be connected to the proposed extension of Big Pine Road (Road 1) because of the significant steep topography at the end of Shawnee Drive. Road names will be coordinated with North Augusta and the owner as the project progresses.

Past, Present, and Proposed Uses of the Site:

Past- Undeveloped woodland

Present- Undeveloped woodland

Future- Conservation Subdivision with 27.830 acres (41.74%) of undisturbed conservation area, 0.780 acres of public park, and 38.08 acres developed area

WRENFIELD AT CHANTICLEER NEIGHBORHOOD NORTH AUGUSTA, SOUTH CAROLINA

TRAFFIC ENGINEERING STUDY

Prepared for:

JOHNSON, LASCHOBER, AND ASSOCIATES

Prepared by:



SPECIALIZED CONSULTING SERVICES

1557 BROAD STREET AUGUSTA, GA 30904 (706) 836-5160 WWW.ISMLLC-ENGR.COM

JUNE 17, 2022 No.

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Appendices



INTRODUCTION

This report analyzes the traffic impact of the proposed Wrenfield at Chanticleer neighborhood (WCN) which will include 123 single-family homes to be located on a 66.9-acre tract located at the existing "stub-out" of Big Pine Road in the existing Chanticleer neighborhood in North Augusta, South Carolina. Full Build-out is expected by 2026.

The location of the proposed development is shown in Figure 1.

Access for the additional homes will be provided via Southwood Road, which is the existing main access fort the Chanticleer neighborhood at Martintown Road.

The impact of WCN to traffic operations of the surrounding roadway network was determined in accordance with "Appendix B – Application Documents" of the North Augusta Development Code (NADC) and as well as the South Carolina Department of Transportation's Access and Roadside Management Standards (ARMS) and includes existing, future no-build, and future build traffic conditions at the following intersections:

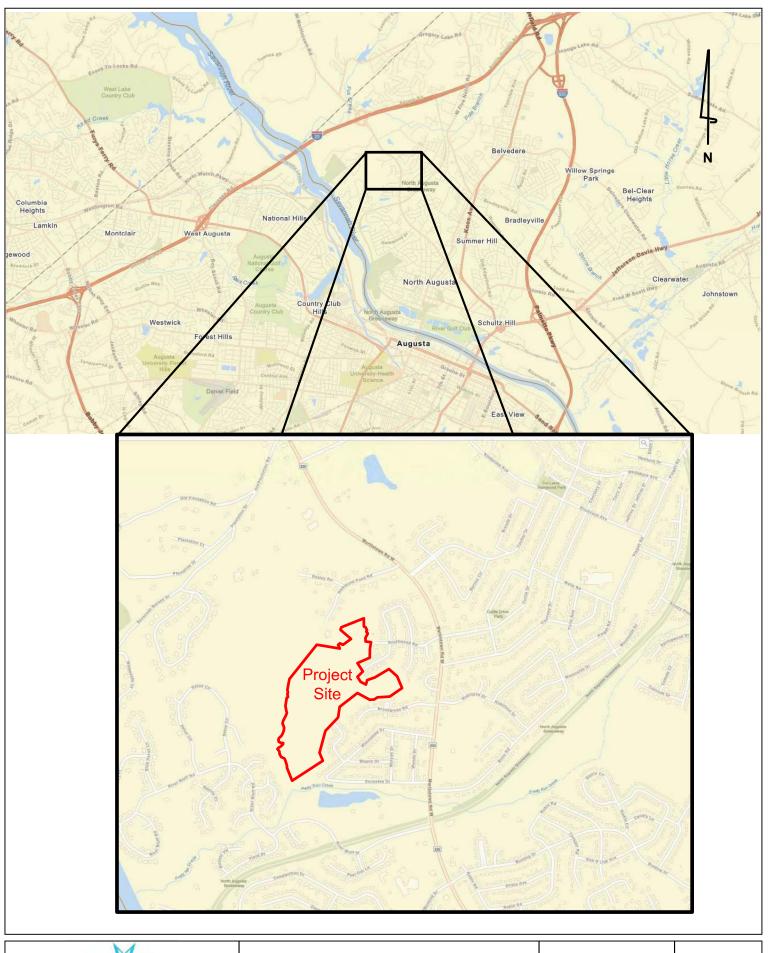
- Martintown Road (SC-230) at Southwood Road/Curtis Drive and
- Martintown road (SC-230) at Courtney Drive

Each intersection was analyzed for the existing, future no-build, and future build traffic conditions to determine any mitigation necessary to alleviate existing or projected deficiencies. Additionally, each driveway will be analyzed to provide recommendations for driveway configuration and traffic control to provide safe, efficient ingress and egress to the site.

In addition to traffic from RCL, both the future no-build and future build conditions will account for traffic from several approved developments in the area.

The methodology to assess operations and the study findings are summarized in the sections that follow.







Wrenfield at Chanticleer Traffic Impact Analysis

Site Location Map

Figure 1

Page 2

CAPACITY ANALYSIS METHODOLOGY

Synchro 11 software were used to perform capacity analysis at each intersection within the study network in accordance with criteria set forth in the Transportation Research Board's <u>Highway Capacity Manual</u>, 2010 Edition (HCM).

In general, the LOS may be defined as a measure of operations conditions within a traffic stream and the perception of the condition by the general motoring public. The six levels of service are briefly described, as follows:

- LOS A Little or no traffic delays;
- LOS B Minimal to short traffic delays;
- LOS C Average traffic delays;
- LOS D Relatively long traffic delays;
- LOS E Intersections are at or near the maximum capacity and traffic experiences long delays; and
- LOS F Intersections are operating above their maximum capacity and traffic delays are long and unstable.

For signalized intersections, one overall intersection LOS is reported. At unsignalized intersections, the LOS for each controlled approach or movement (side-streets and main-street left-turns) is reported. Table 1 presents LOS criteria for signalized and unsignalized intersections.

Table 1 Level of Service Criteria												
Average Control Delay (sec / veh)												
LOS	Signalized Intersections	Unsignalized Intersections										
A	≤ 10	≤10										
В	> 10 and ≤20	> 10 and ≤ 15										
С	> 20 and ≤35	> 15 and ≤ 25										
D	> 35 and ≤55	> 25 and ≤ 35										
Е	> 55 and ≤80	> 35 and ≤ 50										
F	> 80	> 50										

Source: 2000 Highway Capacity Manual

For signalized intersections, a volume-to-capacity ratio (v/c) is also computed. The capacity of the intersection is calculated based on the geometry and signal green-time allocation. Intersection capacity is then compared to the volumes entering the intersection. A v/c ratio of less than 1.0 indicates that there is sufficient capacity for the traffic demand. A v/c ratio of more than 1.0 generally indicates the need for intersection improvements.



EXISTING ROADWAY FACILITIES

A site visit was performed to develop an inventory and observations of the existing roadways within the study network, which are described in the sections that follow.

Martintown Road (SC-230)

In the vicinity of the site, Martintown Road is designated SC-230 and is essentially a north-south, state-maintained with a functional classification as an Urban Arterial and a posted speed limit of 40 miles-per-hour (mph). Land uses along Martintown Road are a mix of commercial, residential, industrial, and institutional.

At it's both unsignalized intersections with Southwood Road/Curtis Drive and Courtney Drive, Martintown Road is uncontrolled with an exclusive left-turn lane, one through lane, and one shared through/right-turn lane both its northbound and southbound approaches.

In 2021, SCDOT reported an annual average daily traffic volume (AADT) of 18,300 vehicles per day (vpd) along Martintown Road, just north of the site. A 24-hour bi-directional count performed for this study showed a 24-hour volume of 16,488vpd between Southwood Road and Courtney Drive.

Southwood Road/Curtis Road (S-537)

Southwood Road is a two-lane, east-west local road with a 30-mph speed limit. Southwood Road serves as the main entrance and only access for the Chanticleer subdivision and only serves residential land uses.

Curtis Drive is a two-lane, east-west state-maintained secondary road classified as an urban local road with a 25-mph speed limit. Curtis Drive serves as one of the main entrance for the Smithfield subdivision with connectivity via Pinehurst subdivision to West Five Notch Road.

At it's unsignalized intersection with Martintown Road, Southwood Road and Curtis Drive are both stop-controlled with a single exiting lane and a single entrance lane.

SCDOT does not maintain a count station along Southwood Road, but a 24-hour, bi-directional count performed along Southwood Rod for this study showed a 24-hour volume of 782 vpd.

In 2021, SCDOT recorded an AADT along Curtis Drive, east of Martintown Road of 650 vpd.



Courtney Drive (S-506)

Courtney Drive is a two-lane, east-west state-maintained secondary road classified as an urban local road with a 25-mph speed limit. Courtney Drive serves as one of the main entrances for the Smithfield subdivision with connectivity via Pinehurst subdivision to West Five Notch Road.

At it's unsignalized intersection with Martintown Road, Courtney Drive is stop-controlled with a single exiting lane and a single entrance lane.

In 2021, SCDOT recorded an AADT along Curtis Drive, east of Martintown Road of 800 vpd.



EXISTING CONDITIONS

Existing Traffic Volumes

Peak hour turning movement counts were collected at both intersections in the study network on Tuesday, March 8, 2022. From these data, the peak hour volumes for the intersections were found to occur between 7:15 am and 8:15 am for the morning peak hour and between 4:45 pm and 5:45 pm for the evening peak hour.

Existing morning and peak hour volumes as well as lane configurations are shown in Figure 2.

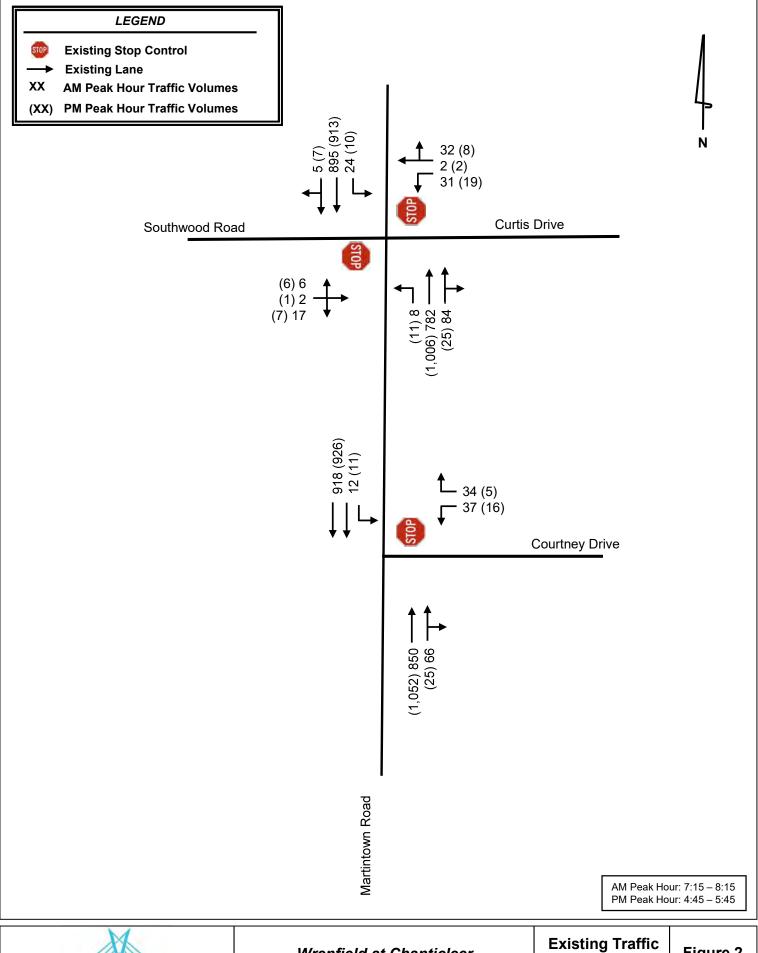
Existing Operations

Existing intersection operations were analyzed to determine current traffic conditions and identify existing deficiencies that should be addressed. Peak hour intersection traffic volumes and existing intersection geometries were used in the analysis and the results are presented in Table 2.

Table 2 Existing Intersection Operations														
A.M. Peak Hour P.M. Peak Hour														
Intersection LOS Delay (s) LOS Delay (s)														
Martintown Rd at Southwood Rd/Curtis Dr	Α	1.5	Α	0.9										
- eastbound approach	С	18.2	С	21.6										
 westbound approach 	С	23.6	D	30.9										
- northbound left-turn	В	10.3	В	10.7										
- southbound left-turn	В	10.2	В	10.9										
Martintown Rd at Courtney Dr	Α	0.8	Α	0.4										
- westbound approach	C	19.8	D	30.4										
- southbound left-turn	В	10.3	В	13.1										

As shown by the results in Table 2, while overall operations for each intersection is within the LOS Standard in the Existing Condition, delay along the westbound side street approaches are operating at LOS D during the evening peak hour at both intersections. This is due to the relatively heavy volume of traffic along Martintown Road that is limiting gaps for the side street exiting movements which is not uncommon or outside of driver expectations in an urban area accessing an arterial roadway during peak hours.







Wrenfield at Chanticleer Traffic Impact Analysis Existing Traffic Volumes

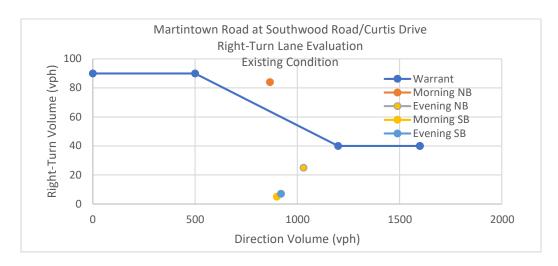
Figure 2

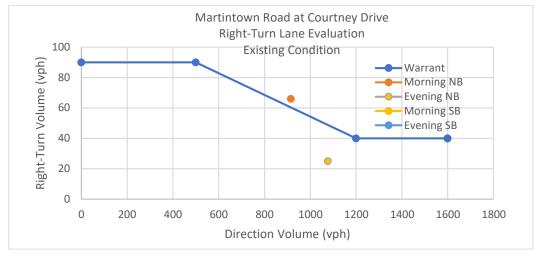
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Existing Condition Auxiliary Lane Analyses

The need for auxiliary lanes at the intersections of Martintown Road at Southwood Road/Curtis Drive and Martintown Road at Courtney Drive in the Existing Condition was evaluated in accordance with section 9.5 Auxiliary Turn Lanes of the SC DOT Roadway Design Manual (February 2021) which provides volume guidelines and criteria for the installation of right-turn and left-turn lanes at unsignalized intersections. As noted previously, the geometry of this intersection currently includes a left-turn lane in each direction, therefore, warrant analyses were only performed for right-turn lanes.

The right-turn lane analysis relies on the peak hour right turn volume versus the total peak hour traffic volume in the same direction and this analysis is shown below:







As shown by the above evaluations, a right-turn lane is currently warranted for the northbound approach at both intersections. Because this improvement is necessary to address existing deficiencies, it is considered a "system" improvement. "System" improvements are those required to mitigate existing deficiencies not associated with traffic generated by the proposed development not typically considered to be the whole responsibility of the developer.

Analysis was performed for the Existing Condition with the warranted right-turn lane is presented in Table 3.

Table 3 Existing Intersection Operations with System Improvements														
A.M. Peak Hour P.M. Peak Hour														
Intersection LOS Delay (s) LOS Delay (s)														
Martintown Rd at Southwood Rd/Curtis Dr	Α	1.5	Α	0.9										
 eastbound approach 	C	18.1	С	21.6										
 westbound approach 	C	22.3	D	30.4										
- northbound left-turn	В	10.3	В	10.7										
- southbound left-turn	В	10.2	В	10.9										
Martintown Rd at Courtney Dr	Α	0.8	Α	0.4										
- westbound approach	C	19.0	D	29.7										
- southbound left-turn	В	10.3	В	13.1										

As shown by the above analyses, the addition of a northbound right-turn lane at both intersections does not result in a significant improvement of overall operation of either intersection. Therefore, careful consideration should be given to adding these lanes to determine if the benefit justifies this level of investment.



BACKGROUND GROWTH

Background growth estimates include were performed using a combination of historic traffic volumes and census data for the area. This methodology is shown in the paragraphs that follow.

South Carolina DOT maintains several count stations in the vicinity of the site with data available between 2015 and 2020. The 2020 daily traffic volumes and calculated growth rates are presented in Table 4 for the count stations closest to the site.

			Table 4											
	Traffic Growth in the Study Area													
Route Location 2021 10-year 5-year 2-year														
		AADT	Average Annual	Average Annual	Average Annual									
			Growth	Growth	Growth									
SC 230	South of site	22,600	0.88%	2.37%	-0.66%									
SC 230	North of site	18,300	1.87%	2.98%	-0.54%									
SC 230	North of I-20	13,300	2.10%	3.13%	-0.37%									
S- 1905	NE of site	2,400	-1.11%	-3.04%	-19.46%									
S- 537	East of site	650	0.00%	-4.07%	-3.64%									
S- 506	East of Site	800	0.96%	2.71%	0.00%									
	Overall Average		1.37%	2.38%	1.64%									

As shown by the data in Table 4, traffic growth in the immediate vicinity of the site has been fairly aggressive over the past 10-years. More data shows signs leveling off or decline, but this is a function of the CoVid-19 pandemic's impact as opposed to a slowing in development in the area

In addition to traffic growth, estimated census data from the South Carolina Revenue and Fiscal Affairs Office were obtained for both Edgefield and Aiken County and reviewed. These data, as well as calculated average annual growth rates, are shown in Table 5.

Table 5 Population Projection Trends for Edgefield and Aiken County													
Year Population Projections % Change Average Annua													
	Edgefield County	Aiken County	Total		Growth								
2020	27,150	171,320	198,470										
2025	27,370	175,635	203,005	2.3%	0.5%								
2030	27,475	178,735	206,210	3.9%	0.4%								
2035	27,425	180,550	207,975	4.8%	0.3%								

Similar to traffic trends shown previously, the annual growth in population for the county is also projected to stabilize over the long term as well, with annual growth falling below 1% in the next twenty years.



Finally, a review of the <u>West Martintown Road Corridor Study</u> done by AECOM and adopted by North Augusta City Council in 2021 was performed and revealed that a 2.0% annual growth rate was utilized in the study.

Therefore, taking all of the above factors into consideration, a 2.0% annual growth factor was utilized to estimate background conditions.

Background Development Traffic

Review of background developments included in the West Martintown Road Corridor Study was performed along with recently-approved developments in the area to determine if any approved developments were of close enough proximity to the WCN development that their impact would be greater than what was either captured in the traffic counts or captured within the 2.0% annual growth rate and completed by 2026.

Based on this review, two developments were identified and included:

- River Falls Apartments 220 Apartments proposed approximately one mile to the north between Frontage Road and Plantation Drive.
- Hamrick Farms Planned Development Mixed-Use including single-family, multi-family, and large commercial uses.

For the purposes of this study, it was assumed that the River Falls Apartments would be completed and that Hamrick Farms Phase I would be 50% complete by 2026.

Volumes from these developments were obtained from the <u>West Martintown Road Corridor Study</u> and added to the background growth.



2026 No-Build Condition

WCN is expected to be completed in 2026, therefore, an estimate was made for the 2026 No-Build Condition which represents the traffic operations of the study network in 2026 without traffic from the proposed development.

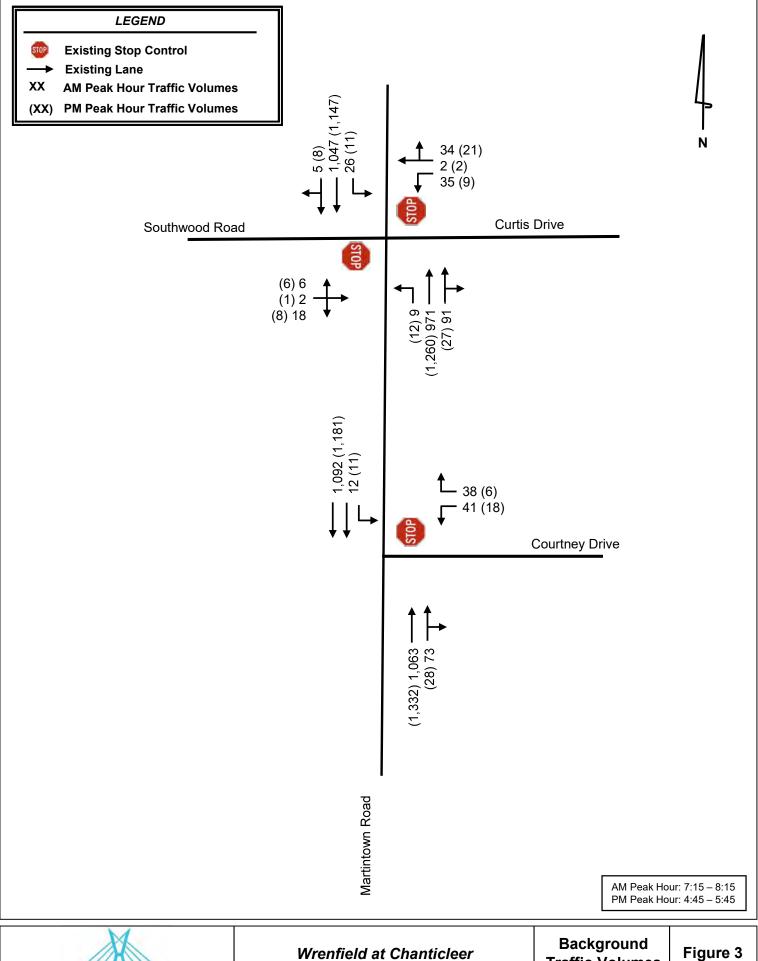
To project traffic volumes for the 2026 No-Build Condition, the background growth rate, which was calculated previously at 2.0%, was applied to the adjusted existing traffic volumes for five years. Projected traffic volumes from the proposed River Falls Apartments and Hamrick Farms developments were then added to this growth to establish the 2026 No-Build Traffic Volumes which are shown in Figure 3.

These volumes were used to analyze the 2026 No-Build traffic conditions surrounding the site with existing intersection geometry. The results of this analysis are presented in Table 6.

Table 6 2026 No-Build Intersection Operations														
A.M. Peak Hour P.M. Peak Hour														
Intersection LOS Delay (s) LOS Delay (s)														
Martintown Rd at Southwood Rd/Curtis Dr	Α	1.9	Α	1.3										
- eastbound approach	C	21.8	D	28.9										
 westbound approach 	D	34.6	F	52.1										
- northbound left-turn	В	11.2	В	12.3										
- southbound left-turn	В	11.3	В	12.6										
Martintown Rd at Courtney Dr	Α	1.0	Α	0.5										
- westbound approach	D	27.4	F	50.2										
- southbound left-turn	В	11.6	С	16.6										

As shown by the results in Table 6, while overall operations for each intersection is within the LOS Standard in the No-Build Condition, delay along the westbound side street approaches are operating at LOS F during the evening peak hour at both intersections. This is due to the relatively heavy volume of traffic along Martintown Road that limit gaps for the side street exiting movements which is not uncommon or outside of driver expectations in an urban area accessing an arterial roadway during peak hours.







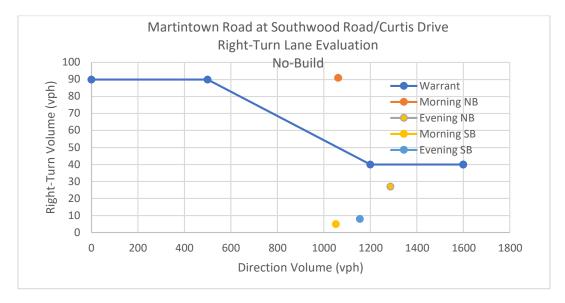
Wrenfield at Chanticleer Traffic Impact Analysis

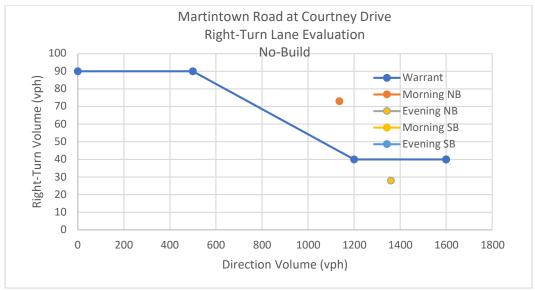
Traffic Volumes

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No Build Auxiliary Lane Analyses

As with the Existing Conditions, the intersections of Martintown Road at Southwood Road/Curtis Drive and Martintown Road at Courtney Drive in the No-Build Condition was evaluated in accordance with section 9.5 Auxiliary Turn Lanes of the SC DOT Roadway Design Manual (March 2021) and is shown below:





As would be expected with the increased traffic from background growth, a right-turn lane continues to be warranted for the northbound approach at both intersections. Initial analysis with the inclusion of the northbound right-turn lane showed slight improvement of the overall intersection operations, but continued LOS F operation for the westbound approach.

Outside of a change in traffic control, such as signalization which would likely be warranted, the only way to improve the side street operations would be to restripe the westbound approaches to provide separate left-turn and right-turn lanes.

Analysis was performed for the No-Build Condition with the above system improvements and is presented in Table 6.

Table 6 2026 No-Build Intersection Operations with System Improvements														
A.M. Peak Hour P.M. Peak Hour														
Intersection	LOS	Delay (s)	LOS	Delay (s)										
Martintown Rd at Southwood Rd/Curtis Dr	Α	1.6	Α	1.1										
- eastbound approach	С	21.7	D	28.9										
 westbound left-turn 	E	38.9	F	56.2										
- westbound right-turn	В	14.4	С	20.2										
- northbound left-turn	В	11.2	В	12.3										
- southbound left-turn	В	11.3	В	12.6										
Martintown Rd at Courtney Dr	Α	0.8	Α	0.5										
- westbound left-turn	D	31.1	F	56.2										
- westbound right-turn B 13.6 C 18.1														
- southbound left-turn	В	11.6	С	16.6										

As shown by the above analyses, the addition of a northbound right-turn lane at both intersections does not result in significant improvement of overall operation of either intersection. The delays are improved somewhat for the westbound right-turns, but operations of the left-turns still fall in the LOS F range.

To improve the left-turn delays below LOS F, would require signalization, which is not likely to be warranted due to the low side-street volumes, which account for less than 5% of the total traffic at the intersection. Therefore, careful consideration should be given prior to implementing any improvements to determine if the benefit justifies this level of investment.

Because these improvements are necessary to address background deficiencies, they are considered "system" improvements. "System" improvements are those required to mitigate existing deficiencies not associated with traffic generated by the proposed development not typically considered to be the whole responsibility of the developer.



PROJECT TRAFFIC PROJECTIONS

WCN is proposed to include 123-unit single family homes located on an a 66.9-acre tract located at the existing "stub-out" of Big Pine Road in the existing Chanticleer neighborhood in North Augusta, South Carolina. Full Build-out is expected by 2026.

Trip Generation

An estimate of traffic that will be generated by WCN was made based on trip generation characteristics for similar land uses nationwide. The trip generation rates used in this study were taken from the 11th edition of the Institute of Transportation Engineers' (ITE) <u>Trip Generation</u> report utilizing the following land-uses: *ITE Land Use 210 – Single-Family Detached Housing*.

Table 7 presents a summary of the projected trip generation Deerfield Pines.

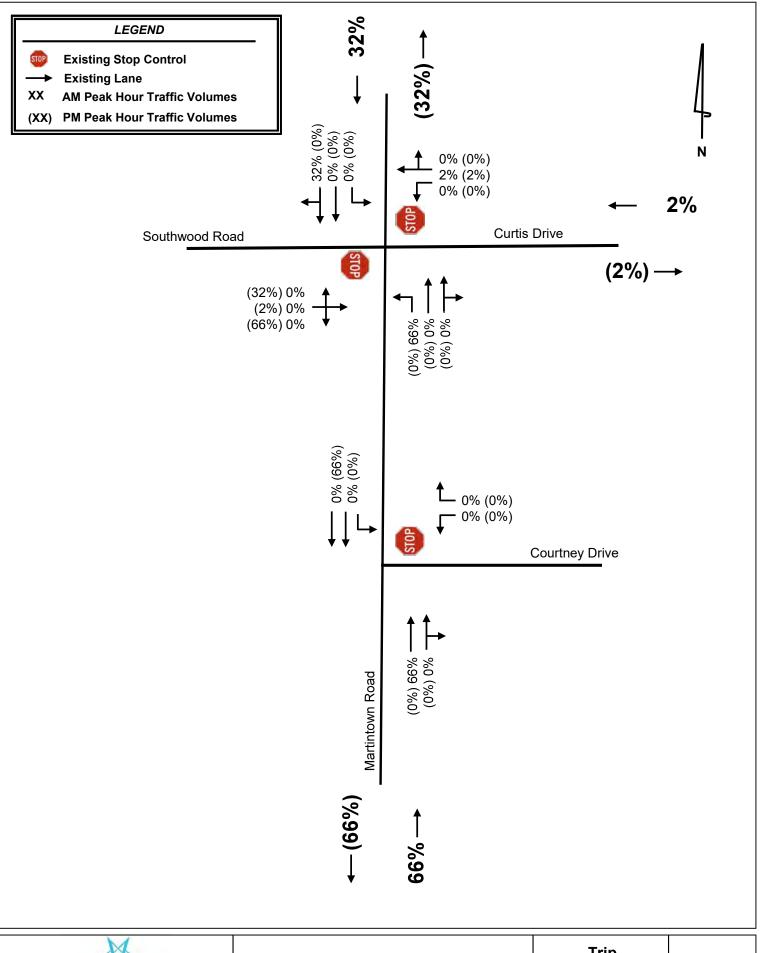
Table 7 Trip Generation													
Size A.M. Peak Hour P.M. Peak Hour 2													
Land Use		Enter	Exit	Total	Enter	Exit	Total	2-way					
220 – Single-Family Detached	123	23	67	90	76	45	121	1,221					

Trip Distribution and Traffic Assignment

Trip distribution describes the direction drivers will be going to and coming from when they turn into and depart from the development. Typically, this type of development draws from the local area, and therefore, it is believed that using the existing travel patterns in the area will most closely approximate the trip distribution for this site.

This trip distribution developed for WCN is shown in Figure 4. The projected traffic that will be generated by this project was assigned to the study area based on this distribution is shown in Figure 5.



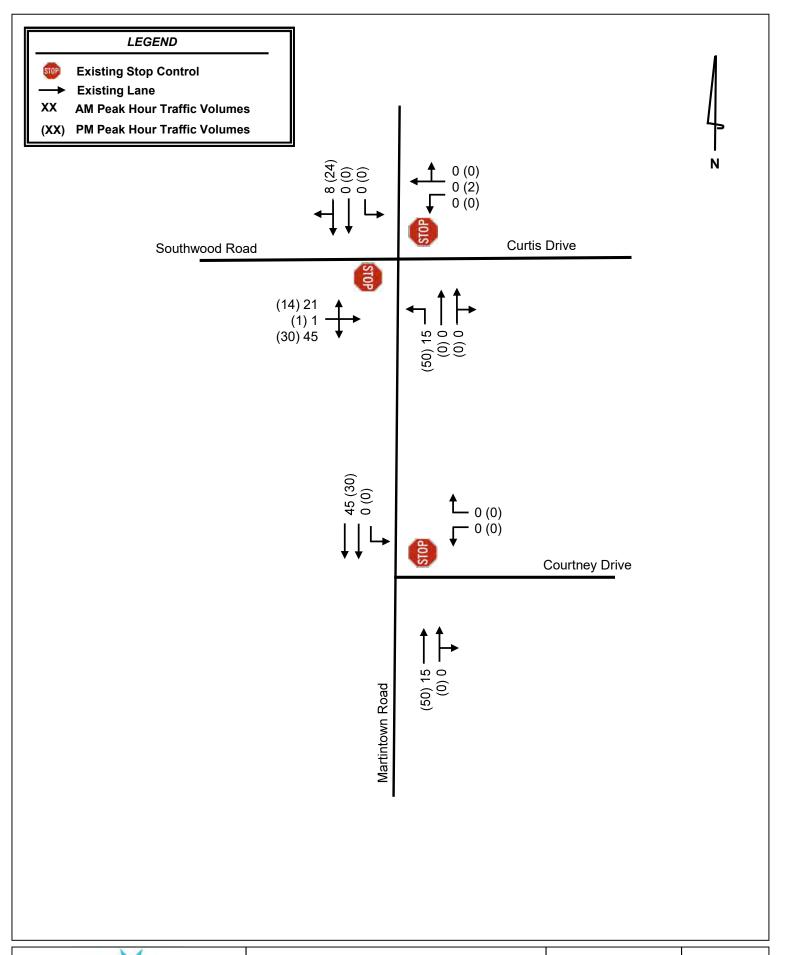




Wrenfield at Chanticleer Traffic Impact Analysis Trip Distribution

Figure 4

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FUTURE CONDITIONS

Future Traffic Volumes

Future Conditions represents traffic conditions at full build-out of WCN. Future traffic volumes are made up of the 2026 No-Build Traffic volumes, presented previously in Figure 3, plus the site generated volumes shown in Figure 5. Figure 6 shows the future traffic volumes for after completion WCN.

These volumes were used to analyze the 2026 Future traffic conditions surrounding the site with existing intersection geometry. The results of this analysis are presented in Table 8.

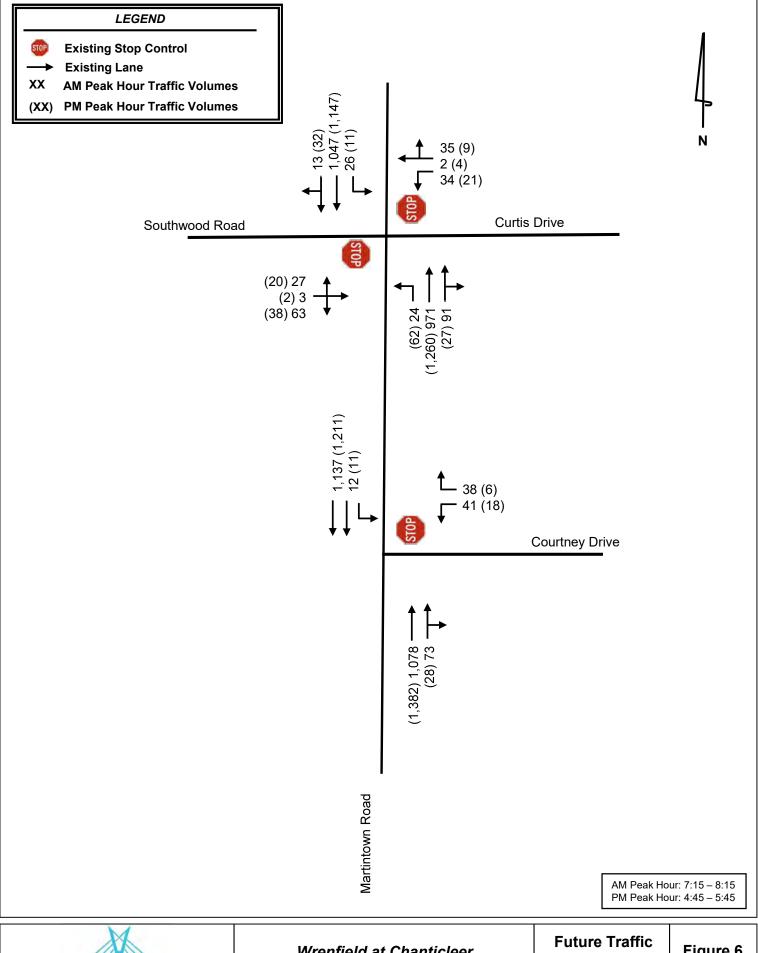
Table 8 2026 Future Intersection Operations														
A.M. Peak Hour P.M. Peak Hour														
Intersection LOS Delay (s) LOS Delay (s)														
Martintown Rd at Southwood Rd/Curtis Dr	Α	4.0	Α	1.3										
- eastbound approach	E	39.7	E	45.2										
 westbound approach 	E	41.1	F	79.6										
- northbound left-turn	В	11.4	В	13.4										
- southbound left-turn	В	11.3	В	12.6										
Martintown Rd at Courtney Dr	Α	1.0	Α	0.5										
- westbound approach	D	28.0	F	50.2										
- southbound left-turn	В	11.7	С	16.6										

As shown by the results in Table 8, as with previous conditions, while overall operations for each intersection is within the LOS Standard in the Future Conditions, however delay along the westbound side street approaches are operating at LOS E and LOS F during the evening peak hour at both intersections. This is due to the relatively heavy volume of traffic along Martintown Road that limit gaps for the side street exiting movements which is not uncommon or outside of driver expectations in an urban area accessing an arterial roadway during peak hours.

Auxiliary Lane Analyses

As with the Existing Conditions and No-Build, the intersections of Martintown Road at Southwood Road/Curtis Drive and Martintown Road at Courtney Drive in the No-Build Condition was evaluated in accordance with section 9.5 Auxiliary Turn Lanes of the SC DOT Roadway Design Manual (March 2021) and is shown below:





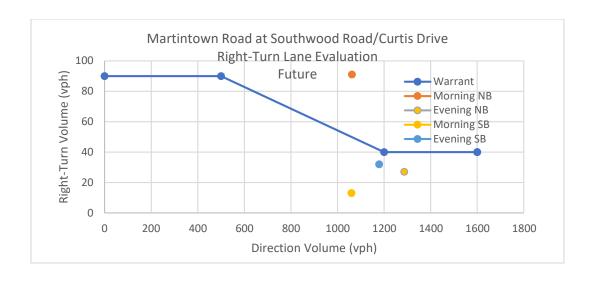


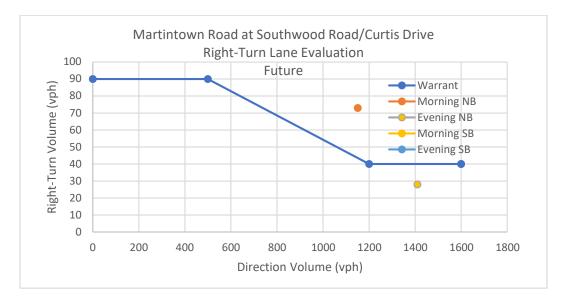
Wrenfield at Chanticleer Traffic Impact Analysis

Volumes

Figure 6

Page 20





As would be expected with the increased traffic from background growth, a right-turn lane continues to be warranted for the northbound approach at both intersections. Initial analysis with the inclusion of the northbound right-turn lanes showed slight improvement of the overall intersection operations, but continued LOS F operation for the westbound approach.

Outside of a change in traffic control, such as signalization which would likely be warranted, the only way to improve the side street operations would be to restripe the westbound approaches to provide separate left-turn and right-turn lanes.



Because these improvements are necessary to address background deficiencies, they are considered "system" improvements. "System" improvements are those required to mitigate existing deficiencies not associated with traffic generated by the proposed development not typically considered to be the whole responsibility of the developer.

With addition of project traffic, it was found that, in addition to the system improvements identified above that modification of the eastbound approach of Southwood Road to include separate left-turn and right-turn lanes will improve operations of the approach as well.

Analysis was performed for the Future Condition with the above system improvements and is presented in Table 9.

Table 9 2026 Future Intersection Operations with Improvements														
A.M. Peak Hour P.M. Peak Hour														
Intersection LOS Delay (s) LOS Delay (s)														
Martintown Rd at Southwood Rd/Curtis Dr	Α	2.9	Α	2.5										
- eastbound left-turn	E	47.8	F	656										
- eastbound right-turn	C	16.6	С	17.1										
 westbound left-turn 	E	47.6	F	86.0										
- westbound right-turn	В	14.6	С	23.1										
- northbound left-turn	В	11.4	В	13.4										
- southbound left-turn	В	11.3	В	12.6										
Martintown Rd at Courtney Dr	Α	0.8	Α	0.5										
- westbound left-turn	D	31.7	F	61.8										
- westbound right-turn	В	13.7	С	18.8										
- southbound left-turn	В	11.7	С	17.3										

As shown by the above analyses, the addition of a northbound right-turn lane at both intersections does not result in significant improvement of overall operation of either intersection. Restriping the westbound approaches to the intersections offers some improvement for all movements except left-turns which are projected to continue to operate at LOS F.

Additionally, the addition of a right-turn lane eastbound right-turn lane to Southwood Road would require some widening to the south of approximately five-feet that may require acquisition of right-of-way.

Therefore, careful consideration should be given to adding these lanes to determine if the benefit justifies this level of investment.



STUDY FINDINGS

This report analyzes the traffic impact of the proposed Wrenfield at Chanticleer neighborhood (WCN) which will include 123 single-family homes to be located on a 66.9-acre tract located at the existing "stub-out" of Big Pine Road in the existing Chanticleer neighborhood in North Augusta, South Carolina. Full Build-out is expected by 2026.

The location of the proposed development is shown in Figure 1.

Access for the additional homes will be provided via Southwood Road, which is the existing main access fort the Chanticleer neighborhood at Martintown Road.

Analyses were performed for the morning and evening peak hours under three scenarios: existing, future no-build, and future build conditions for the following intersections:

- Martintown Road (SC-230) at Southwood Road/Curtis Drive and
- Martintown Road (SC-230) at Courtney Drive

Historic growth rates and proposed developments in the area to be accounted for were determined through a combination of historic traffic volume data, population projections for the surrounding area, and review of the West Martintown Road Corridor Study (performed by AECOM and adopted by North Augusta City Council in 2021). Based on this methodology, a 2.0% annual growth rate was projected and applied to the existing traffic volumes for a period of five years. Projected traffic volumes for the proposed River Falls Apartments and Hamrick Farms developments were added this growth to establish the 2026 No-Build traffic volumes for the intersection.

Analysis of the existing and no-build conditions showed that there are delays along the side-street approaches of Curtis Drive and Courtney Drive were in the LOS F range. These delays are primarily due to the relatively heavy volume of traffic along Martintown Road and can be improved somewhat by restriping these approaches to separate left-turns and right-turns to allow the right-turns to go around the queued left-turning vehicles. However, this will still result in LOS F operations for the left-turns. To improve the left-turn delays below LOS F, would require signalization, which is not likely to be warranted due to the low side-street volumes, which represent less than 5% of the total traffic at the intersections.

Whiles these improvements are considered a "system" improvement that not typically considered to be the whole responsibility of the developer, careful consideration should be given prior to implementing any improvements to determine if the benefit justifies this level of investment.



Traffic generated by WCN was estimated using the 11th Edition of the ITE <u>Trip Generation</u> report, Land Use 220 – Single-Family Attached Housing. Based on this methodology, the development is expected to generate 1,221 daily trips with 90 occurring during the morning peak hour and 121 occurring during the evening peak hour.

These volumes were distributed to the study network based existing travel patterns added to the 2026 No-Build traffic volumes to estimate the Future traffic volumes after the completion of the WCN.

Based on analyses of the future condition, in addition to deficiencies identified for existing and background deficiencies, the westbound approach of Southwood Drive is projected to operate at LOS F with its existing configuration.

As stated for the other approaches in the existing and background conditions, delays are due to the relatively heavy volume of traffic along Martintown Road and can be improved somewhat by with limited widening and restriping to separate left-turns and right-turns to allow the right-turns to go around the queued left-turning vehicles. While this will allow the right-turns to flow more efficiently, it will still result in LOS F operations for the left-turns., which could on be improved through signalization. However, a change in traffic control at this intersection is not likely to be warranted due to the low side-street volumes, which represent less than 5% of the total traffic at the intersection.

Moreover, careful consideration should be given prior to implementing any improvements to determine if the benefit justifies this level of investment.



APPENDIX



TRAFFIC DATA

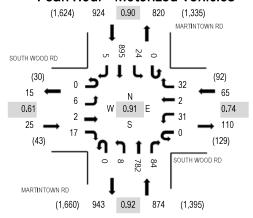


Location: #1 MARTINTOWN RD & SOUTH WOOD RD AM

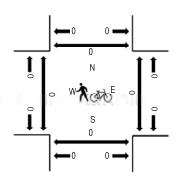
Date: Tuesday, March 8, 2022 **Peak Hour:** 07:15 AM - 08:15 AM

Peak 15-Minutes: 07:30 AM - 07:45 AM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

SOUTH WOOD RD			RD	SOL	JTH W	OOD R	D	MARTINTOWN RD				MARTINTOWN RD										
Interval	Eastbound					Westbound				Northbound			Southbound					Rolling	Pedestrian Crossings			
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
7:00 AM	0	3	0	4	0	4	1	2	0	1	128	4	0	3	192	0	342	1,804	0	0	0	0
7:15 AM	0	0	0	5	0	4	0	5	0	3	183	12	0	5	226	0	443	1,888	0	0	0	0
7:30 AM	0	1	2	1	0	6	0	12	0	0	222	16	0	5	251	0	516	1,778	0	0	0	0
7: 4 5 AM	0	3	0	8	0	9	2	11	0	1	206	27	0	13	221	2	503	1,549	0	0	0	0
8:00 AM	0	2	0	3	0	12	0	4	0	4	171	29	0	1	197	3	426	1,350	0	0	0	0
8:15 AM	0	1	0	3	0	6	0	3	0	3	114	4	1	2	194	2	333		0	0	0	0
8:30 AM	0	1	0	5	0	3	1	1	0	4	125	2	0	1	143	1	287		0	0	0	0
8:45 AM	0	0	0	1	0	2	0	4	0	2	132	2	0	1	160	0	304		0	0	0	0

Eastbound					Westbound				Northbound				Southbound				
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	2	0	0	0	4	0	6
Lights	0	6	2	17	0	31	2	32	0	8	776	84	0	24	886	5	1,873
Mediums	0	0	0	0	0	0	0	0	0	0	4	0	0	0	5	0	9
Total	0	6	2	17	0	31	2	32	0	8	782	84	0	24	895	5	1,888

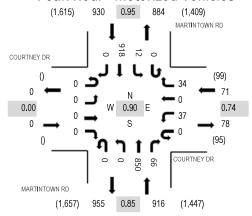


Location: #2 MARTINTOWN RD & COURTNEY DR AM

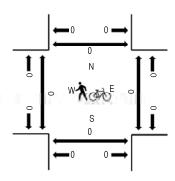
Date: Tuesday, March 8, 2022 **Peak Hour:** 07:15 AM - 08:15 AM

Peak 15-Minutes: 07:30 AM - 07:45 AM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	C	OURTI	NEY DE	7	CC	DURTN	EY DF	₹	MA	RTINT	OWN R	D	MA	RTINT	OWN F	RD.						
Interval		Eastb	ound			Westb	ound			Northb	ound			South	oound			Rolling	Ped	destriar	n Crossir	ngs
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
7:00 AM	0	0	0	0	0	9	0	4	0	0	118	6	0	0	192	0	329	1,805	0	0	0	0
7:15 AM	0	0	0	0	0	12	0	2	0	0	191	14	0	2	221	0	442	1,917	0	0	0	0
7:30 AM	0	0	0	0	0	9	0	9	0	0	236	35	0	2	241	0	532	1,798	0	0	0	0
7:45 AM	0	0	0	0	0	5	0	10	0	0	228	13	0	6	240	0	502	1,557	0	0	0	0
8:00 AM	0	0	0	0	0	11	0	13	0	0	195	4	0	2	216	0	441	1,356	0	0	0	0
8:15 AM	0	0	0	0	0	5	0	1	0	0	136	4	0	1	176	0	323		0	0	0	0
8:30 AM	0	0	0	0	0	4	0	0	0	0	127	2	0	2	156	0	291		0	0	0	0
8:45 AM	0	0	0	0	0	3	0	2	0	0	137	1	0	1	157	0	301		0	0	0	0

		East	bound			Westk	oound			Northb	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	3	0	0	0	6	0	9
Lights	0	0	0	0	0	37	0	34	0	0	843	66	0	12	908	0	1,900
Mediums	0	0	0	0	0	0	0	0	0	0	4	0	0	0	4	0	8
Total	0	0	0	0	0	37	0	34	0	0	850	66	0	12	918	0	1,917

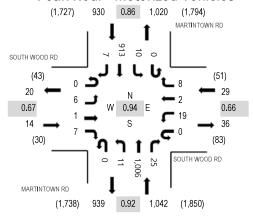


Location: #1 MARTINTOWN RD & SOUTH WOOD RD PM

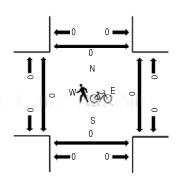
Date: Tuesday, March 8, 2022 **Peak Hour:** 04:45 PM - 05:45 PM

Peak 15-Minutes: 05:15 PM - 05:30 PM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	SO	UTH W	OOD F	RD	SOL	JTH W	OOD RE)	MA	RTINT	OWN R	D	MA	RTINT	OWN F	RD.						
Interval		Eastb	ound			Westb	ound			Northb	ound			South	oound			Rolling	Ped	lestriar	n Crossir	ngs
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru F	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
4:00 PM	0	3	0	2	0	4	0	3	0	2	198	7	0	3	181	6	409	1,713	0	0	0	0
4:15 PM	0	0	1	0	0	1	0	1	0	2	176	9	0	2	196	2	390	1,811	0	0	0	0
4:30 PM	0	0	0	5	0	5	1	1	0	3	207	12	0	3	202	2	441	1,959	0	0	0	0
4:45 PM	0	2	0	1	0	6	1	4	0	4	238	5	0	1	211	0	473	2,015	0	0	0	0
5:00 PM	0	1	0	2	0	4	0	2	0	2	273	7	0	4	210	2	507	1,945	0	0	0	0
5:15 PM	0	1	0	1	0	4	0	1	0	4	254	4	0	4	263	2	538		0	0	0	0
5:30 PM	0	2	1	3	0	5	1	1	0	1	241	9	0	1	229	3	497		0	0	0	0
5:45 PM	0	1	1	3	0	4	1	1	0	3	183	6	0	3	196	1	403		0	1	0	0

		East	bound			Westk	oound			North	bound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	2	0	0	0	5	0	7
Lights	0	6	1	7	0	19	2	8	0	11	1,003	25	0	10	907	7	2,006
Mediums	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	2
Total	0	6	1	7	0	19	2	8	0	11	1,006	25	0	10	913	7	2,015

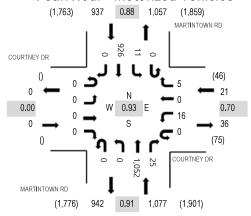


Location: #2 MARTINTOWN RD & COURTNEY DR PM

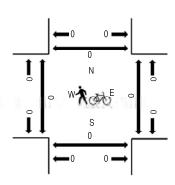
Date: Tuesday, March 8, 2022 **Peak Hour:** 04:45 PM - 05:45 PM

Peak 15-Minutes: 05:15 PM - 05:30 PM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	Interval	С	OURTI Eastb	NEY DI	₹		OURTN Westb	EY DR		MA	RTINT(Northb		D	MA	RTINT South	OWN F	RD		Rolling	Ped	destriar	n Crossii	ngs
	Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru F	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West		South	
_	4:00 PM	0	0	0	0	0	8	0	2	0	0	205	2	0	2	197	0	416	1,724	0	0	0	0
	4:15 PM	0	0	0	0	0	4	0	1	0	0	186	6	0	1	182	0	380	1,825	0	0	0	0
	4:30 PM	0	0	0	0	0	5	0	1	0	0	224	14	0	6	218	0	468	1,993	0	0	0	0
	4:45 PM	0	0	0	0	0	5	0	2	0	0	235	4	0	1	213	0	460	2,035	0	0	0	0
	5:00 PM	0	0	0	0	0	2	0	1	0	0	285	11	0	4	214	0	517	1,986	0	0	0	0
	5:15 PM	0	0	0	0	0	4	0	1	0	0	269	6	0	2	266	0	548		0	0	0	0
	5:30 PM	0	0	0	0	0	5	0	1	0	0	263	4	0	4	233	0	510		0	0	0	0
	5:45 PM	0	0	0	0	0	3	0	1	0	0	182	5	0	3	217	0	411		0	1	0	0

		East	bound			Westh	oound			North	bound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	2	0	0	0	5	0	7
Lights	0	0	0	0	0	16	0	5	0	0	1,049	25	0	11	919	0	2,025
Mediums	0	0	0	0	0	0	0	0	0	0	1	0	0	0	2	0	3
Total	0	0	0	0	0	16	0	5	0	0	1,052	25	0	11	926	0	2,035

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Site Code: 1 Station ID: 1 MARTINTOWN RD SOUTH OF SOUTHWOOD RD

	08-Mar-22 Tue	NB	SB		Total
Time 12:00 AM		8	14		22
12:15		12	8		20
12:30		10	4		14
12:45		6	3		9
01:00		2	8		10 8 7
01:15		5	3		8
01:30		1	6		7
01:45		1	2		3
02:00		3	0		3
02:15		2	1		3 3 3 8 12
02:30		3	5		8
02:45		9	3		12
03:00		5	3		8
03:15		2	6		8
03:30		6	5		11
03:45		4	8		12
04:00		8	12		20
04:15		11	18		29
04:30		9	20		29
04:45		21	39		60
05:00		15	44		59
05:15		25	54		79
05:30		34	47		81
05:45		44	63		107
06:00		38	63		101
06:15		59	72		131
06:30		74	97		171
06:45		81	115		196
07:00		92	141		233
07:15		141	182		323
07:30		176	192		368
07:45		162	214		376
08:00		175	181		356
08:15		118	168		286
08:30		101	145		246
08:45		125	146		271
09:00		104	107		211
09:15		100 87	110		210
09:30 09:45		87	98 123		185 210
10:00		92	114		206
10:00		116	113		229
10:13		97	125		222
10:30		114	123		235
11:00		107	110		217
11:15		107	125		226
11:30		99	143		242
11:45		108	129		237
Total		2800	3510		6310
Percent		44.4%	55.6%		23.3
Peak	_	07:15	07:15	 	07:15
Vol.	_	654	769	 	1423
P.H.F.		0.929	0.898		0.946

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Site Code: 1 Station ID: 1 MARTINTOWN RD SOUTH OF SOUTHWOOD RD

Start Time	08-Mar-22 Tue	NB	SB							Total
12:00 PM	140	130	131	;						261
12:15		118	111							229
12:30		100	142							242
12:45		101	136							237
01:00		109	140							249
01:15		142	124							266
01:30		117	141							258
01:45		115	144							259
02:00		106	137							243
02:15		102	150							252
02:30		160	151							311
02:45		134	151							285
03:00		161	151							312
03:15		176	147							323
03:30		149	196							345
03:45		129	181							310
04:00		137	162							299
04:15		148	138							286
04:30		171	179							350
04:45		164	185							349
05:00		180	170							350
05:15		181	229							410
05:30		158	168							326
05:45		120	179							299
06:00		146	184							330
06:15		130	188							318
06:30		118	156							274
06:45		106	121							227
07:00		111	110							221
07:15		78	89							167
07:30		82	75							157
07:45		91	88							179
08:00		70	64							134
08:15		70	65							135
08:30		62	42							104
08:45		64	66							130
09:00		67	46							113
09:15		53	4 9							102
09:30		45	33							78
09:45		59	24							83
10:00		47	24							71
10:15		43	34							77
10:30		31	25							56
10:45		27	21							48
11:00		18	23							41
11:15		8	14							22
11:30		6	22							28
11:45		17	15							32
Total		4857	5321							10178
Percent		47.7%	52.3%							40.00
Peak	-	16:30	16:30	-	=	-	-	-	-	16:30
Vol.	-	696	763	-	-	-	-	-	-	1459
P.H.F.		0.961	0.833							0.890
Grand		7657	8831							16488
Total										
Percent		46.4%	53.6%							

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Site Code: 2 Station ID: 2 SOUTHWOOD RD WEST OF MARTINTOWN RD

Start	08-Mar-22		MD				Total
12:00 AM	Tue	EB0	WB 0				0
12:15		0	0				
12:30		0	2				0 2 2 2 0
12:45		0	2				2
01:00		2	0				2
01:15		0	0				0
01:30		0	0				0
01:45		0	Ö				0
02:00		0	Ö				0
02:15		Ö	Ö				Ö
02:30		Ö	Ö				0
02:45		0	0				0
03:00		0	0				0
03:15		0	1				1
03:30		1	0				1
03:45		0	0				0
04:00		0	0				0
04:15		0	0				0
04:30		0	0				0
04:45		0	2				2
05:00		1	0				1
05:15		2	2				4 2 2
05:30		2	0				2
05:45		2	0				2
06:00		9	1				10
06:15		5	1				6
06:30		8	1				9
06:45		10	3				13
07:00 07:15		6	6 2				12
07:13		4 16	7				6 23
07:45		4	10				14
08:00		4	13				17
08:15		11	7				18
08:30		5	11				16
08:45		2	5				7
09:00		6	11				17
09:15		2	2				4
09:30		8	3				11
09:45		2	2				4
10:00		4	1				5
10:15		7	6				13
10:30		1	4				5
10:45		3	13				16
11:00		9	7				16
11:15		6	5				11
11:30		10	8				18
11:45		4	6				10
Total		156	144				300
Percent Peak		52.0% 06:45	48.0% 07:45				- 07:30
Vol.	-	36	07:45 4 1	 -	-	<u>-</u>	- 07:30 - 72
P.H.F.	-	0.563	0.788	 -	-	-	0.783
17.414474		0.003	0.700				0.703

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Site Code: 2 Station ID: 2 SOUTHWOOD RD WEST OF MARTINTOWN RD

Start	08-Mar-22									Total
Time	Tue	EB	WB							
12:00 PM		3	4							7
12:15		9	5							14 13
12:30 12:45		5 2	8 5							7
01:00		2	10							19
01:15		9 7	8							15
01:30		6	10							16
01:45		7	10							17
02:00		6	7							13
02:15		8	11							19
02:30		8	16							24
02:45		6	4							10
03:00		5	8							13
03:15		4	7							11
03:30		4	15							19
03:45		9	13							22
04:00		0	10							10
04:15		6	9							15
04:30		8	10							18
04:45		5	4							9
05:00		5	10							15
05:15		7	12							19
05:30		5	7							12
05:45		2	8							10
06:00 06:15		4	11 6							15 15
06:13		9 7	12							19
06:30		10	13							23
07:00		3	10							13
07:15		0	4							4
07:30		3	1							
07:45		3	0							4 3 4 3 5 3 4 3 3 3
08:00		Ö	4							4
08:15		2	1							3
08:30		2	3							5
08:45		0	3							3
09:00		2	2							4
09:15		2	1							3
09:30		1	2 2							3
09:45		1	2							3
10:00		0	0							
10:15		1	2							3
10:30		0	6							6
10:45		0	0							0
11:00		0	2							2
11:15		0	0							0
11:30		0	0							0
11:45 Total		0 186	296						<u> </u>	<u>0</u> 482
Percent		38.6%	296 61.4%							402
Percent		18:00	15:30				_	_		13:45
Vol.	-	30	47	-	-	-	-	-	<u>-</u>	73
P.H.F.	_	0.750	0.783	_	-	_	-	_	-	0.760
Grand							-			
Total		342	440							782
Percent		43.7%	56.3%							

TRAFFIC VOLUME WORKSHEETS



Aiken County,SC 3/9/2022

AM Peak

		East	Eastbound			Westbound	puno			North	Northbound			Sout	Southbound		Intersection
	_	<u> </u>	2	Total	7	⊢	~	Total	_	_	2	Total	7	_	~	Total	Total
Existing	9	2	17	25	31	7	32	65	8	782	84	874	24	895	2	924	1888
D Factor																	
PHF	0.61	0.61	0.61	0.61	0.74	0.74	0.74	0.74	0.92	0.92	0.92	0.92	06.0	06.0	06.0	0.90	
BG Growth Rate	2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		
Years Growth	4	4	4		4	4	4		4	4	4		4	4	4		
Background Growth	9	7	18	56	34	2	32	7	0	846	91	946	26	696	2	1000	2,043
River Falls		0	0		0	0	0	0	0	œ	0	80	0	24	0	24	32
Hamrick Phase 1		0	0		0	0	0	0	0	117	0	117	0	54	0	24	171
Total Background	9	7	18	26	34	2	35	71	6	971	91	1,071	56	1,047	2	1,078	2,246
Site Generated	72	0	42	99	0	0	0	0	15	0	0	15	0	0	8	80	88
Future	27	2	63	92	34	2	35	71	24	1/6	91	1,086	56	1,047	13	1,086	2,335

PM Peak

		East	Eastbound			Westbound	punoc			Northbound	punoc			South	Southbound		Intersection
		 -	2	Total	_	L	~	Total	7	_	ď	Total	_	_	2	Total	Total
Existing	9	_	7	4	19	2	8	29	11	1,006	25	1,042	10	913	7	930	2,015
D Factor																	
PHF	0.67	0.67	0.67	0.67	99.0	99.0	99.0	99.0	0.92	0.92	0.92	0.92	0.86	98.0	98.0	98.0	
Growth	2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		
Years Growth	4	4	4		4	4	4		4	4	4		4	4	4		
Background Growth	9	_	80	15	21	2	တ	32	12	1089	27	1128	11	988	80	1007	2,182
River Falls		0	0		0	0	0	0	0	22	0	25	0	15	0	15	40
Hamrick Phase 1		0	0		0	0	0	0	0	146	0	146	0	144	0	144	290
Total Background	9	-	œ	15	21	7	6	32	12	1,260	27	1,299	7	1,147	œ	1,166	2,512
Site Generated	14	0	30	4	0	0	0	0	20	0	0	20	0	0	24	54	118
													2				
Future	20	1	38	29	21	2	6	32	62	1,260	27	1,349	11	1,147	32	1,190	2,630

AM Peak

		East	Eastbound			Westbound	punoc			Northbound	puno			South	Southbound		Intersection
	٦	⊥	ď	Total	T		ď	Total	7	_	Υ.	Total	7	⊢	Я	Total	Total
Existing	0	0	0	0	37	0	34	71	0	820	99	916	12	918	0	930	1917
D Factor																	
PHF	0.00	0.00	00.0	0.00	0.74	00.0	0.74	0.74	00.0	0.74	0.74	0.74	0.95	0.95	0.00	0.95	
BG Growth Rate	2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		
Years Growth	2	2	2		2	2	2		2	2	2		2	2	2		
Background Growth	0	0	0	0	41	0	38	79	0	938	73	1011	13	1014	0	1027	2,117
River Falls	0	0	0	0	0	0	0	0	0	8	0	8	0	24	0	24	32
Hamrick Phase 1	0	0	0	0	0	0	0	0	0	117	0	117	0	54	0	54	171
Total Background	0	0	0	0	41	0	38	79	0	1063	73	1,136	13	1092	0	1,105	2,320
Site Generated	0	0	0	0	0	0	0	0	0	15	0	15	0	45	0	45	09
Future	0	0	0	0	4	0	38	79	0	1,078	73	1,151	0	1,137	0	1,137	2,367

PM Peak

		East	Eastbound			Westbound	puno			Northbound	punoc			Sout	Southbound		Intersection
	7	⊢	Ж	Total	٦	_	ď	Total	7	⊢	ď	Total	٦	⊢	ድ	Total	Total
Existing	0	0	0	0	16	0	2	21	0	1,052	25	1,077	11	926	0	937	2035
D Factor																	
PHF	0.83	0.83	0.83	0.83	0.89	0.89	0.89	0.89	0.74	0.74	0.74	0.74	0.86	0.86	0.86	0.86	
Growth	2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		2.00%	2.00%	2.00%		
Years Growth	2	2	2		2	2	2		2	2	2		2	2	2		
Background Growth	0	0	0	0	18	0	9	54	0	1161	28	1189	12	1022	0	1034	2,247
River Falls	0	0	0	0	0	0	0	0	0	22	0	22	0	15	0	15	40
Hamrick Phase 1	0	0	0	0	0	0	0	0	0	146	0	146	0	144	0	144	290
Total Background	0	0	0	0	18	0	9	24	0	1332	28	1,360	12	1181	0	1,193	2,577
Site Generated	0	0	0	0	0	0	0	0	0	20	0	20	0	30	0	0	20
Future	0	0	0	0	18	0	9	24	0	1,382	28	1,410	0	1,211	0	1,211	2,645

EXISTING INTERSECTION OPERATIONS



Intersection												
Int Delay, s/veh	1.5											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		7	41		-	14	
Traffic Vol, veh/h	6	2	17	31	2	32	8	782	84	24	895	5
Future Vol, veh/h	6	2	17	31	2	32	8	782	84	24	895	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	250	-	-	250	-	-
Veh in Median Storage	,# -	1	-	-	1	-	-	0	-	-	0	-
Grade, %	_	0	-	-	0	_	-	0	_	-	0	-
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	10	3	28	42	3	43	9	850	91	27	994	6
Major/Minor N	Minor2		_	Minor1			Major1		N	Major2		
Conflicting Flow All	1496	2010	500	1467	1968	471	1000	0	0	941	0	0
Stage 1	1051	1051	-	914	914	-	-	-	-	-	_	_
Stage 2	445	959	_	553	1054	-	_	-	_	_	-	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	-	_
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-		-	_	-	-	_
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	-	-	-	-	-	_	_
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	-	_
Pot Cap-1 Maneuver	85	58	516	89	62	539	688	_	_	724	_	_
Stage 1	243	302	-	294	350	-	_	-	_	-	-	_
Stage 2	562	334	-	485	301	-	-	-	-	-	-	_
Platoon blocked, %								_	_		-	_
Mov Cap-1 Maneuver	74	55	516	80	59	539	688	-	-	724	-	_
Mov Cap-2 Maneuver	175	161	-	193	168	-	-	-	-	-	-	-
Stage 1	240	291	-	290	345	-	-	-	-	-	-	_
Stage 2	506	330	_	437	290	-	_	_	_	_	-	_
Approach	EB			WB			NB			SB		
HCM Control Delay, s	18.2			23.6			0.1			0.3		
HCM LOS	С			С								
Minor Lane/Major Mvm	ıt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		688	_	_	314	280	724	_	_			
HCM Lane V/C Ratio		0.013	-	-		0.314		_	_			
HCM Control Delay (s)		10.3	-	-	18.2	23.6	10.2	-	-			
HCM Lane LOS		В	_	_	C	C	В	_	_			
HCM 95th %tile Q(veh)		0	_	_	0.4	1.3	0.1	_	-			

Intersection												
Int Delay, s/veh	1.5											
		EDT	EDD	MDI	MOT	WDD	NDI	NDT	NDD	ODI	ODT	000
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		7	^	7	7	1	_
Traffic Vol, veh/h	6	2	17	31	2	32	8	782	84	24	895	5
Future Vol, veh/h	6	2	17	31	2	32	8	782	84	24	895	5
Conflicting Peds, #/hr	0	0	0	0	0	0	_ 0	_ 0	_ 0	_ 0	_ 0	_ 0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	250	-	150	250	-	-
Veh in Median Storage	e,# -	1	-	-	1	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	10	3	28	42	3	43	9	850	91	27	994	6
Major/Minor	Minor2		_	Minor1			Major1		Λ	/lajor2		
Conflicting Flow All	1496	2010	500	1421	1922	425	1000	0	0	941	0	0
Stage 1	1051	1051	500	868	868	723	1000		U	J + I		-
Stage 2	445	959	_	553	1054		_	_		_	_	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	<u>-</u>	4.14	_	-
Critical Hdwy Stg 1	6.54	5.54	0.94	6.54	5.54	0.34	7.14	_		7.14	_	_
Critical Hdwy Stg 2	6.54	5.54	<u>-</u>	6.54	5.54	_	<u>-</u>	_	<u>-</u>	<u>-</u>	-	<u>-</u>
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	_	-
Pot Cap-1 Maneuver	85	58	516	97	4.02	578	688	<u>-</u>	<u>-</u>	724	_	<u>-</u>
	243	302	310	314	368	3/0	000	-	-	124	_	-
Stage 1 Stage 2	562	334	-	485	301	-	-	-	-	-	-	-
Platoon blocked, %	302	334		400	JU I	-	-	-	-	-	_	-
Mov Cap-1 Maneuver	75	55	516	87	63	578	688	-	-	724	-	-
Mov Cap-1 Maneuver		161	510	202	173	3/0	000	-	-	124	_	-
Stage 1	240	291	-	310	363	-	-	-	-	-	-	-
	509	330	-	437	290		=	-		=		-
Stage 2	309	330	-	401	290	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	18.1			22.3			0.1			0.3		
HCM LOS	С			С								
Minor Lane/Major Mvr	nt	NBL	NBT	NBR F	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		688		-	315	295	724					
HCM Lane V/C Ratio		0.013	_	<u>-</u>		0.298	0.037	_	_			
HCM Control Delay (s	1	10.3	_		18.1	22.3	10.2		_			
HCM Lane LOS	7	10.3 B	-	<u>-</u>	C	22.3 C	В		_			
HCM 95th %tile Q(veh	1)	0			0.4	1.2	0.1		_			
	1)	U	_	_	0.4	1.2	0.1	_	_			

Intersection						
Int Delay, s/veh	0.8					
		WDD	NDT	NDD	CDI	CDT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	7	0.4	^	7	10	^
Traffic Vol, veh/h	37	34	850	66	12	918
Future Vol, veh/h	37	34	850	66	12	918
Conflicting Peds, #/hr	0	0	0	0	0	_ 0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	150	200	-
Veh in Median Storage		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	40	37	924	72	13	998
Major/Miner	Minari		Anic 1	N	Mais = 0	
	Minor1		Major1		Major2	
Conflicting Flow All	1449	462	0	0	996	0
Stage 1	924	-	-	-	-	-
Stage 2	525	-	-	-	-	-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	122	547	-	-	690	-
Stage 1	347	-	-	-	-	-
Stage 2	558	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	120	547	-	-	690	-
Mov Cap-2 Maneuver	245	-	-	_	-	_
Stage 1	347	_	_	-	-	-
Stage 2	547	_	_	_	_	_
Olago Z	JTI					
Approach	WB		NB		SB	
HCM Control Delay, s	19		0		0.1	
HCM LOS	С					
Minor Long/Major M.	a t	NDT	MDDV	MDI 1	CDI	CDT
Minor Lane/Major Mvn	IL	NBT		VBLn1	SBL	SBT
Capacity (veh/h)		-	-		690	-
HCM Lane V/C Ratio		-	-	0.232		-
HCM Control Delay (s)		-	-	19	10.3	-
HCM Lane LOS		-	-	С	В	-
HCM 95th %tile Q(veh		-	-	0.9	0.1	-

Intersection												
Int Delay, s/veh	0.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDIN	VVDL	4	VVDIX	T	^	T T)	14	ODIN
Traffic Vol, veh/h	6	1	7	19	2	8	11	1006	25	10	913	7
Future Vol, veh/h	6	1	7	19	2	8	11	1006	25	10	913	7
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	- -	-	None	-	- -	None	-	-	None	-	-	None
Storage Length	_	-	-	_	_	-	250	_	150	250	_	-
Veh in Median Storage	.# -	1	_	-	1	_		0	-	-	0	-
Grade, %	-	0	_	_	0	_	_	0	_	_	0	_
Peak Hour Factor	67	67	67	60	66	66	92	92	92	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	1	10	32	3	12	12	1093	27	12	1062	8
Major/Minor N	Minor2			Minor1		1	Major1		<u> </u>	Major2		
Conflicting Flow All	1662	2234	535	1673	2211	547	1070	0	0	1120	0	0
Stage 1	1090	1090	-	1117	1117	-	-	_	_	-	_	_
Stage 2	572	1144	_	556	1094	_	_	-	_	_	_	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	-	_
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	-	-	_	_	-	-
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	64	42	490	62	44	481	647	-	-	619	-	-
Stage 1	230	289	-	221	281	-	-	-	-	-	-	-
Stage 2	472	273	-	483	288	-	-	-	-	-	_	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	60	40	490	58	42	481	647	-	-	619	-	_
Mov Cap-2 Maneuver	160	141	-	156	144	-	-	-	-	-	-	-
Stage 1	226	284	-	217	276	-	-	-	-	-	-	-
Stage 2	447	268	-	461	283	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	21.6			30.4			0.1			0.1		
HCM LOS	С			D								
Minor Lane/Major Mvm	ıt	NBL	NBT	NBR I	EBLn1V	WBLn1	SBL	SBT	SBR			
Capacity (veh/h)		647	-	-		188	619	-	_			
HCM Lane V/C Ratio		0.018	_			0.249		_	_			
HCM Control Delay (s)		10.7	_	_		30.4	10.9	_	_			
HCM Lane LOS		В	_	-	C	D	В	_	_			
HCM 95th %tile Q(veh))	0.1	-	-	0.3	0.9	0.1	-	-			
					0.0	- 0.0						

EXISTING INTERSECTION OPERATIONS WITH SYSTEM IMPROVEMENTS



Int Delay, s/veh Movement Lane Configurations	0.4					
Movement Lane Configurations	0.4					
Lane Configurations		WDD	NDT	NDD	CDI	CDT
	WBL	WBR	NBT	NBR	SBL	SBT
T (C - \ / - ! ! //	**	_	^	7	11	^
Traffic Vol, veh/h	16	5	1052	25	11	926
Future Vol, veh/h	16	5	1052	25	11	926
Conflicting Peds, #/hr		0	_ 0	_ 0	_ 0	_ 0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	150	200	-
Veh in Median Storag		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	89	89	74	74	76	86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	18	6	1422	34	14	1077
Major/Minar	Minard	N	Anie 1		Mais = 0	
Major/Minor	Minor1		Major1		Major2	
Conflicting Flow All	1989	711	0	0	1456	0
Stage 1	1422	-	-	-	-	-
Stage 2	567	-	-	-	-	-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	53	375	-	-	461	-
Stage 1	189	-	-	-	-	-
Stage 2	531	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuve	r 51	375	-	-	461	-
Mov Cap-2 Maneuve		-	-	_	-	_
Stage 1	189	-	_	_	-	-
Stage 2	515	_	_	_	_	_
Glago Z	010					
Approach	WB		NB		SB	
	29.7		0		0.2	
HCM Control Delay, s	D					
HCM Control Delay, s HCM LOS						
HCM LOS	mt	NDT	NDDV	VDI ~1	CDI	CDT
HCM LOS Minor Lane/Major Mv	mt	NBT		VBLn1	SBL	SBT
Minor Lane/Major Mv Capacity (veh/h)		-	-	169	461	-
Minor Lane/Major Mv Capacity (veh/h) HCM Lane V/C Ratio		NBT - -	-	169 0.14	461 0.031	-
Minor Lane/Major Mv Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s		-	-	169 0.14 29.7	461 0.031 13.1	- - -
Minor Lane/Major Mv Capacity (veh/h) HCM Lane V/C Ratio	s)	-	-	169 0.14	461 0.031	-

Intersection						
Int Delay, s/veh	0.8					
		WED	NET	NDD	051	ODT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		14		ሻ	^
Traffic Vol, veh/h	37	34	850	66	12	918
Future Vol, veh/h	37	34	850	66	12	918
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	200	-
Veh in Median Storage	, # 1	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	40	37	924	72	13	998
Major/Minor N	linar1		laior1		Majora	
	Minor1		Major1		Major2	
Conflicting Flow All	1485	498	0	0	996	0
Stage 1	960	-	-	-	-	-
Stage 2	525	-	-	-	-	-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	115	518	-	-	690	-
Stage 1	332	-	-	-	-	-
Stage 2	558	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	113	518	-	-	690	-
Mov Cap-2 Maneuver	236	-	-	-	-	-
Stage 1	332	-	-	-	-	-
Stage 2	547	-	-	-	-	-
-						
A	MD		ND		OB	
Approach	WB		NB		SB	
	400		0		0.1	
HCM Control Delay, s	19.8					
	19.8 C					
HCM Control Delay, s						
HCM Control Delay, s HCM LOS	С	NRT	NBRV	VBLn1	SBI	SRT
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm	С	NBT_		VBLn1	SBL 690	SBT
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h)	С	-	-	319	690	-
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio	С	-	-	319 0.242	690 0.019	-
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)	С	- - -	-	319 0.242 19.8	690 0.019 10.3	- - -
HCM Control Delay, s HCM LOS Minor Lane/Major Mvm Capacity (veh/h) HCM Lane V/C Ratio	C t	-	-	319 0.242	690 0.019	-

Intersection												
Int Delay, s/veh	0.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDI	1100	4	TIDIC	TABL	14	אפא)	14	ODIN
Traffic Vol, veh/h	6	1	7	19	2	8	11	1006	25	10	913	7
Future Vol, veh/h	6	1	7	19	2	8	11	1006	25	10	913	7
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	_	_	-	_	-	-	250	_	-	250	-	-
Veh in Median Storage	.# -	1	_	_	1	_		0	_		0	_
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	67	67	67	60	66	66	92	92	92	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	1	10	32	3	12	12	1093	27	12	1062	8
Major/Minor N	Minor2			Minor1		1	Major1		N	Major2		
Conflicting Flow All	1662	2234	535	1687	2225	560	1070	0	0	1120	0	0
Stage 1	1090	1090	-	1131	1131	-	-	-	-	-	-	-
Stage 2	572	1144	-	556	1094	-	_	-	_	_	_	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	64	42	490	61	43	472	647	-	-	619	-	-
Stage 1	230	289	-	217	277	-	-	-	-	-	-	-
Stage 2	472	273	-	483	288	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	60	40	490	58	41	472	647	-	-	619	-	-
Mov Cap-2 Maneuver	160	141	-	154	143	-	-	-	-	-	-	-
Stage 1	226	284	-	213	272	-	-	-	-	-	_	-
Stage 2	446	268	-	461	283	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	21.6			30.9			0.1			0.1		
HCM LOS	С			D								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		647	-	-		185	619	-				
HCM Lane V/C Ratio		0.018				0.253		<u>-</u>	_			
HCM Control Delay (s)		10.7	_	_		30.9	10.9	_	_			
HCM Lane LOS		В	_	_	C C	D	В	_	<u>-</u>			
HCM 95th %tile Q(veh))	0.1	_	_	0.3	1	0.1	_	_			
riom oour /outo Q(von)		0.1			0.0		V. 1					

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y	WDIX	113	NDIX	SDL 1	↑ ↑
Traffic Vol, veh/h	16	5	1052	25	11	926
Future Vol, veh/h	16	5	1052	25	11	926
Conflicting Peds, #/hr	0	0	0	25	0	920
			Free	Free	Free	Free
Sign Control RT Channelized	Stop -	Stop		None		None
	0	NOHE -	-	INOHE -	200	None -
Storage Length			0		200	0
Veh in Median Storage	0	-	0		-	0
Grade, %				- 71	76	
Peak Hour Factor	89	89	74	74		86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	18	6	1422	34	14	1077
Major/Minor N	Minor1	N	Major1		Major2	
Conflicting Flow All	2006	728	0	0	1456	0
Stage 1	1439	-	-	-	-	_
Stage 2	567	_	-	_	_	_
Critical Hdwy	6.84	6.94	_	_	4.14	_
Critical Hdwy Stg 1	5.84	-	_	<u>-</u>	-	_
Critical Hdwy Stg 2	5.84	_	_	_	_	_
Follow-up Hdwy	3.52	3.32	_	_	2.22	_
Pot Cap-1 Maneuver	52	366	_	_	461	_
Stage 1	185	-	_	_	_	_
Stage 2	531	_	_	_	_	_
Platoon blocked, %	551		_	_		_
Mov Cap-1 Maneuver	50	366			461	_
Mov Cap-1 Maneuver	141	-		_	401	_
Stage 1	185	_	-	_	-	-
•	515		-	-	-	-
Stage 2	313	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	30.4		0		0.2	
HCM LOS	D					
Minor Long /Maior Ma		NDT	MDDV	MDL 4	CDI	CDT
Minor Lane/Major Mvm		NBT		VBLn1	SBL	SBT
Capacity (veh/h)		NBT -	-	165	461	-
Capacity (veh/h) HCM Lane V/C Ratio	nt		-	165 0.143	461 0.031	-
Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)	nt	-	- - -	165 0.143 30.4	461 0.031 13.1	- - -
Capacity (veh/h) HCM Lane V/C Ratio	nt	-	-	165 0.143	461 0.031	-

2026 No-Build Intersection Operations



Intersection												
Int Delay, s/veh	1.9											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4		7	14		7	14	
Traffic Vol, veh/h	6	2	18	34	2	35	9	971	91	26	1047	5
Future Vol, veh/h	6	2	18	34	2	35	9	971	91	26	1047	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	250	-	-	250	-	-
Veh in Median Storage	, # -	1	-	-	1	-	-	0	-	-	0	-
Grade, %	_	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	10	3	30	46	3	47	10	1055	99	29	1163	6
Major/Minor I	Minor2		1	Minor1		1	Major1		N	Major2		
Conflicting Flow All	1773	2398	585	1766	2352	577	1169	0	0	1154	0	0
Stage 1	1224	1224	-	1125	1125	-	-	-	-	-	_	_
Stage 2	549	1174	_	641	1227	_	_	_	_	_	-	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	-	_
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-		_	_	-	-	_
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	_	-	-	-	-	_	_
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	-	_
Pot Cap-1 Maneuver	53	33	454	53	35	460	593	_	-	601	_	_
Stage 1	190	250	-	218	278	-	-	_	_		-	_
Stage 2	488	264	_	430	249	-	-	_	-	_	_	_
Platoon blocked, %								_	_		_	_
Mov Cap-1 Maneuver	44	31	454	46	33	460	593	_	-	601	_	_
Mov Cap-2 Maneuver	133	121	-	143	128	-	-	_	_	-	-	_
Stage 1	187	238	_	214	273	_	-	-	-	_	_	_
Stage 2	426	260	_	377	237	_	_	_	_	_	_	_
	.20	_00		011	_0,							
Approach	EB			WB			NB			SB		
HCM Control Delay, s	21.8			34.6			0.1			0.3		
HCM LOS	C			D			J .,			3.0		
Minor Lane/Major Mvm	nt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		593			257	215	601	-				
HCM Lane V/C Ratio		0.016	-	_		0.446		_	_			
HCM Control Delay (s)		11.2		_	21.8	34.6	11.3	_	_			
HCM Lane LOS		11.2 B	<u>-</u>	<u>-</u>	21.0 C	54.0 D	11.3 B	_				
HCM 95th %tile Q(veh)	\	0.1			0.6	2.1	0.2		_			
HOW JOHN JOHN WINE WINE		0.1	_	-	0.0	Z. I	U.Z	_	_			

Intersection						
Int Delay, s/veh	1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y	VVDIX	1 1>	אטא	ODL 7	**
Traffic Vol, veh/h	41	38	1063	73	13	1137
Future Vol, veh/h	41	38	1063	73	13	1137
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	_	-	200	-
Veh in Median Storage,		_	0	_	-	0
Grade, %	0	_	0	_	_	0
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	45	41	1155	79	14	1236
		• •			• •	
					4 . 0	
	Minor1		Major1		Major2	
Conflicting Flow All	1841	617	0	0	1234	0
Stage 1	1195	-	-	-	-	-
Stage 2	646	<u>-</u>	-	-	-	-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	67	433	-	-	560	-
Stage 1	250	-	-	-	-	-
Stage 2	484	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	65	433	-	-	560	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver	175	433 -		- - -	560 -	
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1	175 250		-	-		-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver	175	-	-	-		-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1	175 250	-	- - -	- -	-	- -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2	175 250 472	-	- - -	- -	- - -	- - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach	175 250 472 WB	-	- - - NB	- -	- - - SB	- - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s	175 250 472 WB 27.4	-	- - -	- -	- - -	- - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach	175 250 472 WB	-	- - - NB	- -	- - - SB	- - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS	175 250 472 WB 27.4 D	-	- - - - NB 0	-	SB 0.1	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt	175 250 472 WB 27.4 D	-	- - - - NB 0	- - - - VBLn1	- - - SB 0.1	- - -
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt Capacity (veh/h)	175 250 472 WB 27.4 D	-	- - - - NB 0	- - - - - VBLn1 245	SB 0.1	-
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio	175 250 472 WB 27.4 D	-	- - - - NB 0	- - - - - - - - - - 245 0.35	SB 0.1 SBL 560 0.025	- - - - SBT
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)	175 250 472 WB 27.4 D	- - - NBT	- - - - NB 0	VBLn1 245 0.35 27.4	SB 0.1 SBL 560 0.025 11.6	- - - - SBT
Mov Cap-1 Maneuver Mov Cap-2 Maneuver Stage 1 Stage 2 Approach HCM Control Delay, s HCM LOS Minor Lane/Major Mvmt Capacity (veh/h) HCM Lane V/C Ratio	175 250 472 WB 27.4 D	NBT	- - - NB 0	- - - - - - - - - - 245 0.35	SB 0.1 SBL 560 0.025	

Verment EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR	Intersection													
The Configurations The Confi	Int Delay, s/veh	1.3												
Iffice Vol. Verbith 6	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Iffice Vol, veh/h	Lane Configurations		4			4		*	4%		7	41,		
ure Vol, veh/h 6 1 8 21 2 9 12 1260 27 11 1147 8 n Control Stop Stop Stop Stop Stop Stop Free	Traffic Vol, veh/h	6		8	21		9			27			8	
nflicting Peds, #/hr 1	Future Vol, veh/h	6	1	8	21	2	9			27	11	1147	8	
n Control	Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Channelized None - None None None rage Length None None None rage Length 250 250	Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
rage Length	RT Channelized				•									
n in Median Storage, # - 1	Storage Length	_	_	-	_	_		250	_		250	_		
ak Hour Factor 67 67 67 67 60 66 66 92 92 92 92 86 86 86 86 ac avy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		# -	1	_	_	1	_		0	_		0	_	
ak Hour Factor 67 67 67 67 60 66 66 92 92 92 92 86 86 86 avy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Grade, %			_	_			_			_		_	
avy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2														
Minor Minor Minor Minor Major Major Major														
Inflicting Flow All 2078 2790 672 2105 2780 700 1343 0 0 1399 0 0 Stage 1 1365 1365 - 1411 1411	VIVIIIL FIOW	9	ı	12	33	3	14	13	1370	29	13	1334	9	
Inflicting Flow All 2078 2790 672 2105 2780 700 1343 0 0 1399 0 0 Stage 1 1365 1365 - 1411 1411	Major/Minor N	Minor?			Minor1		ı	Major1		N	Major?			
Stage 1			2700			2700			0			0	Λ	
Stage 2 713 1425 - 694 1369								1545			1399			
tical Hdwy 7.54 6.54 6.94 7.54 6.54 6.94 7.54 6.54 6.94 4.14 - 4.14 4.14	•						-	_	-	-	-	-	-	
tical Hdwy Stg 1 6.54 5.54 - 6.54 5.54							-	-	-	-	-	-	-	
tical Hdwy Stg 2 6.54 5.54 - 6.54 5.54	•			6.94			6.94	4.14	-	-	4.14	-	-	
Now-up Hdwy				-			-	-	-	-	-	-	-	
Cap-1 Maneuver 31								-	-	-	-	-	-	
Stage 1 155 214 - 145 203 - - - - - - - - - - - - - - - - -	Follow-up Hdwy								-	-		-	-	
Stage 2 389 200 - 399 213 - - - - - - - - - - - - - - - - -	Pot Cap-1 Maneuver			398			382	509	-	-	484	-	-	
toon blocked, % v Cap-1 Maneuver 28 17 398 ~ 27 18 382 509 484 v Cap-2 Maneuver 107 96 - 102 98 Stage 1 151 208 - 141 198 Stage 2 360 195 - 374 207 Oroach EB WB NB SB M Control Delay, s 28.9 52.1 0.1 0.1 M LOS D F Nor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 509 173 126 484 M Lane V/C Ratio 0.026 0.129 0.41 0.026 M Control Delay (s) 12.3 - 28.9 52.1 12.6 M Lane LOS B - D F B M 95th %tile Q(veh) 0.1 - 0.4 1.8 0.1 Ites	Stage 1			-			-	-	-	-	-	-	-	
v Cap-1 Maneuver 28 17 398 ~ 27 18 382 509 - - 484 - - v Cap-2 Maneuver 107 96 - 102 98 - <	Stage 2	389	200	-	399	213	-	-	-	-	-	-	-	
v Cap-2 Maneuver 107 96 - 102 98 -	Platoon blocked, %								-	-		-	-	
Stage 1 151 208 - 141 198 -	Mov Cap-1 Maneuver	28	17	398	~ 27	18	382	509	-	-	484	-	-	
Stage 1 151 208 - 141 198 -	Mov Cap-2 Maneuver	107	96	-	102	98	-	-	-	-	-	-	-	
Stage 2 360 195 - 374 207 -		151	208	-	141	198	-	-	-	-	-	-	-	
NB		360	195	-	374	207	-	-	-	-	-	-	-	
M Control Delay, s 28.9	Ť													
M Control Delay, s 28.9	Approach	EB			WB			NB			SB			
M LOS D F nor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 509 173 126 484 M Lane V/C Ratio 0.026 0.129 0.41 0.026 M Control Delay (s) 12.3 - 28.9 52.1 12.6 M Lane LOS B - D F B M 95th %tile Q(veh) 0.1 - 0.4 1.8 0.1														
nor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 509 - - 173 126 484 - - M Lane V/C Ratio 0.026 - - 0.129 0.41 0.026 - - M Control Delay (s) 12.3 - - 28.9 52.1 12.6 - - M Lane LOS B - - D F B - - M 95th %tile Q(veh) 0.1 - - 0.4 1.8 0.1 - -	HCM LOS							J. 1			J. 1			
pacity (veh/h) 509 173 126 484 M Lane V/C Ratio 0.026 0.129 0.41 0.026 M Control Delay (s) 12.3 28.9 52.1 12.6 M Lane LOS B D F B M 95th %tile Q(veh) 0.1 0.4 1.8 0.1 M tes	TIOW EOO													
pacity (veh/h) 509 173 126 484 M Lane V/C Ratio 0.026 0.129 0.41 0.026 M Control Delay (s) 12.3 28.9 52.1 12.6 M Lane LOS B D F B M 95th %tile Q(veh) 0.1 0.4 1.8 0.1	Minor Lane/Major Mum	t	NRI	NRT	MRD	=RL n 1\/	VRI n1	SBI	SRT	SBD				
M Lane V/C Ratio 0.026 0.129 0.41 0.026 M Control Delay (s) 12.3 28.9 52.1 12.6 M Lane LOS B D F B M 95th %tile Q(veh) 0.1 0.4 1.8 0.1				NDT	NDIX I				ODT	JDI				
M Control Delay (s) 12.3 28.9 52.1 12.6 M Lane LOS B D F B M 95th %tile Q(veh) 0.1 0.4 1.8 0.1				-	-				-	-				
M Lane LOS B D F B M 95th %tile Q(veh) 0.1 0.4 1.8 0.1 tes				-	-									
M 95th %tile Q(veh) 0.1 0.4 1.8 0.1 tes				-	-				-	-				
tes	HCM Lane LOS			_	-					-				
	HCM 95th %tile Q(veh)		0.1	-	-	0.4	1.8	0.1	-	-				
	Notes													
Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon	~: Volume exceeds cap	acity	\$: De	elay exc	eeds 3	00s	+: Com	putation	Not D	efined	*: All	major v	volume i	in platoon

Intersection						
Int Delay, s/veh	0.5					
		WDD	NDT	NDD	007	ODT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		14		ሻ	^
Traffic Vol, veh/h	18	6	1332	28	12	1181
Future Vol, veh/h	18	6	1332	28	12	1181
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	200	-
Veh in Median Storage	e, # 1	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	89	89	74	74	76	86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	20	7	1800	38	16	1373
NA - ' /NA'	N 4° 4		1.1.1		4-10	
	Minor1		Major1		Major2	
Conflicting Flow All	2538	919	0	0	1838	0
Stage 1	1819	-	-	-	-	-
Stage 2	719	-	-	-	-	-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	22	273	-	-	327	-
Stage 1	114	-	-	-	-	-
Stage 2	444	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	21	273	-	-	327	-
Mov Cap-2 Maneuver	88		-	-		-
Stage 1	114	-	_	_	_	_
Stage 2	422	_	_	_	_	_
Clayo Z	144					
Approach	WB		NB		SB	
HCM Control Delay, s	50.2		0		0.2	
HCM LOS	F					
Minor Long/Major Mare	\ 1	NBT	MDDW	MDI -1	CDI	SBT
Minor Lane/Major Mvm	IL			VBLn1	SBL	
Capacity (veh/h)		-	-		327	-
HCM Lane V/C Ratio		-	-	0.254		-
HCM Control Delay (s)		-	-	50.2	16.6	-
HCM Lane LOS		-	-	F	С	-
HCM 95th %tile Q(veh)	-	-	0.9	0.2	-

2026 No-Build Intersection Operations with System Improvements



Intersection												
Int Delay, s/veh	1.6											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		7	B		-	*	7	7	14	
Traffic Vol, veh/h	6	2	18	34	2	35	9	971	91	26	1047	5
Future Vol, veh/h	6	2	18	34	2	35	9	971	91	26	1047	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	_	-	None	-	-	None	-	-	None
Storage Length	-	-	-	0	-	-	250	-	150	250	-	-
Veh in Median Storage	,# -	1	-	-	1	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	10	3	30	46	3	47	10	1055	99	29	1163	6
Major/Minor N	Minor2		ı	Minor1			Major1		<u> </u>	Major2		
Conflicting Flow All	1773	2398	585	1716	2302	528	1169	0	0	1154	0	0
Stage 1	1224	1224	-	1075	1075	-	-	-	-	-	_	-
Stage 2	549	1174	_	641	1227	_	-	_	_	_	_	_
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	-	_
Critical Hdwy Stg 1	6.54	5.54	_	6.54	5.54	_	-	-	-	_	-	-
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	-	_	-	-	-	_	_
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	53	33	454	58	38	495	593	-	-	601	_	_
Stage 1	190	250	-	234	294	-	-	-	-	-	-	-
Stage 2	488	264	-	430	249	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	45	31	454	51	36	495	593	-	-	601	-	-
Mov Cap-2 Maneuver	134	121	-	151	132	-	-	-	-	-	-	-
Stage 1	187	238	-	230	289	-	-	-	-	-	-	-
Stage 2	430	260	_	377	237	-	-	-	_	-	-	-
, and the second												
Approach	EB			WB			NB			SB		
HCM Control Delay, s	21.7			26.1			0.1			0.3		
HCM LOS	С			D								
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1V	VBLn1V	VBLn2	SBL	SBT	SBR		
Capacity (veh/h)		593	-		258	151	431	601	-	-		
HCM Lane V/C Ratio		0.016	<u> </u>	_		0.304			<u>-</u>	_		
HCM Control Delay (s)		11.2	_	_	21.7	38.9	14.4	11.3	_	_		
HCM Lane LOS		В	<u> </u>	<u>-</u>	C C	50.5 E	В	В	<u>-</u>	_		
HCM 95th %tile Q(veh)		0.1	_	_	0.6	1.2	0.4	0.2	_	_		
		J. 1			3.5	1.4	J. 1	J.L				

Intersection							J
Int Delay, s/veh	0.8						
Movement	WBL	WBR	NBT	NBR	SBL	SBT	Į
Lane Configurations	T	₩ P	^	TADIX	JDL 7	↑ ↑	
Traffic Vol, veh/h	41	38	1063	73	13	1137	
Future Vol, veh/h	41	38	1063	73	13	1137	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	- Otop	None	-	None	-	None	
Storage Length	0	0	_	150	200	-	
Veh in Median Storage		-	0	-	200	0	
Grade, %	0	_	0	_	_	0	
Peak Hour Factor	92	92	92	92	92	92	
	2	2	2	2	2	2	
Heavy Vehicles, %							
Mvmt Flow	45	41	1155	79	14	1236	
Major/Minor	Minor1	N	Major1	١	Major2		
Conflicting Flow All	1801	578	0	0	1234	0	
Stage 1	1155	-	_	-	-	-	
Stage 2	646	_	-	_	_	_	
Critical Hdwy	6.84	6.94	_	_	4.14	_	
Critical Hdwy Stg 1	5.84	-	_	_		_	
Critical Hdwy Stg 2	5.84	_	_	_	_	_	
Follow-up Hdwy	3.52	3.32	_	_	2.22	_	
Pot Cap-1 Maneuver	71	459	_	_	560	_	
Stage 1	262	-	_	_	-	_	
Stage 2	484	_	_	_	_	_	
Platoon blocked, %	707		_	_		_	
Mov Cap-1 Maneuver	69	459	_	_	560	_	
	182						
Mov Cap-2 Maneuver	262	-	-	-	-	-	
Stage 1		-	-	=	-	-	
Stage 2	472	-	-	-	-	-	
Approach	WB		NB		SB		
HCM Control Delay, s	22.7		0		0.1		
HCM LOS	С						
= 0.0	J						
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1W	VBLn2	SBL	
Capacity (veh/h)		_	_	182	459	560	
HCM Lane V/C Ratio		_	_	0.245		0.025	
HCM Control Delay (s)				31.1	13.6	11.6	
HCM Lane LOS		_	_	D D	13.0 B	В	
HCM 95th %tile Q(veh	١	_	_	0.9	0.3	0.1	
HOW SOUT /OUIE W(VEI)	1	_	-	0.5	0.5	0.1	

Intersection													
Int Delay, s/veh	1.1												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		4		7	1		*	^	7	7	1	<u> </u>	
Traffic Vol, veh/h	6	1	8	21	2	9	12	1260	27	11	1147	8	
Future Vol, veh/h	6	1	8	21	2	9	12	1260	27	11	1147	8	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	Stop -	Stop -	None	Stop -	- -	None	-	-	None	-	-	None	
Storage Length	_	-	NOITE	0	_	INUITE	250	-	150	250	_	NONE	
Storage Lerigtii Veh in Median Storage		- 1	_		1			0	150	250	0		
		1 0		-	0		-	0			0	-	
Grade, %	- 67		67	-		-	-		-	- 00	86	- 06	
Peak Hour Factor	67	67	67	60	66	66	92	92	92	86		86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	9	1	12	35	3	14	13	1370	29	13	1334	9	
Major/Minor	Minor2		ı	Minor1		ľ	Major1		N	//ajor2			
Conflicting Flow All	2078	2790	672	2090	2765	685	1343	0	0	1399	0	0	
Stage 1	1365	1365	-	1396	1396	-	-	-	-	-	-	-	
Stage 2	713	1425	_	694	1369	_	_	_	_	_	_	_	
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	_	_	4.14	-	-	
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	_	_	_	_	_	_	
Critical Hdwy Stg 2	6.54	5.54	_	6.54	5.54	_	_	_	_	_	_	_	
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	_	_	
Pot Cap-1 Maneuver	31	18	398	~ 30	19	391	509	_	_	484	_	_	
Stage 1	155	214	-	148	206	-	-	_	_	-10-1	_	_	
Stage 2	389	200	_	399	213	_	_	_	_	_	_	_	
Platoon blocked, %	303	200		333	210			_	_		_	_	
Mov Cap-1 Maneuver	28	17	398	~ 28	18	391	509	_	_	484	_	-	
Mov Cap-1 Maneuver		96	390	104	98	391	309	-	_	404	-	-	
	151	208	_	144	201	<u>-</u>	_	_	-	-	_	-	
Stage 1			-			-	-	-	-	-	-	-	
Stage 2	360	195	-	374	207	-	-	-	-	-	-	-	
Approach	EB			WB			NB			SB			
HCM Control Delay, s	28.9			44.6			0.1			0.1			
HCM LOS	D			Е									
Minor Lane/Major Mvn	nt	NBL	NBT	NRRI	-RI n1\	WBLn1V	VRI n2	SBL	SBT	SBR			
	iit.		INDT	ואטוז					ומט	אומט			
Capacity (veh/h)		509	-	-	173	104	253	484	-	-			
HCM Caratas Dalay (\	0.026	-					0.026	-	-			
HCM Control Delay (s)	12.3	-	-	28.9	56.2	20.2	12.6	-	-			
HCM Lane LOS	,	В	-	-	D	F	С	В	-	-			
HCM 95th %tile Q(veh	1)	0.1	-	-	0.4	1.3	0.2	0.1	-	-			
Notes													
~: Volume exceeds ca	pacity	\$: De	elav exc	eeds 3	00s	+: Com	putation	Not D	efined	*: All	maior v	/olume i	in platoon
	.paoity	ψ. Δ	, one	.5040 0		. 50111	Patation		J5u	. 7 111	ajor (3.47110 1	platoon

Intersection						
Int Delay, s/veh	0.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	T	₹ T	^	TVDIX	JDL 1	^
Traffic Vol, veh/h	18	6	1332	28	12	1181
Future Vol, veh/h	18	6	1332	28	12	1181
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	Stop -	None	-		-	None
Storage Length	0	0	-	150	200	None -
		-	0	100	200	0
Veh in Median Storage Grade, %	0	-	0			0
· · · · · · · · · · · · · · · · · · ·			74	- 71	- 76	
Peak Hour Factor	89	89		74	76	86
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	20	7	1800	38	16	1373
Major/Minor N	Minor1	N	Major1	ľ	Major2	
Conflicting Flow All	2519	900	0	0	1838	0
Stage 1	1800	_	_	-	-	-
Stage 2	719	_	-	_	_	_
Critical Hdwy	6.84	6.94	_	_	4.14	_
Critical Hdwy Stg 1	5.84	-	_	<u>-</u>	-	_
Critical Hdwy Stg 2	5.84	_	_	_	_	_
Follow-up Hdwy	3.52	3.32	_	_	2.22	_
Pot Cap-1 Maneuver	23	282	_	_	327	_
Stage 1	117		_	_	-	_
Stage 2	444	_	_	_	_	_
Platoon blocked, %	-1-1-1		_	_		_
Mov Cap-1 Maneuver	22	282		_	327	_
Mov Cap-1 Maneuver	90	- 202	_	_	321	_
	117		-	_	-	-
Stage 1	422	-	-	-	-	-
Stage 2	422	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	46.7		0		0.2	
HCM LOS	Ε					
Minor Lane/Major Mvm	.+	NBT	NDDV	VBLn1V	VDI n2	SBL
	ıı					
Capacity (veh/h)		-	-	50	282	327
HCM Cartral Palace (a)		-	-	0.225		
HCM Control Delay (s)		-	-	56.2	18.1	16.6
HCM Lane LOS		-	-	F	C	С
HCM 95th %tile Q(veh)		-	-	8.0	0.1	0.2

FUTURE CONDITION INTERSECTION OPERATIONS



Intersection													
Int Delay, s/veh	4												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		4			4		*	44		7	17>		
Traffic Vol, veh/h	27	2	63	34	2	35	24	971	91	26	1047	13	
Future Vol, veh/h	27	2	63	34	2	35	24	971	91	26	1047	13	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	-	250	-	-	250	-	-	
Veh in Median Storage	,# -	1	-	-	1	-	-	0	-	-	0	_	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	44	3	103	46	3	47	26	1055	99	29	1163	14	
Major/Minor N	Minor2		ľ	Minor1			Major1		N	Major2			
Conflicting Flow All	1809	2434	589	1798	2392	577	1177	0	0	1154	0	0	
Stage 1	1228	1228	-	1157	1157	-	-	-	-	-	_	-	
Stage 2	581	1206	_	641	1235	-	-	_	_	_	-	_	
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	_	-	4.14	_	_	
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	-	_	_	_	-	_	
Critical Hdwy Stg 2	6.54	5.54	_	6.54	5.54	_	-	_	-	_	_	_	
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	-	_	
Pot Cap-1 Maneuver	49	31	452	50	33	460	589	_	-	601	_	_	
Stage 1	189	249	_	209	269	-	-	_	_	_	-	_	
Stage 2	467	255	-	430	247	-	-	-	-	-	_	-	
Platoon blocked, %								-	-		-	-	
Mov Cap-1 Maneuver	~ 40	28	452	~ 35	30	460	589	-	-	601	-	-	
Mov Cap-2 Maneuver	126	116	-	123	119	-	-	-	-	-	-	-	
Stage 1	181	237	-	200	257	-	-	-	-	-	-	-	
Stage 2	396	244	-	311	235	-	-	-	-	-	-	-	
, and the second													
Approach	EB			WB			NB			SB			
HCM Control Delay, s	39.7			41.1			0.3			0.3			
HCM LOS	Е			Е									
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR				
Capacity (veh/h)		589	-	-	248	192	601	-	_				
HCM Lane V/C Ratio		0.044	-	-	0.608		0.048	-	-				
HCM Control Delay (s)		11.4	-	-	39.7	41.1	11.3	-	-				
HCM Lane LOS		В	-	-	Е	Е	В	-	-				
HCM 95th %tile Q(veh)		0.1	-	-	3.6	2.5	0.2	-	-				
Notes													
~: Volume exceeds cap	acity	\$: De	elay exc	eeds 3	00s	+: Com	putation	Not D	efined	*: All	maior	volume	in platoon
2.2		,. . ,	, 					,.				, .	p. 18.18.1.

Intersection						
Int Delay, s/veh	1					
	MDI	WED	NDT	NDD	ODI	ODT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		14		7	^
Traffic Vol, veh/h	41	38	1078	73	13	1137
Future Vol, veh/h	41	38	1078	73	13	1137
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	200	-
Veh in Median Storage		-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	45	41	1172	79	14	1236
Major/Minor	\ Aire = =4		10:001		Asis =0	
	Minor1		Major1		Major2	
Conflicting Flow All	1858	626	0	0	1251	0
Stage 1	1212	-	-	-	-	-
Stage 2	646	-	-	-		-
Critical Hdwy	6.84	6.94	-	-	4.14	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.52	3.32	-	-	2.22	-
Pot Cap-1 Maneuver	65	427	-	-	552	-
Stage 1	244	-	-	-	-	-
Stage 2	484	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	63	427	-	-	552	-
Mov Cap-2 Maneuver	172	-	-	-	-	-
Stage 1	244	-	-	-	-	-
Stage 2	472	-	_	_	-	-
						
Annragah	MD		ND		CD	
Approach	WB		NB		SB	
HCM Control Delay, s	28		0		0.1	
HCM LOS	D					
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)			-		552	-
HCM Lane V/C Ratio				0.356		_
HOW LAND V/O NAID				28	11.7	_
HCM Control Delay (s)		_				
HCM Lane LOS		_				
HCM Control Delay (s) HCM Lane LOS HCM 95th %tile Q(veh)		-	-	D 1.5	B 0.1	-

Delay, s/veh 3
Configurations ## ## ## ## ## ## ## ## ## ## ## ##
ffic Vol, veh/h
ffic Vol, veh/h
Stage 1 1379 1379
Control Stop Stop Stop Stop Stop Stop Stop Stop Stop Free Free
Control Stop Stop Stop Stop Stop Stop Stop Stop Stop Free Free
Channelized None None None None None rage Length
n in Median Storage, # - 1
n in Median Storage, # - 1
Add Add
Ak Hour Factor 67 67 67 67 60 66 66 92 92 92 92 86 86 86 86 86 86 86 86 86 86 86 86 86
avy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Minor Minor Minor Minor Major Majo
Minor Minor Minor Minor Major Major Major
Afficiting Flow All 2202 2914 686 2215 2919 700 1372 0 0 1399 0 0 0 Stage 1 1379 1379 - 1521 1521
Afficiting Flow All 2202 2914 686 2215 2919 700 1372 0 0 1399 0 0 0 Stage 1 1379 1379 - 1521 1521
Stage 1 1379 1379 - 1521 1521 -
Stage 2 823 1535 - 694 1398
ical Hdwy 7.54 6.54 6.94 7.54 6.54 6.94 4.14 - 4.14 - 5 ical Hdwy Stg 1 6.54 5.54 - 6.54 5.54 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 -
ical Hdwy Stg 1 6.54 5.54 - 6.54 5.54
ical Hdwy Stg 2 6.54 5.54 - 6.54 5.54
Now-up Hdwy
Cap-1 Maneuver ~ 25
Stage 1 152 210 - 124 179 -
Stage 2 334 176 - 399 206 -
toon blocked, % v Cap-1 Maneuver ~ 20 13 390 ~ 18 13 382 496 484 v Cap-2 Maneuver 87 81 - 76 71 Stage 1 131 204 - 107 154 Stage 2 272 152 - 329 200 oroach EB WB NB SB M Control Delay, s 45.2 79.6 0.6 0.1 M LOS E F or Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 496 174 96 484
v Cap-1 Maneuver ~ 20 13 390 ~ 18 13 382 496 484 v Cap-2 Maneuver 87 81 - 76 71
v Cap-2 Maneuver 87 81 - 76 71 -
Stage 1 131 204 - 107 154 -
Stage 2 272 152 - 329 200 -
broach EB WB NB SB M Control Delay, s 45.2 79.6 0.6 0.1 M LOS E F For Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Dacity (veh/h) 496 - - 174 96 484 - -
M Control Delay, s 45.2 79.6 0.6 0.1 M LOS E F or Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 496 174 96 484
M Control Delay, s 45.2 79.6 0.6 0.1 M LOS E F or Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 496 174 96 484
M Control Delay, s 45.2 79.6 0.6 0.1 M LOS E F or Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 496 174 96 484
M LOS E F or Lane/Major Mvmt
or Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR pacity (veh/h) 496 174 96 484
pacity (veh/h) 496 174 96 484
pacity (veh/h) 496 174 96 484
WLANE V/∪ KANO U.138 U.5U0 U.538 U.UZ6
M Control Delay (s) 13.4 45.2 79.6 12.6
M Lane LOS B E F B
M 95th %tile Q(veh) 0.5 2.5 2.4 0.1
es
/olume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

Intersection								
Int Delay, s/veh	0.5							
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	Y	וטייי	14	וטוז	JDL 1	↑ ↑		
Traffic Vol, veh/h	18	6	1383	28	12	1211		
uture Vol, veh/h	18	6	1383	28	12	1211		
conflicting Peds, #/hr		0	0	0	0	0		
Sign Control	Stop	Stop	Free	Free	Free	Free		
RT Channelized	- Clop	None	-		-			
Storage Length	0	-	_	-	200	-		
eh in Median Storag		_	0	_	-	0		
Grade, %	0	_	0	_	_	0		
Peak Hour Factor	89	89	74	74	76	86		
Heavy Vehicles, %	2	2	2	2	2	2		
Nymt Flow	20	7	1869	38	16	1408		
Acior/Minor	Minart		lois=1		/aicr0			
	Minor1		Major1		Major2	^		
Conflicting Flow All	2624	954	0	0	1907	0		
Stage 1	1888	-	-	-	-	-		
Stage 2	736 6.84	6.94	-	-	4.14	-		
itical Hdwy	5.84		-	-	4.14	-		
ritical Hdwy Stg 1	5.84	-	-	-	-	-		
ritical Hdwy Stg 2 ollow-up Hdwy	3.52	3.32	_	-	2.22	=		
ot Cap-1 Maneuver	~ 19	259	-	-	308			
Stage 1	105	209	_	_	300	_		
Stage 2	435		-	-	_			
latoon blocked, %	400	_	_	_	_	_		
lov Cap-1 Maneuver	~ 18	259	-		308			
lov Cap-1 Maneuver lov Cap-2 Maneuver		209	_	_	300	_		
Stage 1	105	_		_	_	_		
Stage 2	412	<u>-</u>	_	_	_	_		
Clago Z	TIL							
www.aab	MD		ND		OD.			
pproach	WB		NB		SB			
HCM Control Delay, s			0		0.2			
ICM LOS	F							
linor Lane/Major Mvr	mt	NBT	NBRV	VBLn1	SBL	SBT		
apacity (veh/h)		-	-	98	308	-		
CM Lane V/C Ratio		-	-	0.275		-		
CM Control Delay (s	s)	-	-	••••	17.3	-		
CM Lane LOS		-	-	F	С	-		
HCM 95th %tile Q(veh	n)	-	-	1	0.2	-		
lotes								
: Volume exceeds ca	apacity	\$∙ De	lav evo	ceeds 3	00s	+. Com	outation Not Defined	*: All major volume in platoon
V Gluffic CACCCUS Co	apaoity	ψ. De	nay ext	occus o	000		odtation Not Delined	. 7 (ii iliajoi volulile ili piatooli

FUTURE CONDITION INTERSECTION OPERATIONS WITH IMPROVEMENTS



Intersection														
Int Delay, s/veh	2.9													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations	7	B		1	B		*	*	7	7	14			
Traffic Vol, veh/h	27	2	63	34	2	35	24	971	91	26	1047	13		
Future Vol, veh/h	27	2	63	34	2	35	24	971	91	26	1047	13		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None		
Storage Length	0	-	-	0	-	-	250	-	150	250	-	-		
Veh in Median Storage	,# -	1	-	-	1	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	61	61	61	74	74	74	92	92	92	90	90	90		
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2		
Mvmt Flow	44	3	103	46	3	47	26	1055	99	29	1163	14		
Major/Minor N	Minor2		ľ	Minor1			Major1		1	Major2				
Conflicting Flow All	1809	2434	589	1748	2342	528	1177	0	0	1154	0	0		
Stage 1	1228	1228	-	1107	1107	-	-	-	-	-	-	-		
Stage 2	581	1206	_	641	1235	_	_	_	_	_	_	_		
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	_	_	4.14	_	_		
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	-	_	_	-	_	_		
Critical Hdwy Stg 2	6.54	5.54	_	6.54	5.54	-	-	-	-	-	-	-		
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	_	_	2.22	_	_		
Pot Cap-1 Maneuver	49	31	452	55	36	495	589	-	_	601	_	-		
Stage 1	189	249	_	224	284	-	-	_	_	-	-	_		
Stage 2	467	255	-	430	247	-	-	-	-	-	-	-		
Platoon blocked, %								_	-		-	-		
Mov Cap-1 Maneuver	~ 41	28	452	~ 39	33	495	589	-	-	601	-	-		
Mov Cap-2 Maneuver	127	116	-	129	123	-	-	-	-	-	-	-		
Stage 1	181	237	-	214	272	-	-	-	-	-	-	-		
Stage 2	400	244	-	311	235	-	-	-	-	-	-	-		
Ü														
Approach	EB			WB			NB			SB				
HCM Control Delay, s	25.8			30.4			0.3			0.3				
HCM LOS	D			D										
Minor Lane/Major Mvm	t	NBL	NBT	NBR	EBLn1	EBLn2V	VBLn1\	VBLn2	SBL	SBT	SBR			
Capacity (veh/h)		589	-	_	127	415	129	425	601	-	_			
HCM Lane V/C Ratio		0.044	_	_				0.118		_	_			
HCM Control Delay (s)		11.4	_	_	47.8	16.6	47.6	14.6	11.3	_	_			
HCM Lane LOS		В	_	_	E	C	E	В	В	_	_			
HCM 95th %tile Q(veh)		0.1	-	-	1.4	1	1.5	0.4	0.2	-	-			
Notes														
~: Volume exceeds cap	acity	\$: D4	elay exc	eeds 3	00s	+. Com	putatio	n Not D	efined	*· All	maiory	volume	in platoon	
. Volumo oxocous cap	Jaonty	ψ. υ	July ONG	.50000		. 0011	Patatio		Jiii lou	. <i>T</i> WI	major	· Jiairii	piatoon	

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	T	₹	^	TVDIX	ODL 1	↑ ↑
Traffic Vol, veh/h	41	38	1078	73	13	1137
Future Vol, veh/h	41	38	1078	73	13	1137
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	Stop -	None	-		-	None
Storage Length	0	0	-	150	200	None -
					200	
Veh in Median Storage	,	-	0	-		0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	45	41	1172	79	14	1236
Major/Minor I	Minor1	N	Major1	1	Major2	
Conflicting Flow All	1818	586	0	0	1251	0
Stage 1	1172	-	-	_	-	-
Stage 2	646	_	_	_	_	_
Critical Hdwy	6.84	6.94	_	_	4.14	_
Critical Hdwy Stg 1	5.84	- 0.3		_	7.17	_
Critical Hdwy Stg 1	5.84	_	-		_	_
Follow-up Hdwy	3.52	3.32	_	_	2.22	_
Pot Cap-1 Maneuver	69	454	-	_	552	_
•	257	404	_	_	332	_
Stage 1	484		-	-	-	
Stage 2	404	-	-	-	-	-
Platoon blocked, %	07	454	-	-	FF0	-
Mov Cap-1 Maneuver	67	454	-	-	552	-
Mov Cap-2 Maneuver	179	-	-	-	-	-
Stage 1	257	-	-	-	-	-
Stage 2	472	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	23		0		0.1	
HCM LOS	23 C		U		0.1	
HCIVI LOS	U					
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1V	VBLn2	SBL
Capacity (veh/h)		-	_	179	454	552
HCM Lane V/C Ratio		_	_	0.249		
HCM Control Delay (s)		_	-	31.7	13.7	11.7
HCM Lane LOS		_	_	D	В	В
HCM 95th %tile Q(veh))	-	_	0.9	0.3	0.1
	1			0.0	3.0	V. 1

Intersection														
Int Delay, s/veh	2.5													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations	1	B		*	B		*	*	7	7	14			
Traffic Vol, veh/h	20	1	38	21	2	9	63	1260	27	11	1147	33		
Future Vol, veh/h	20	1	38	21	2	9	63	1260	27	11	1147	33		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None		
Storage Length	0	-	-	0	-	-	250	-	150	250	-	-		
Veh in Median Storage	,# -	1	-	-	1	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	67	67	67	60	66	66	92	92	92	86	86	86		
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2		
Mvmt Flow	30	1	57	35	3	14	68	1370	29	13	1334	38		
Major/Minor N	Minor2		<u> </u>	Minor1			Major1			Major2				
Conflicting Flow All	2202	2914	686	2200	2904	685	1372	0	0	1399	0	0		
Stage 1	1379	1379	-	1506	1506	_	-	-	-	-	-	-		
Stage 2	823	1535	-	694	1398	-	-	-	-	-	-	-		
Critical Hdwy	7.54	6.54	6.94	7.54	6.54	6.94	4.14	-	-	4.14	_	-		
Critical Hdwy Stg 1	6.54	5.54	-	6.54	5.54	-	-	-	-	-	-	-		
Critical Hdwy Stg 2	6.54	5.54	-	6.54	5.54	-	-	-	-	-	-	-		
Follow-up Hdwy	3.52	4.02	3.32	3.52	4.02	3.32	2.22	-	-	2.22	-	-		
Pot Cap-1 Maneuver	~ 25	15	390	~ 25	15	391	496	-	-	484	-	-		
Stage 1	152	210	-	127	182	-	-	-	-	-	-	-		
Stage 2	334	176	-	399	206	-	-	-	-	-	-	-		
Platoon blocked, %								-	-		-	-		
Mov Cap-1 Maneuver	~ 21	13	390	~ 18	13	391	496	-	-	484	-	-		
Mov Cap-2 Maneuver	88	81	-	77	71	-	-	-	-	-	-	-		
Stage 1	131	204	-	110	157	-	-	-	-	-	-	-		
Stage 2	273	152	-	329	200	-	-	-	-	-	-	-		
Approach	EB			WB			NB			SB				
HCM Control Delay, s	33.5			65.7			0.6			0.1				
HCM LOS	D			F										
Minor Lane/Major Mvm	t	NBL	NBT	NBR I	EBL _{n1}	EBLn2V	VBLn1\	VBLn2	SBL	SBT	SBR			
Capacity (veh/h)		496	-	-	88	355	77	215	484	-	-			
HCM Lane V/C Ratio		0.138	-	-	0.339	0.164	0.455	0.078	0.026	-	-			
HCM Control Delay (s)		13.4	-	-	65.6	17.1	86	23.1	12.6	-	-			
HCM Lane LOS		В	-	-	F	С	F	С	В	-	-			
HCM 95th %tile Q(veh)		0.5	-	-	1.3	0.6	1.8	0.2	0.1	-	-			
Notes														
~: Volume exceeds car	pacity	\$: De	elay exc	eeds 3	00s	+: Com	putatio	n Not D	efined	*: All	maior	volume	in platoon	
		,. . ,	, <i></i>				1	,,,					p. 10.112.11	

Intersection								
nt Delay, s/veh	0.5							
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	7	7	^	7	7	*		
Traffic Vol, veh/h	18	6	1383	28	12	1211		
uture Vol, veh/h	18	6	1383	28	12	1211		
Conflicting Peds, #/hr	0	0	0	0	0	0		
Sign Control	Stop	Stop	Free	Free	Free	Free		
T Channelized	-	None	-	None	-	None		
Storage Length	0	0	-	150	200	-		
eh in Median Storag	e,# 1	-	0	-	-	0		
Grade, %	0	-	0	-	-	0		
Peak Hour Factor	89	89	74	74	76	86		
leavy Vehicles, %	2	2	2	2	2	2		
1vmt Flow	20	7	1869	38	16	1408		
/ajor/Minor	Minor1	N	//ajor1	N	//ajor2			
Conflicting Flow All	2605	935	0	0	1907	0		
Stage 1	1869	-	-	-	-	-		
Stage 2	736	_	_	_	_	_		
critical Hdwy	6.84	6.94	_	_	4.14	_		
ritical Hdwy Stg 1	5.84	-	_	_	-	_		
ritical Hdwy Stg 2	5.84	-	_	_	_	-		
follow-up Hdwy	3.52	3.32	_	_	2.22	_		
of Cap-1 Maneuver	~ 20	267	_	_	308	_		
Stage 1	107	-	_	_	-	_		
Stage 2	435	_	_	_	_	_		
Platoon blocked, %	-100		_	_		_		
Nov Cap-1 Maneuver	~ 19	267	_	_	308	-		
Mov Cap-1 Maneuver		- 201	_	_	-	_		
Stage 1	107	_	_	-	_	-		
Stage 2	412	_	_	_	_	_		
Olugo Z	-T 1 Z							
Approach	WB		NB		SB			
HCM Control Delay, s	51.1		0		0.2			
HCM LOS	51.1 F		- 0		0.2			
IOWI LOO	' 							
Minor Lane/Major Mvr	nt	NBT	NBRV	VBLn1V	VBLn2	SBL	SBT	
Capacity (veh/h)				83	267	308	-	
HCM Lane V/C Ratio		<u>-</u>		0.244			-	
HCM Control Delay (s)	<u>-</u>	_	61.8	18.8	17.3	-	
ICM Control Delay (s ICM Lane LOS)	<u>-</u>	_	61.6 F	10.0	17.3	<u>-</u>	
ICM 95th %tile Q(veh	1)	<u>-</u>	_	0.9	0.1	0.2	-	
·	'/			0.9	0.1	U.Z		
lotes								
: Volume exceeds ca	pacity	\$: De	lay exc	eeds 30)0s	+: Com	outation Not Defined	*: All major volume in platoon

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"Civil & Construction Engineering Services"

MEMORANDUM

TO: Ms. Alexandra Reynolds, PE

FROM: Steven J. Cassell, PE

DATE: June 17, 2022

SUBJECT: Wrenfield at Chanticleer Neighborhood Traffic Engineering Study Addendum

The purpose of this memorandum is to provide an addendum to the Wrenfield at Chanticleer Neighborhood Traffic Engineering Study dated June 17, 2022 based on a request from North Augusta staff with regard to existing sight distance at the intersection of Southwood Drive and Martintown Road.

To that end, a field visit was made to the intersection on June 15, 2022 and it was observed that existing vegetation on both sides of the intersection was obscuring the clear line of sight for exiting traffic. Photographs taken are provide as attached figures.

Based on rough field measurements, existing sight distances exiting Southwood Drive were approximately 450-feet to the left (north) and 550-feet to the right (south).

Recommended sight distances were determined using the methodology in *Section 4.4 – Intersection Sight Distance* for "Case B – Intersections with Stop-Control on the Minor Road", required intersection sight-distances were calculated. Sight distances were calculated for all three potential movements at the intersection:

- Case B1 Left-Turn from Minor Road
- Case B2 Right-Turn from Minor Road
- Case B3 Crossing from Minor Road

The following formula was used to calculate the recommended sight distance for each Case:

 $ISD = 1.47 \times V_{major} \times t_g$

Where:

ISD = length of sight line along major road

 $V_{\text{major}} = \text{Speed limit along major road (mph)}$

 $T_g = gap$ acceptance for entering major road (seconds)



For each Case, sight distance was calculated for passenger cars and single unit trucks and are shown below.

Case B1 – Left-Turn from the Minor Road

For a two-lane road, the time gap is 7.5 seconds for passenger cars and 9.5 seconds for single-unit trucks to perform left-turns.

For a multi-lane roads, like Martintown Road, the methodology recommends adding 0.5 seconds and 0.7 seconds for each additional lane required to cross for passenger cars and single-unit trucks, respectively.

For left-turns, vehicles would have to cross one additional through lane and the center left-turn lane (2 lanes). Therefore, the time gap was increased by 1.0 second for passenger cars and 1.4 seconds for single-unit trucks. Table 1 presents a summary of the recommended sight distances for left-turns.

Table 1 Recommended Sight-Distance for Left-turns								
	Base Time gap (s)	Time Gap Adjustment (2 add'l lanes)	Calculated Left- turn minimum Sight Distance	Left-turn minimum				
Passenger Car	6.5	1.0	499.8	500				
Single Unit	8.5	1.4	640.92	645				

As shown by the results in Table 1, existing sight distance is below the calculated recommended sight distance for left-turns at the intersection.

Case B2 - Right-Turn from the Minor Road

The time gap for right-turns is 6.5 seconds for passenger cars and 8.5 seconds for single-unit trucks, irrespective of the width of the main road. Table 2 presents a summary of the recommended sight distances for right-turns.

Table 2 Recommended Sight-Distance for Right-turns							
	Time gap (s)	Calculated Left- turn minimum Sight Distance	Right-turn minimum				
Passenger Car	6.5	382.2	385				
Single Unit	8.5	499.8	500				



As shown by the results in Table 1, existing sight distance is sufficient for passenger cars to below the calculated recommended sight distance for single-unit trucks to perform right-turns at the intersection.

Case B3 - Crossing Maneuvers from the Minor Road

For a two-lane road, the time gap is 6.5 seconds for passenger cars and 8.5 seconds for single-unit trucks to cross over.

As stated previously, for a multi-lane roads the methodology recommends adding 0.5 seconds and 0.7 seconds for each additional lane required to cross for passenger cars and single-unit trucks, respectively.

For crossing, vehicles would have to cross two additional through lanes and the center left-turn lane (3 lanes). Therefore, the time gap was increased by 1.5 seconds for passenger cars and 2.1 seconds for single-unit trucks. Table 3 presents a summary of the recommended sight distances for crossing manuevers.

Table 3 Recommended Sight-Distance for Crossing Manuevers								
	Base Time gap	Time Gap Adjustment (3 add'l lanes)	Calculated crossing minimum Sight Distance	Left-turn minimum				
Passenger Car	6.5	1.5	470.4	475				
Single Unit	8.5	2.1	623.3	625				

As shown by the results in Table 3, existing sight distance is below the calculated recommended sight distance for crossing maneuvers at the intersection.

Findings

Based on field observations existing sight distances at the intersection of Martintown Road and Southwood Drive are less than recommended values. These limitations are caused by existing vegetation on the parcels on both sides of the intersection. The solution would be to work the property owners of these two parcels to clear the vegetation to the extent of providing at least 650-feet of clear sight distance.



FIGURES





Exiting sight distance to the north.





Exiting sight distance to the south.





Approaching sight distance from the north.





Approaching from the south.



Tony

ORDINANCE NO. 91-05 TO CHANGE THE CORPORATE LIMITS OF THE CITY OF NORTH AUGUSTA BY ANNEXING PROPERTY LOCATED ADJACENT TO CHANTICLEER SUBDIVISION OWNED BY BISHOP F. STRICKLAND

WHEREAS, Section 5-3-150 of the Code of Laws of the State of South Carolina provides that: "Any area or property which is contiguous to a city or town may be annexed to the city or town by filing with the municipal governing body a petition signed by seventy-five percent or more of the freeholders owning seventy-five percent or more of the assessed valuation of the real property in the area requesting annexation. Upon the agreement of the governing body to accept the petition and annex the area, and the enactment of an ordinance declaring the area annexed to the city or town, the annexation shall be complete;" and

WHEREAS, the Mayor and City Council of the City of North Augusta, by adoption of Resolution No. 91-03, dated March 4, 1991, wish to annex the below described property.

NOW, THEREFORE, BE IT ORDAINED by the Mayor and City Council of the City of North Augusta, South Carolina, in meeting duly assembled and by the authority thereof that:

I. The corporate limits of the City of North Augusta, South Carolina, shall be expanded by annexing the following property:

All those pieces, parcels, or tracts of land with, improvements thereon, situate, lying and being in the County of Aiken, State of South Carolina, adjacent to the present City limits of North Augusta, containing 41.4 +/- acres, beginning at a point of intersection of the western right-of-way line of Big Pine Road and the present City limits, thence S 350 39' W 2,750 +/- feet along said City limits line, thence N 500 23' W 80 +/feet, thence N 41° 51' E 161 +/- feet, thence N 7° 6' E 181.2 +/- feet, thence N 00 40' E 287.7 +/- feet, thence N 50 46' E 222.10 +/- feet, thence N 110 9' E 122.3 +/- feet, thence N 00 17' W 147.4 +/- feet, thence N 230 32' E 175.1 +/- feet, thence N 380 49' E. 900.9 +/- feet, thence N 380 49' E 129.6 +/- feet, thence N 680 27' E 298.1 +/- feet, thence N 680 27' E 240.41 +/- feet, thence N 680 50' E 380.0 +/- feet, thence S 240 44' E 236.02 +/- feet, thence S 240 44' E approximately 230.0 +/- feet along the western rightof-way line of Big Pine Road to the point of beginning.

Said property is shown on a plat identified as Exhibit "A", entitled "Plat of Property Sought to be Annexed to the City of North Augusta, South Carolina," dated February, 1991. Said property is further identified on a plat entitled "Property Located in Northwest Section of North Augusta" prepared by Joe L. Grant, dated March, 1970, from which a more complete and accurate description of the metes, bounds, and location of the property can be determined.

Said property is identified by the following Tax Map Parcel Numbers and Plat Reference Numbers.

Tax Map Parcel No.

00-008-01-918

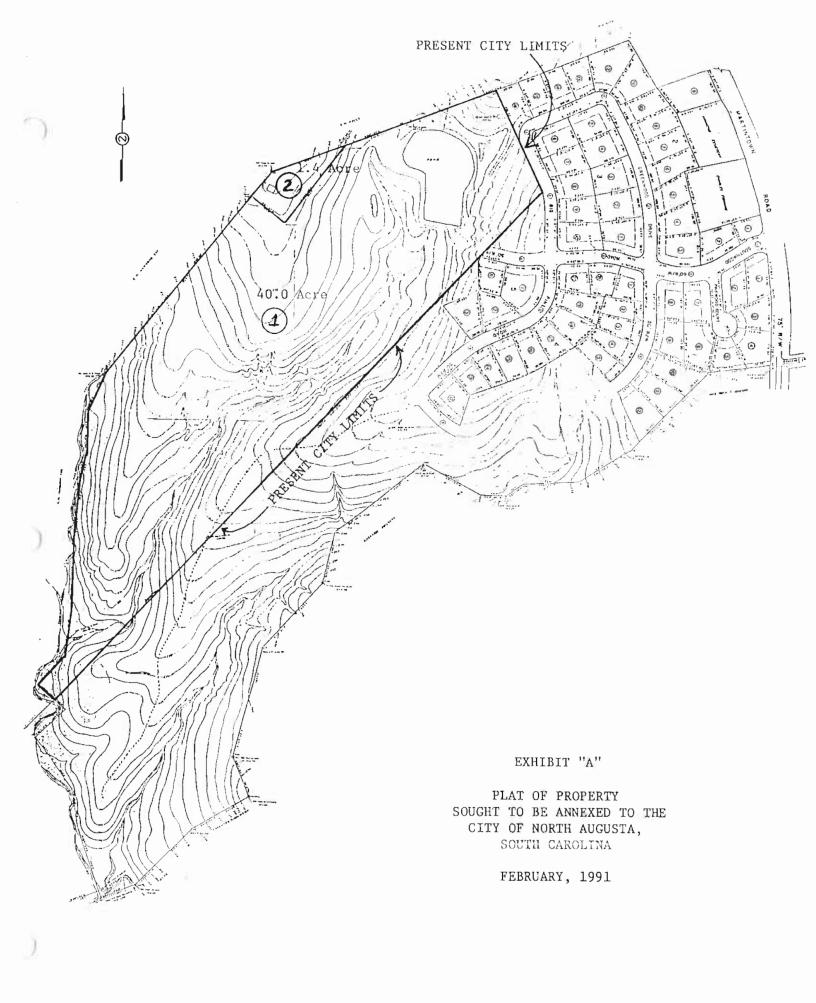
2 00-008-01-024 II. In conformance with the City's Land Use & Development Plan, the property shall be zoned R-2, Single-Family Residential, under the official Zoning Ordinance of the City of North Augusta and shown on the official Zoning Map as same, as shown on a plat attached hereto marked Exhibit "B" entitled "Zoning of Property Sought to be Annexed to the City of North Augusta, South Carolina," dated February, 1991. III. This Ordinance shall become effective immediately upon its adoption on third reading. IV. All ordinances or parts of Ordinances in conflict herewith are, to the extent of such conflict, hereby repealed. DONE, RATIFIED AND ADOPTED BY THE MAYOR AND CITY COUNCIL OF THE CITY OF NORTH AUGUSTA, SOUTH CAROLINA, ON THIS 18cl DAY OF March, 1991. First Reading 3-4-9/ Thomas W. Greene, Mayor

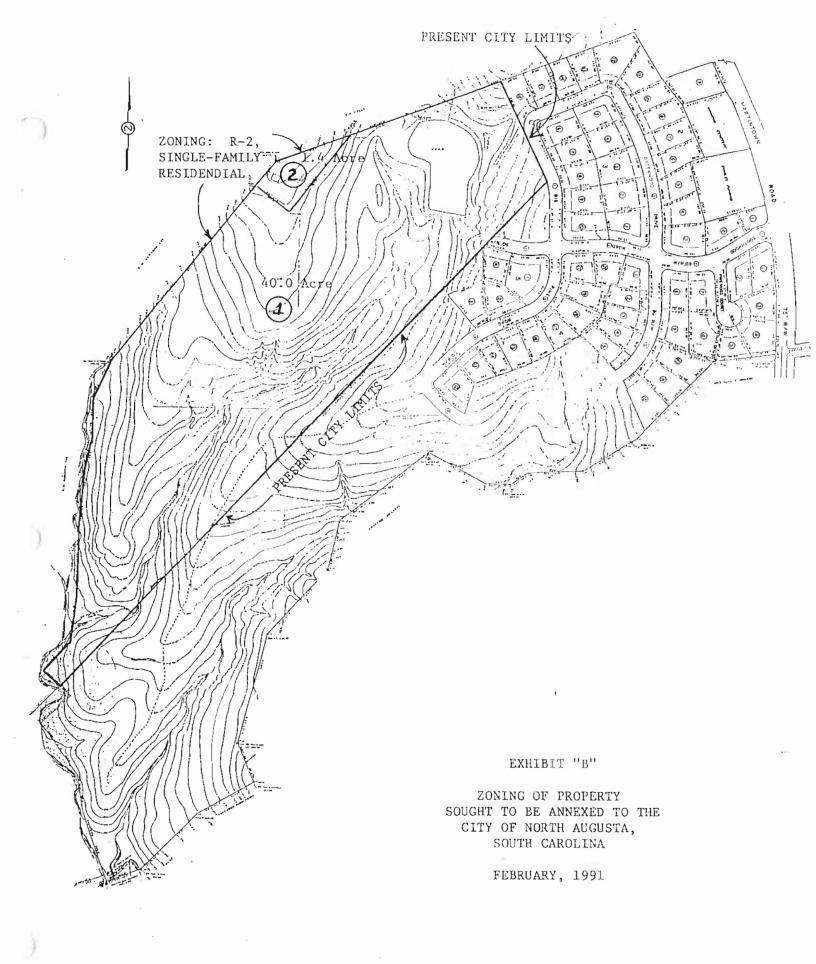
Plat Reference No.

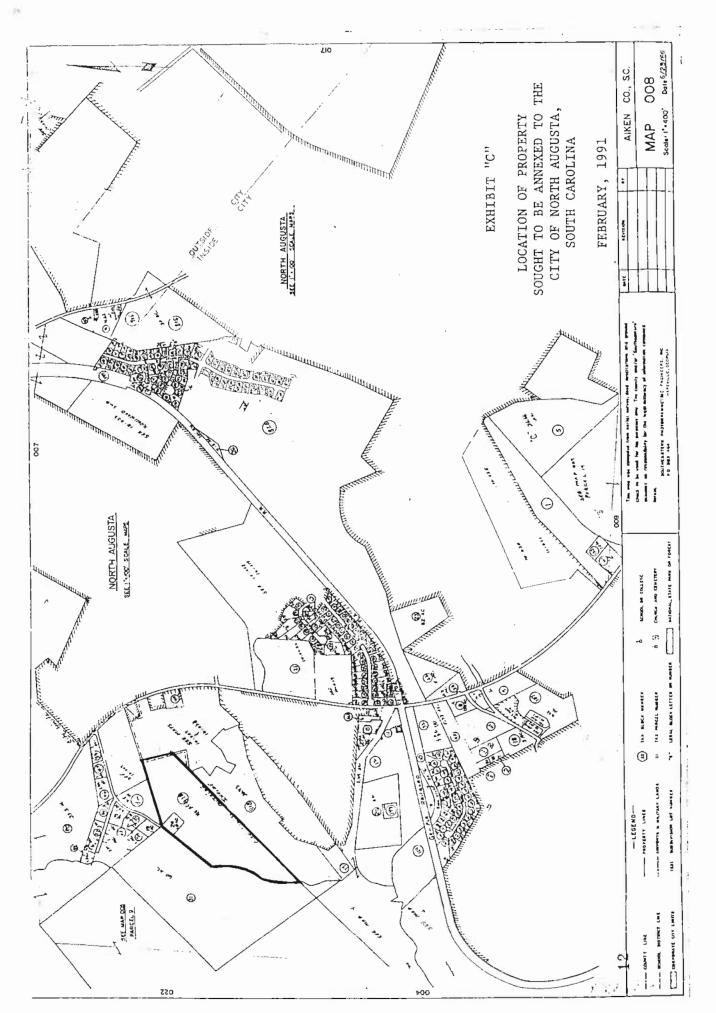
1

Second Reading 3-4-9/

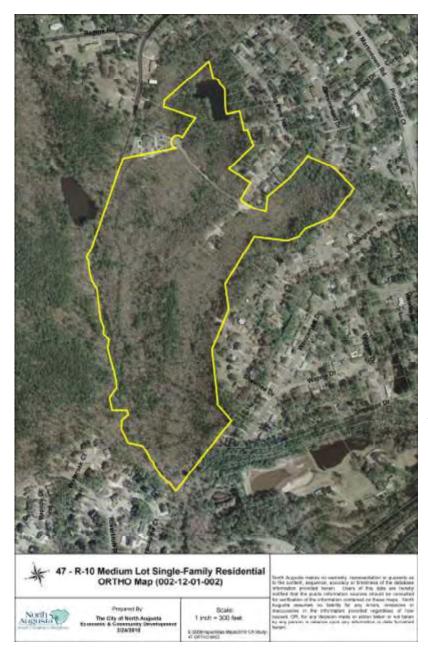
Third Reading 3-/8-9/







7.



Parcel Number: 002-12-01-002

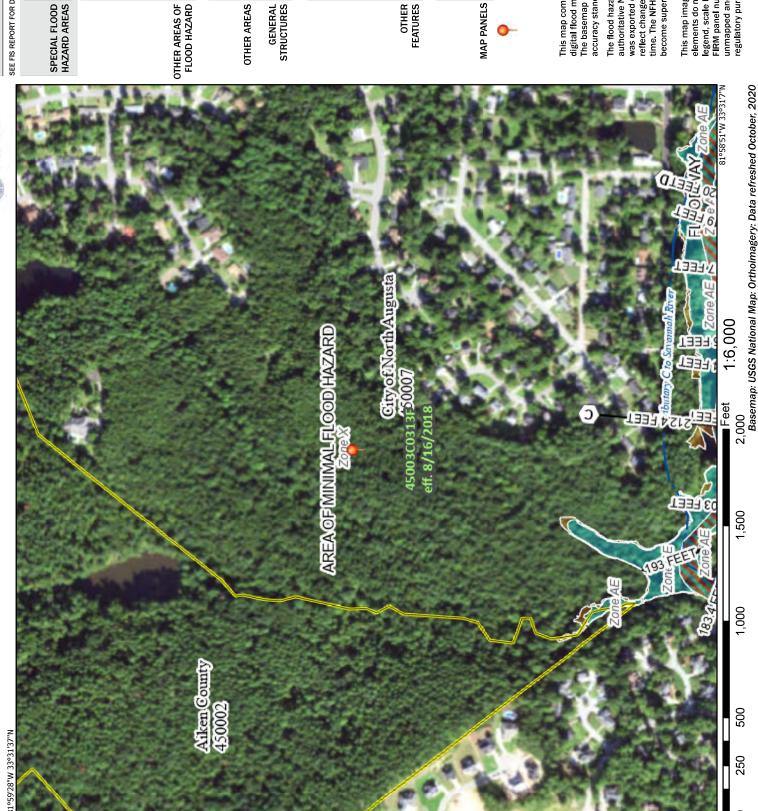
Description: This 61-acre parcel is zoned Medium Lot Single-Family Residential, and it is located southwest of the Chanticleer subdivision and northeast of The Rapids subdivision. There is a pond and associated wetland on the northeastern section of the property which receives seepage, as well as drainage from homes and streets in Chanticleer. The pond drains into a streambed which crosses under Big Pine Road and flows to the south to merge with two other streams that flow along the eastern and western boundaries (see figure). The stream along the east originates with a spring that is located near the end of Greenwood Drive. The stream along the west is drainage from Hammond Pond, which is located on the adjacent parcel (#002-12-01-001). The area provides critical habitat for bottlebrush buckeye (Aesculus parviflora) and relict trillium (Trillium reliquum). Both of these are protected plant species mentioned in the Natural Resources section of the City's Comprehensive Plan for growth and development (see section 8.7, page 8-3). Portions of this parcel are also listed on the U.S. Fish and Wildlife Service's National Wetlands Inventory.

Recommendation: Development of this parcel is not recommended due to due to issues with drainage and critical wetland habitat.



National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

Regulatory Floodway

With BFE or Depth Zone AE, AO, AH, VE, AR Without Base Flood Elevation (BFE)

SPECIAL FLOOD HAZARD AREAS

0.2% Annual Chance Flood Hazard, Areas depth less than one foot or with drainage areas of less than one square mile Zone X of 1% annual chance flood with average

Future Conditions 1% Annual

Area with Reduced Flood Risk due to Chance Flood Hazard Zone X Levee. See Notes. Zone X Area with Flood Risk due to Levee Zone D

No screen Area of Minimal Flood Hazard Zone X **Effective LOMRs**

Area of Undetermined Flood Hazard Zone D

OTHER AREAS

Channel, Culvert, or Storm Sewer GENERAL | - - - - Channel, Culvert, or Storn STRUCTURES | 1111111 Levee, Dike, or Floodwall

Cross Sections with 1% Annual Chance Water Surface Elevation

Base Flood Elevation Line (BFE) Coastal Transect mm 513 mm

Limit of Study

Coastal Transect Baseline Jurisdiction Boundary

Hydrographic Feature

OTHER

FEATURES

Digital Data Available

No Digital Data Available

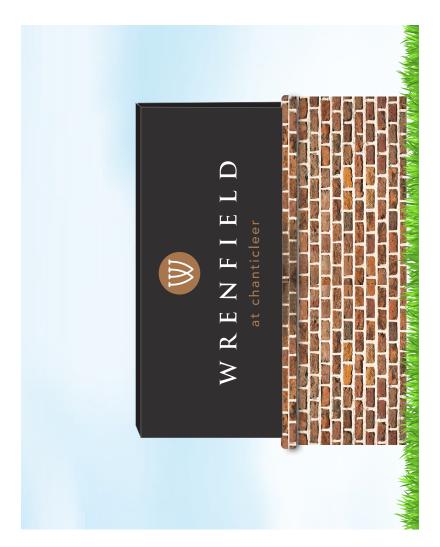
Unmapped

MAP PANELS

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of The basemap shown complies with FEMA's basemap digital flood maps if it is not void as described below

authoritative NFHL web services provided by FEMA. This map reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or The flood hazard information is derived directly from the was exported on 8/8/2022 at 4:47 PM and does not become superseded by new data over time. This map image is void if the one or more of the following map legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for elements do not appear: basemap imagery, flood zone labels, regulatory purposes.



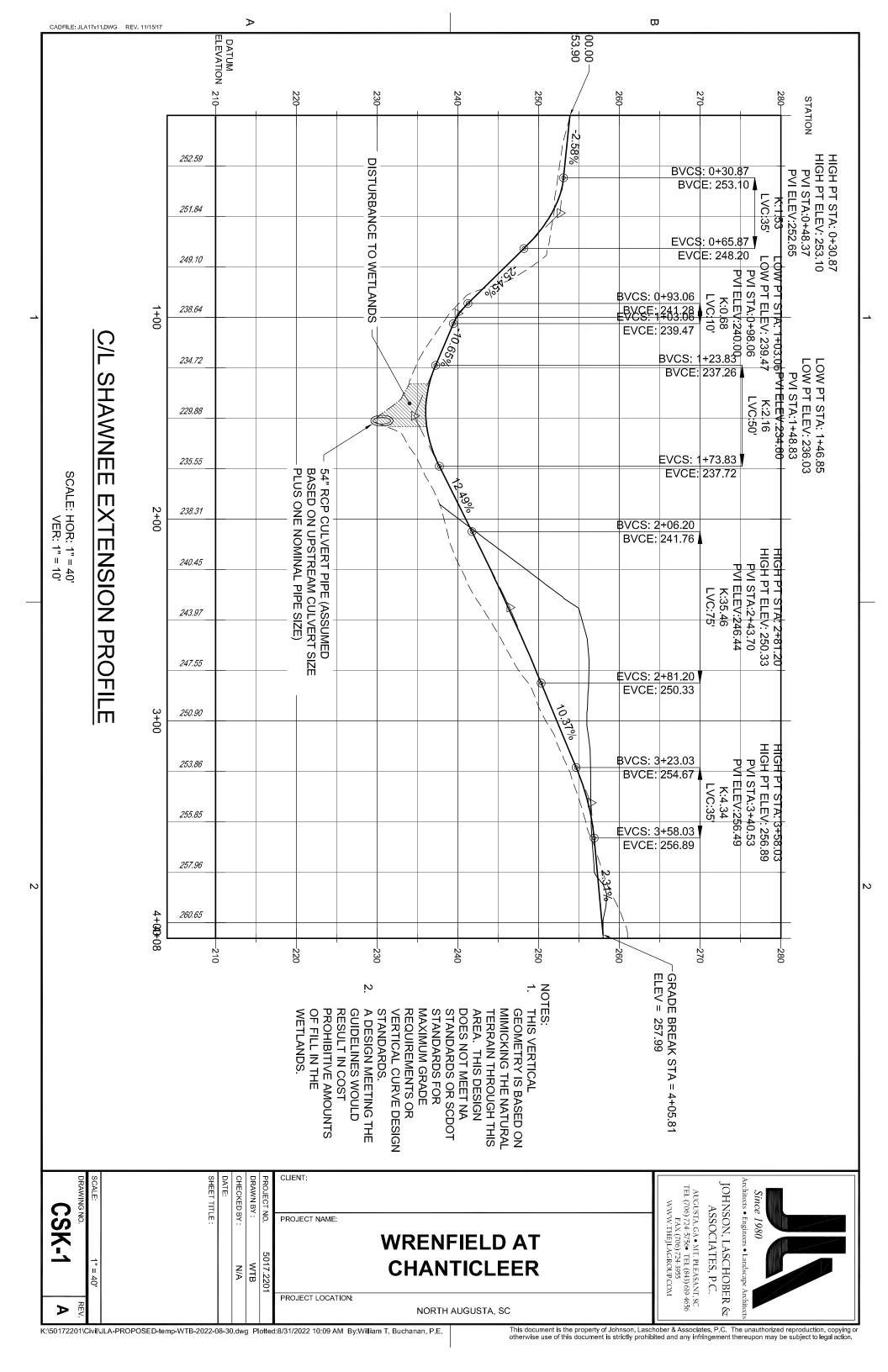
Manticleer

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Infrastructure Systems Management, LLC

P.O. Box 277, Augusta, Georgia 30903

Tel (706) 250-3228 **Fax** (706) 397-3523

Website <u>www.ismllc-engr.com</u> Email scassell@ismllc-engr.com



"Civil & Construction Engineering Services"

MEMORANDUM

TO: Ms. Alexandra Reynolds, PE

FROM: Steven J. Cassell, PE

DATE: August 26, 2022

SUBJECT: Wrenfield at Chanticleer Neighborhood Signal Warrant Assessment

The purpose of this memorandum is to provide an assessment of the need of a traffic signal being at the intersection of Martintown Road and Southwood Road/Curtis Drive as part of the Wrenfield at Chanticleer Neighborhood.

As presented in the study, the addition of projected traffic from the Wrenfield at Chanticleer Neighborhood will no doubt have an impact on the operations of the intersection and could be expected to increase delay during the morning and evening peak hours as was noted in the traffic study and a traffic signal could improve this situation from a delay standpoint for exiting traffic only.

However, taking into account the overall impact to delay along Martintown Road corridor as well as the fact that the projected volumes at the intersection would not likely meet signal warrants, I would not recommend pursuing installation of a traffic signal at this point.



Department of Planning and Development



Project Staff Report

CONPL21-002 Big Pine Subdivision

Prepared by: Kuleigh Baker Meeting Date: October 21, 2021

SECTION 1: PROJECT SUMMARY

Project Name	Big Pine Subdivision
Applicant	JLA
Address/Location	Termini of Southwood Drive, Big Pine Road, and
	Greenwood Drive
Parcel Numbers	002-12-01-002
Total Development Size	± 66.9 ac
Zoning	R-10, Medium Lot, Single-Family Residential
Use Pattern	Conservation Subdivision
Traffic Impact Tier	2
Proposed Use	122 Single-Family Residential detached dwellings
Future Land Use	Low Density Residential

SECTION 2: PLANNING COMMISSION CONSIDERATION

The plans have been submitted for review by the Planning Commission based on the following portions of the Development Code:

NADC § 5.1.2.2 Sketch Plan

- a. In addition to the pre-application conference, at the request of the applicant subsequent to the pre-application conference, the Planning Commission may grant an informal review of a sketch or concept plan for a development for which the applicant intends to prepare and submit an application for development. The purpose of the sketch plan review process is to provide the Planning Commission input in the formative stages of a development plan.
- b. Applicants seeking sketch plan review shall submit the items stipulated in Appendix B, Application Documents, ten (10) days before the Planning Commission meeting at which the sketch plan will be reviewed. These items provide the applicant and Planning Commission with an opportunity to discuss the development proposal in its formative stages.
- c. A brief written summary of the sketch plan review shall be provided within ten (10) working days of the sketch plan review meeting.
- d. The applicant may be charged reasonable fees for the sketch plan review.

- e. The Planning Commission may make specific recommendations regarding the proposed development including the implementation of a citizen participation process (§5.1.7) prior to submitting the development application.
- f. The applicant shall not be bound by any sketch plan for which review is requested, nor shall the Planning Commission be bound by any such review.

SECTION 3: PUBLIC NOTICE

Per NADC Table 5-1, no notice of the request is required.

SECTION 4: SITE HISTORY

A portion of the subject property adjacent to the existing Chanticleer subdivision was annexed on March 18, 1991 by Ordinance No. 91-05. At that time, the property was zoned R-2, Single-Family Residential in conformance with the City's Land Use and Development Plan. The equivalent R-10, Medium Lot, Single-Family Residential zoning district was adopted with the Official Zoning Map of the 2008 North Augusta Development Code.

SECTION 5: EXISTING SITE CONDITIONS

	Existing Land Use	Future Land Use	Zoning
Subject	Vacant	Low Density Residential	R-10, Medium Lot, Single-Family
Parcel			Residential
North	Residential	Low Density Residential	Outside City Limits/R-10,
			Medium Lot, Single-Family
			Residential
South	Residential	Low Density Residential	R-14, Large Lot, Single-Family
			Residential
East	Residential	Low Density Residential	R-10, Medium Lot, Single-Family
			Residential/ R-14, Large Lot,
			Single-Family Residential
West	Vacant/Residential	Low Density Residential	Outside City Limits

Access - The site currently has access to West Martintown Road from Shawnee Drive, Southwood Drive, Big Pine Road, and Greenwood Drive.

Prepared by: Kuleigh Baker Meeting Date: October 21, 2021

<u>Topography</u> – The subject site has variable topography. The property does have streams on site, and would need to be properly delineated.

<u>Utilities</u> – Water and wastewater connections would have to be brought in from neighboring developments.

<u>Floodplain and Environmental Conditions</u> – A small portion of the site is located in Flood Zone X and AE with a 0.2% annual chance of flood hazard. Site located on FEMA FIRM panel 45003C.

<u>Drainage Basin</u> – The proposed development is located in the Pretty Run/Rapids Basin. Pretty Run basin is located in a highly dense residential part of North Augusta. The preliminary physical stream assessments at two reaches of the stream indicate that this stream channel is currently not effective at transporting current loads of stormwater during heavy storm events. A main sewer line runs along and in the stream channel and some of its tributaries. Overtopping of banks is obvious in several locations and manholes present in those locations may overflow if surcharging occurs. High nutrient concentrations have been detected in two samples during the period. The results indicate that urban runoff is impacting the stream channel. Many homes back up to the creek along its way through the city. The high density residential area contains well-maintained lawns in many instances. In addition, animals are penned at or near the creek along most of its reach. The city will continue to reach out to residents in the area to provide information that may help reduce pollutant loads.

SECTION 6: STAFF EVALUATION AND ANALYSIS

Applicable sections of the North Augusta Development Code have been provided for Planning Commission review and consideration. Staff commentary is provided in *italics*. Items of particular importance are highlighted in **bold**.

1) Purpose and Zoning Districts

The concept plan proposes 122 single-family residential detached dwellings developed in the R-10, Medium Lot, Single-Family Residential Zoning District using a Conservation Subdivision Use Pattern.

The purpose of these R-10, Medium Lot, Single-Family Residential District is to recognize and promote the character of particular areas in North Augusta where single-family residential development is the predominant living environment. Also, changing patterns of work and home environments create incentives to view the single-family dwelling as a place of work and residential living activities.

The Use Patterns established in the development code are not zoning districts. Instead, they are forms of development that may be permitted in the various zoning districts established by this Chapter, where indicated in this Article or Article 3, Zoning Districts, or both. Use Patterns are specific land use activities involving specific land uses and design controls which produce a discrete pattern of development. Article 2, Use Patterns of the NADC applies to any application for development approval where the applicant chooses to develop pursuant to the standards and procedures of a Use Pattern described in this Article. These provisions are optional, in that a decision to develop pursuant to the regulations established herein is subject to the discretion of the applicant. However, the improvement standards, parking requirements, and other regulations may vary depending upon whether an applicant chooses to develop pursuant to a Use Pattern established in the Article.

The purpose of this section is to provide flexibility in site design in order to allow developers to preserve common open space and natural resources in Conservation **Areas within a subdivision**. The specific purposes of this section are:

- a. To protect the public health, safety and general welfare by avoiding surface and ground water pollution, contaminated runoff, air quality contamination and urban heat islands which result from pavement and the clearing of natural vegetation;
- b. To protect and preserve natural resources such as wetlands, streams, lakes, steep slopes, woodlands and water recharge areas;
- c. To reduce infrastructure and housing costs by reducing the engineering and construction costs produced by conventional subdivision design, which requires more pavement, wetland crossings, grading of trees and natural areas, and lawn and landscaping maintenance;
- d. To protect property values by allowing open space design features which enhance the marketability of development;
- e. To provide design flexibility; and
- f. To promote development on soils which are most suitable for urban densities, while preserving soils that are primarily adaptable to other uses such as woodlands, wildlife habitat and agricultural uses
- 2.3.4.2 There is no minimum or maximum size for a Conservation Subdivision provided, however, that the minimum open space requirements may limit the availability of this option for some landowners. Parcels that cannot demonstrate compliance with the minimum open space standards on-site shall dedicate and maintain an open space system that is connected to an open space system on an adjacent site in accordance

Prepared by: Kuleigh Baker Meeting Date: October 21, 2021

with Article 11, Open Space and Parks.

2.3.4.3 Platted lots located within subdivisions and PDs shall be located outside of the Conservation Areas, which constitute the total required open space. Conservation Areas shall be placed in undivided preserves, although they are not required to be contiguous.

Conservation subdivisions are permitted as a use pattern in the R-10, Medium Lot, Single-Family Residential Zoning District by Table 3-2, Use Matrix of the North Augusta Development Code. Single-family detached dwellings are also permitted as a use in the R-10, Medium Lot, Single-Family Residential Zoning District by Table 3-2, Use Matrix of the North Augusta Development Code.

The R-10, Medium Lot, Single-Family Residential Zoning District has dimensional standards outlined in Table 3-3 of the NADC.

А	В	С	D	E	F	G	Н	I	J	K	L
Zoning District and Use Types	Minimum Lot Size (sq. ft)	Maximum Gross Density (du/ga)	ea	Impervious Surface Ratio	ە ⊐	Minimum Lot Width (ft)	Maximum Building	Minimum Front Setback (ft)	Maximum Front Setback (ft)	Minimum Side Setback (ft)	Minimum Rear Setback (ft)
3 R-10, Medium Lot, Single- . Family Residential	10,000	4.5		0.3	40	50	35	15		5	15

Note: 2.3.6.2 Lots within a Conservation Subdivision are not subject to the minimum lot size, minimum frontage or minimum lot width requirements of the Use Matrix, Table 3-2.

2) Landscaping

Landscape plans were not included as part of the concept plan review. Landscape plans are required per Section 10.4.1, and plans would be reviewed for conformance the article including street trees, entry landscaping, and any parking areas. Final landscaping on individual lots would be evaluated prior to final home certificates of occupancy.

Based on table 10-10, Street Tree Landscaping Requirements, the single-family detached development will require 1 large tree plus 1 per 40 feet of frontage or 1 small tree plus 1 per 30 feet of frontage.

Subdivision Entrance Landscaping will be reviewed per Article 10.8.

Individual residential lot landscaping specifications are not typically included at the time of major subdivision preliminary plat submittal. A sample detail based on the average lot and house size may be presented. Individual residential lot landscaping must pass inspection prior to issuance of a Certificate of Occupancy.

2.3.5.2 In order to provide undivided open space, direct views and access, not less than forty percent (40%) of the lots within a Conservation Subdivision shall abut a Conservation Area. Direct pedestrian access to the open space from all lots not adjoining the open space shall be provided through a continuous system of sidewalks and Greeneways.

Approximately 83%, 101 of the 122 planned lots will abut a conservation area.

3) Open Space

- 2.3.10.1 Lands designated as permanent open space including Conservation Areas:
 - a. Are not to be further subdivided; and
 - b. Shall be protected through a conservation easement or fee simple title held by the city or by an approved land trust or conservancy. The conservation easement or fee simple title shall prohibit further development of the open space.
- 2.3.10.2 Article 11, Open Space and Parks, relating to maintenance, shall apply to a Conservation Subdivision. No other requirements of the Open Space and Parks standards shall apply to a Conservation Subdivision.
- 2.3.10.3 Conservation Areas A minimum of forty percent (40%) of the total tract area shall be designated as Conservation Areas. The following areas may be designated as Conservation Areas:
 - a. Wetlands:
 - b. Woodlands;
 - c. Sensitive aquifer recharge features, including areas with highly permeable, excessively drained, soil;
 - d. All of the floodway and flood fringe within the 100-year floodplain, as shown on official Federal Emergency Management Association (FEMA) maps;
 - e. All areas within one hundred (100) feet of the edge of the 100-year floodplain as delineated on the FEMA maps and any Letter of Map Revision;
 - f. All areas within one hundred (100) feet of the banks of any stream shown as a blue line on the United States Geological Survey (USGS) 1:24,000 (7.5 minute) scale topographic maps for Aiken County;
 - g. Slopes exceeding twenty five percent (25%);

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- h. Soils subject to slumping, as indicated on the medium-intensity maps contained in the county soil survey published by the United States Department of Agriculture (USDA) Natural Resources Conservation Service;
- i. Significant wildlife habitat areas;
- j. Historic, archaeological or cultural features listed, or eligible to be listed, on national, state or county registers or inventories; and
- k. Scenic views into the property from existing public roads.

Approximately 51.76% of the proposed neighborhood will be provided as open space.

- 2.3.10.4 Stormwater detention ponds or basins and land within the rights of way for underground pipelines may be included as part of a Conservation Area. Not more than fifty percent (50%) of the land within the right of way of high-tension power lines shall be included within a Conservation Area.
- 2.3.10.5 Conservation Areas shall abut existing open space land on adjacent parcels, including the North Augusta Greeneway, passive open space located in other subdivisions, public parks or properties owned by or leased to private land conservation organizations.
- 2.3.11 Natural Resource Protection -- A Conservation Subdivision shall comply with Article 9, Floodplain Management, and Article 10, Landscaping. In addition, the Conservation Subdivision shall comply with the following standards:
- 2.3.11.1 No Conservation Area shall be cleared, graded, filled or subject to construction. However, rights of way for Greeneways, Article 14, Streets, any streets needed to provide access to the proposed subdivision, and water, sewer, electric, or cable lines may be cleared. The width of rights of way for streets or Greeneways shall be restricted to the minimum as designated in §14.4.
- 2.3.11.2 No lot may be platted within woodlands located on highly erodible soils with slopes exceeding ten percent (10%).

The parcel area provides critical habitat for bottlebrush buckeye (Aesculus parviflora) and relict trillium (Trillium reliquum). Both of these are protected plant species mentioned in the Natural Resources section of the City's Comprehensive Plan (Chapter 8). The proposed development does not reach the boundary of this habitat as illustrated in the Critical Areas Assessment No. 47 completed in 2011 and attached to this staff report.

4) Parking

2.3.13 In order to encourage design flexibility, to preserve open space and to minimize impervious surfaces, a Conservation Subdivision shall not be subject to the minimum parking requirements of Article 12, Parking. A Conservation Subdivision shall be subject to the maximum parking requirements of Article 12. Table 12-1 Parking Requirements by Use does not assign a maximum number of vehicle spaces for single-family detached dwellings.

Parking will be accomplished through garages and driveways on individual lots. Further information regarding parking for any potential postal cluster boxes (if applicable) will be required for staff review of the preliminary plat.

5) Signage

Signage information is not required at Preliminary Plat, but is recommended. Signage will be reviewed per Section 13.8.2 by Staff.

13.8.2.c.i. Subdivision Entrance Signs

- a. Applicability: this section applies to signage identifying a development and is located internal to and visible from the initial point of entry to the neighborhood.
- b. The size, location and design of subdivision entrance signs shall be included on the approved preliminary plat. If a subdivision sign is requested after the plat has been approved it may be approved in accordance with this section.
- c. If a Subdivision/Project Identification Sign is preferred within an existing subdivision or as part of a phased development, a "Master Signage Plan" shall be required.
- d. Subdivision Identification Signs must meet the following:
 - i. Not more than one (1) subdivision entrance sign shall be located at the entry to any subdivision as identified on the preliminary plat.
 - ii. Shall be a monument sign not to exceed 32 sq. ft. or 5' in height.
 - iii. If two (2) identical monument signs are used, they may not exceed sixteen (16) square feet each in size and four (4) feet in height and must be placed symmetrically on each side of an entry road.
 - iv. Subdivision entrance signs may be located in the right of way within a required median but must be outside of the paved section of the roadway.
 - v. Shall not be internally illuminated.

6) Street Design

Street types should be indicated on the preliminary and final subdivision plats, with the developer's Traffic Impact Analysis (TIA) serving as a guide for the number of trips.

Table 14-1 Street Design Criteria (Rev. 12-1-08; Ord. 2008-18)

			Lo	ocal		Subcollector			Coll	ector	Arterial	
	A	В	С	D	E	F	G	Н	I	J	K	L
	Design Factor	Alley	Lane	Small Street	Street	Large Street	Rural Street	Boulevard Street	Collector 1	Collector 2	Arterial 1	Arterial 2
1.	Right of Way (ft)	20	17-23	24-40	36-50	42-52	38	50-156	56-78	62-100	62-180	80-200
2.	Travel Lanes	1	1	2	2	2	2	2-4	2-4	4-6	4-6	4-7
3.	Parking Lanes	0	0	0-1	0-1	0-2	0	2	2	0-2	0	0
4.	Pavement Width (ft)	12	16-18	18-24	20-30	30-36	22	30-56	38-60	44-82	44-66	44-80
5.	Corner Radius (ft)	10	10	10	15	15	15	15	15	25	25	25
6.	Centerline Radius (ft)	50	90	90	90	100	100	250	600	500	1,000	1,000
7.	Drainage	SH	CG (SH) (SW)	CG (SH) (SW)	CG	CG	CG (SH) (SW)	CG	CG	CG	CG or SH	CG or SH
8.	Median	1	-	-	-	-	-	Yes	Yes	Yes	Yes	Yes
9.	Block Length (ft)	400	200	500	650	750	-	750	850	1,000	-	-
10.	Sidewalks	-	-	2	2	2	-	2	2	2	2	2
11.	Planting Strip (ft)	ı	4	4	5	5	-	-	6	8	10	10
12.	Bike Lanes	Ī	-	-	-	-	Yes	-	Yes	Yes	Yes	Yes

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13.	Trees	-	-	Yes								
14.	Grade (%)	6	8	12	12	12	15	8	8	8	8	8

The maximum block length permitted on a local street is 650 ft. The total road length for the proposed Big Pine Road extension is 1786 ft and Sommerhouse Branch Road is 1925 ft. Big Pine Road from the cul-de-sac to the intersection of Pinus Taeda Court is 988 ft. Sommerhouse Brand Road from the cul-de-sac to the intersection of Creek Court is 999 ft. **The proposed block lengths will require a Planning Commission waiver**. Section 14.19.2 gives the Planning Commission permission to increase the length of a cul-de-sac to 1000 ft where natural features including topography, environmental constraints, and natural conditions preclude a connecting street design.

Table 14-2, Street Design Criteria also requires 2 sidewalks (one on each side of the street) for local streets. With a 5 ft planting strip and street trees. The project Engineer has proposed a 7.5 ft planting strip to allow root zone space within the right-of-way for proper tree growth.

Street lighting will be reviewed per Section 14.16. in conjunction with Dominion Energy.

- 2.3.6.3 Lots within one-hundred (100) feet of a Conservation Area shall front on a Local Street, as defined in Article 14, Streets. Lots shall not front on a Collector or higher order street.
- 2.3.7 A Conservation Subdivision shall comply with Article 14, Streets, unless otherwise provided, and this subsection. The design of local streets shall comply with the standards for rural streets, as set forth in Article 14. The Connectivity Index for internal streets as set forth in Article 14 shall not apply to local streets within a Conservation Subdivision. The Connectivity Ratio is exempt for Conservation Subdivisions by Table 14-8 and does not require a waiver.
- 2.3.7.1 The Conservation Subdivision shall include a pedestrian circulation system designed to assure that pedestrians can walk safely and easily on the site, between properties and activities or special features within the neighborhood open space system, by complying with the standards set forth herein. All sidewalks shall connect to other sidewalks or with Greeneways, which in turn shall connect to potential areas qualifying as Conservation Areas on adjoining undeveloped parcels or with existing open space on adjoining developed parcels, where applicable.

2.3.7.2 Streets shall not cross wetlands or existing slopes exceeding fifteen percent (15%).

The proposed street design was laid out to minimize grading and avoid slopes to the extent practical. The two cul-de-sac design avoids additional stream crossings. The Shawnee Drive stubout has not been extended to the property due to the steep topography.

Final street name reservations will be required at the time of Planning Commission review of the Major Subdivision Preliminary Plat application.

7) Summary of Waivers

This list is of anticipated waivers required based on a preliminary review of the plans submitted for this Sketch Plan review. Additional waivers may be identified as more complete plans are developed. Waivers will be considered by the Planning Commission at the time of site plan approval.

Block Length

SECTION 8: ATTACHMENTS

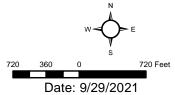
Site/Aerial Map Topography Map **Current Zoning Map** Future Land Use Map **Application Documents** Sketch Plan ANX91-05 Critical Areas Study Ph II Assessment No. 47

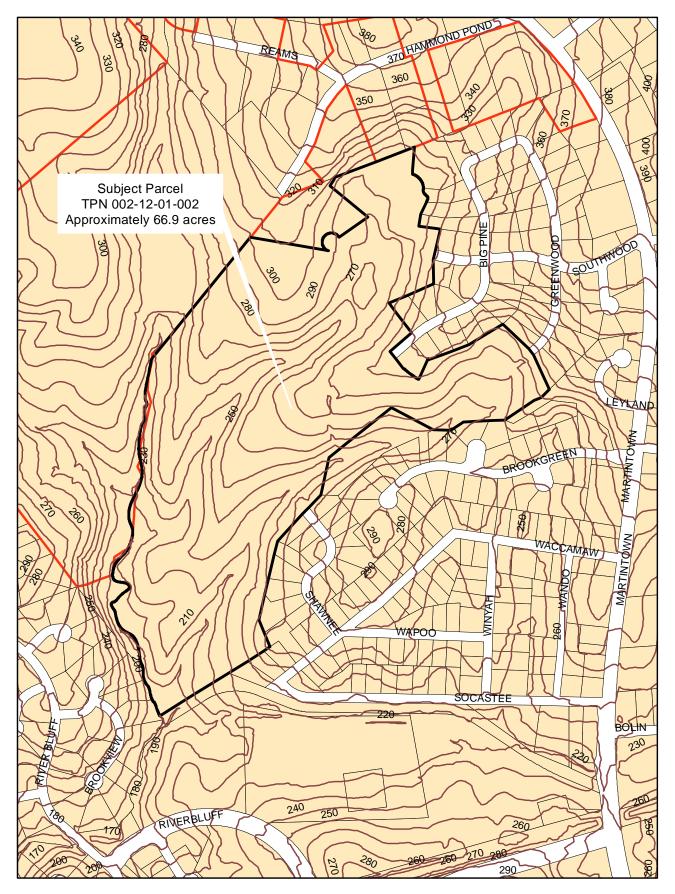
Alexandra Reynolds, Johnson Laschober & Associates, via email CC. Jonathan Crawford, Southeastern Company, via email





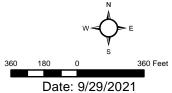
Aerial Map Application CONPL21-002 TPN 002-12-01-002 Approximately 66.9 acres

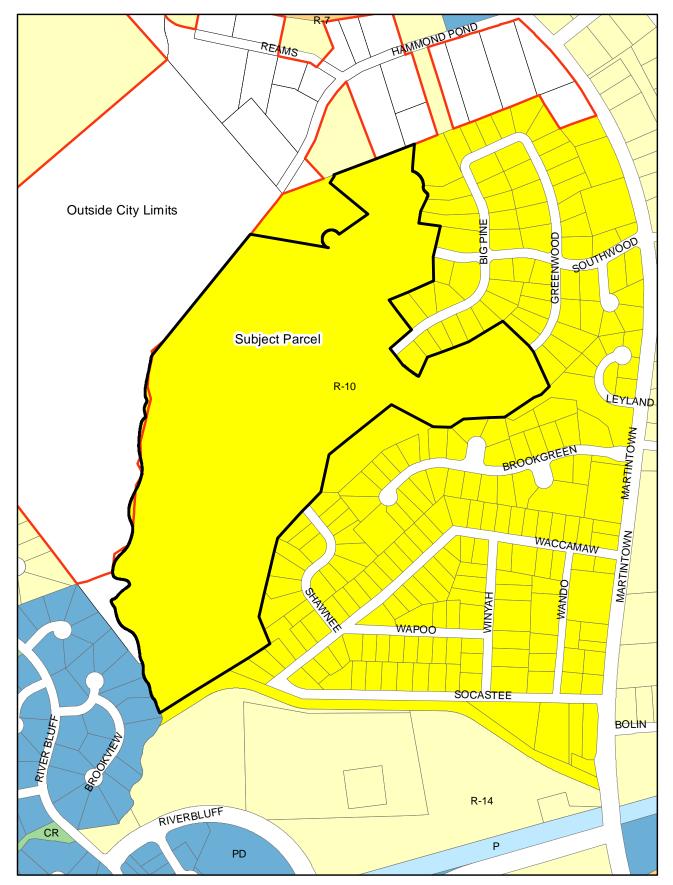






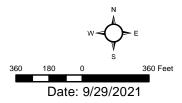
Topography Map
Application CONPL21-002
TPN 002-12-01-002
Approximately 66.9 acres

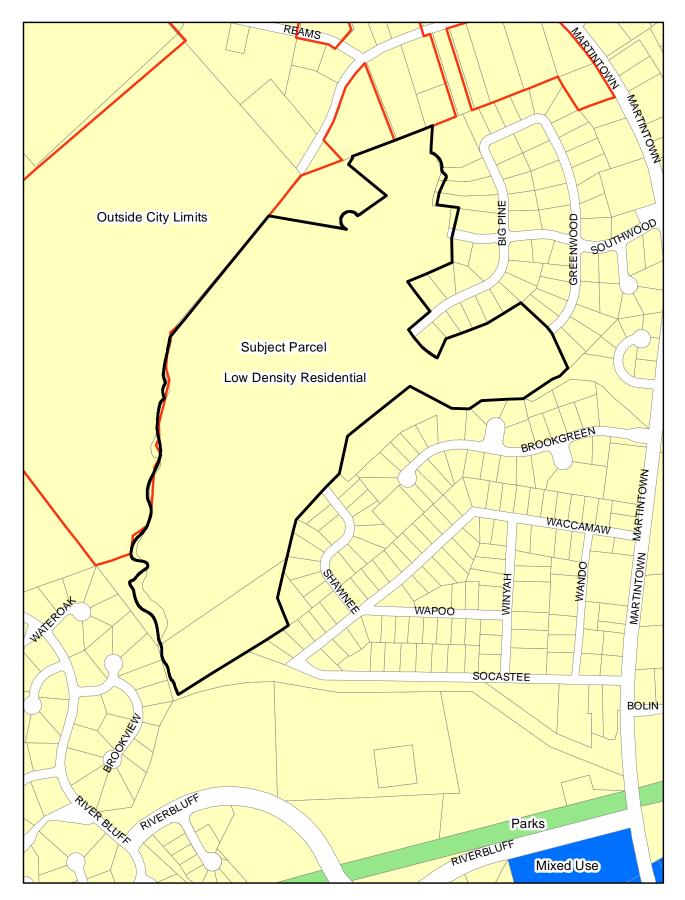






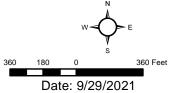
Zoning Map
Application CONPL21-002
TPN 002-12-01-002
Approximately 66.9 acres
R-10, Medium Lot,
Single-Family Residential







Future Land Use Map Application CONPL21-002 TPN 002-12-01-002 Approximately 66.9 acres Low Density Residential



Application for Development Approval





Sta	aff Use
Application Number	Date Received
Review Fee	Date Paid
1. Project Name BIG PINE NEIGHBORHOW (A	NAME SUBJECT TOCHANGE)
Project Address/Location B16 PINE ROAD	(PARCEL BOUNDARY IS WHERE BIG PINE 120AD ENUS)
Total Project Acreage 66.90 ACRES	Current Zoning R-10
Tax Parcel Number(s)	
^ ^	Applicant Phone (706) 833-3585
Mailing Address 2743 Perimeter Pk	30909 Email jonathan.crawfordesoutheastern.
City Mugusta ST GA Zip	30909 Email jonathan.crawtorde southeastern.
or is mere a pesignated Agent for fulls btolects	Yes No form. (required if Applicant is not property owner)
4. Engineer/Architect/Surveyor ALEXANDRA R	EYNOLOS License No. 1557
	S Firm Phone <u>706-724-5756</u>
Firm Mailing Address 1296 BROADSTREET	
City AUGUSTA ST GA Zip 3	3090 Email AREYNOLIS & THE JLAGROUP.COM
	Date 9-28-202
 Is there any recorded restricted covenant or other prohibits the use or activity on the property that is t (Check one.) 	private agreement that is contrary to, conflicts with or
of North Augusta review the attached project pla Augusta, as outlined in Appendix B of the North Au	augusta Development Code, I hereby request the City ans. The documents required by the City of North augusta Development Code, are attached for the City's does that all required documents must be correct and
Applicant or Designated Agent Signature	9 /28/2 Date
Tonathen M. Cranford Print Applicant or Agent Name	

Designation of Agent





This form is required if the property owner is not the applicant.

	Staff Use Only
A	Application Number Date Received
1.	. Project Name BIG PINE NEIGHBORHOOD (NAME SUBJECT TO CHANGE)
	Project Address/Location BIG PINE ROAD (PARCIL BOUNDARY IS WHELE BIG PINE ROAD ENDS)
	Project Parcel Number(s) <u>002-12-01-002</u>
2.	Property Owner Name Maria S. Diffy Owner Phone 706 8295553 Mailing Address 804 Big Pine Rd
	city North Augusta ST SC Zip 2984/ Email doowaha@ comcast net
3.	Designated Agent JONATHAN CRAWFORD
	Relationship to OwnerREAL_ESTATE_AGENT
	Firm Name SOUTHEASTERN Phone 706-854-6738
	Agent's Mailing Address 2743 PERZMETER PARKWAY BUILDING 100 SUIJE 370
	City AUGUSTA ST GA Zip 30009 Email JONATHAN CIZAWFORD & SCUTHEASTER Agent's Signature Agent's Signature Date 9/28/21 COMPAN
	I hereby designate the above-named person (Line 3) to serve as my agent and represent me in the referenced application. Owner Signature Date
	Owner Signature Date Date Sworn and subscribed to before me on this 28 day of September, 20 21. Tandii Simmons Notary Public November 9, 2027
õ	Commission Expiration Date

IIC PINE ROAD NORTH AUGUSTA, SC 29841 COVER SHEET CG001 **NEIGHBORHOOD** BIG PINE ROAD MERIT COMMERCIAL HOLDINGS TIEM O-CHREENT ZONNO, TOTARE, WOTH DEPTH, YARD SETBACKG, BULDING CONFORCE, CPRESS PRINCE, ENGINE ETC. CONFRIENT ZONNO, MEDUNIU OT SHOULE FAMILY. THE ALL OT WITH ACCOMMODATE AT LEAST 2 VEHICLES HAVE ALL OT WITH ACCOMMODATE AT LEAST 2 VEHICLES ITEM FOOTHINED
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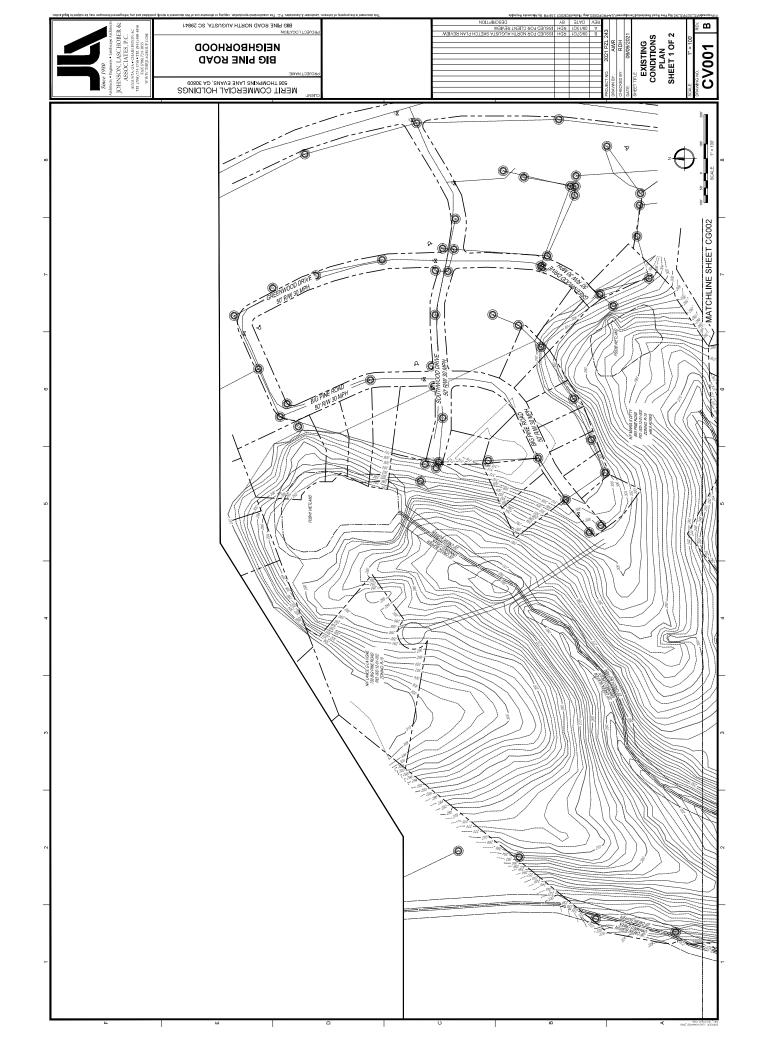
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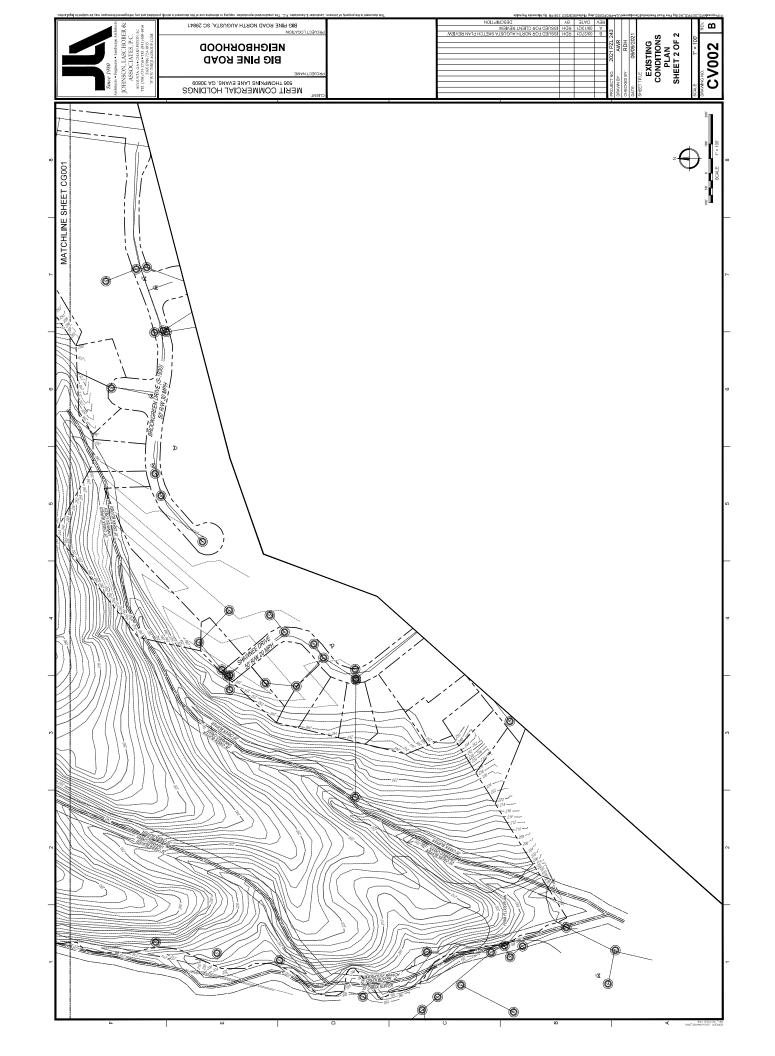
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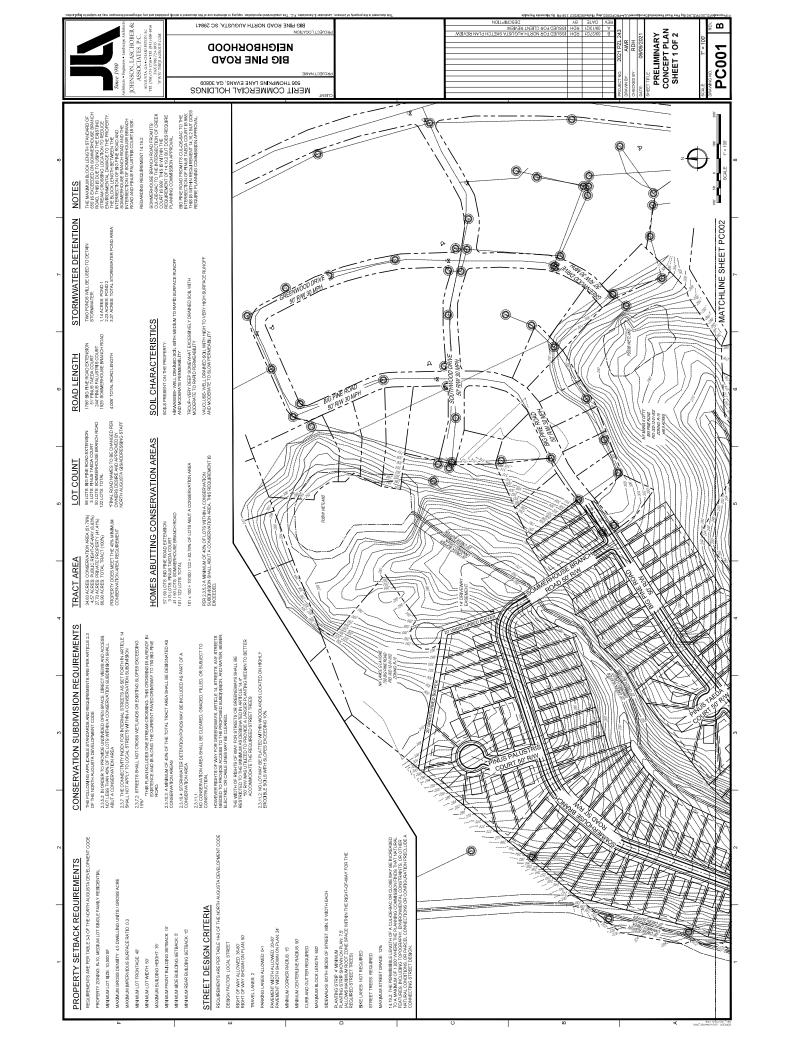
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RINDOFF AND WOORDENTE TO SAND PERMEMBLITY. TOPOGRAPHY.
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SLOPES ON THE SITE RANGE FROM 0.24% THE STEEPEST SLOPES HAVE BEEN
SLOPED AS MUCH AS IS PRACTICAL IN ACCORDANCE WITH 6.1.32. ITEM F. SITE ANALYSIS AND DEVELOPMENT RECOMMENDATIONS REPORT PER 6.1.1
SPETS COWD AND COWDS SHOWE KISTING SITE CONDITIONS, ALL REFRERICED
SPEDNANCES ARE REGM THE NORTH AUGUSTA DEVELOPMENT CODE. BELOWARE
DESCRIPTIONS OF EACH FEATURE. STRUCTURES: NO EXISTING STRUCTURES ARE PRESENT ON THE PROPERTY PLANNED STRUCTURES ARE 122 HOUSES AROUND 2,100 SF (35"X 60"). **BIG PINE NEIGHBORHOOD** EXISTING VEGETATION: THE SITE IS WOODED WITH A MIX OF PINE AND HARDWOODS. MERIT COMMERCIAL HOLDINGS 506 THOMPKINS LANE EVANS, GA 30809 ITEM A. APPLICATION FOR DEVELOPMENT APPROVA SUBMITTED WITH THIS SET OF DRAWINGS OTHER ENVIRONMENTAL CHARACTERISTICS: THERE ARE NONE KNOWN. ITEM C. EXECUTED DESIGNATION OF AGENT FORM SUBMITTED WITH THIS SET OF DRAWINGS BIG PINE ROAD NORTH AUGUSTA, SC ITEM B. REQUIRED \$100.00 FEE SUBMITTED WITH THIS SET OF DRAWINGS ITEM E- LOCATION MAP SEE DRAWING CG001 CONSTRUCTION TYPE: RESIDENTIAL SUBDIVISION PROPERTY COORDINATES: 33.5241° N, -81.9840° W R-10, MEDIUM LOT SINGLE FAMILY RESIDENTIAL 002-12-01-002 66.90 ACRES DISTURBED AREA: 32.27 ACRES **LOCATION MAP** TAX PARCEL#: TOTAL AREA: OWNER CREMARY PERMITEE:
MENT COMMERCIAL HOLDINGS
MAN HOLLOWAY
SOF THOMPINS LANE
EVANS, CA 20020
HONE: COO 323 4-400
IRAN: LUCKUL LOWAY (@MERITELOOR.COM OWNER'S REP'24 HOUR CONTACT.
JOHNSON, LASCHOBER &
ASSOCHATES, P.C.
REIT HARBESON, PLA
1298 BROAD STREET
AUGUSTA, GA, STREET
HOURE: (708) 724-57-56
EMAL. Harbason@heljagroup.com igoplusDESCAPITON
COVER SHEET
COVER SHEET
ENSTING CONDITIONS PLAN SHEET 1 OF 2
ENSTING CONDITIONS PLAN SHEET 2 OF 2
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FRELIMINARY CONCEPT RALM SHEET 1 OF 2
SOLI MAP Know what's below.

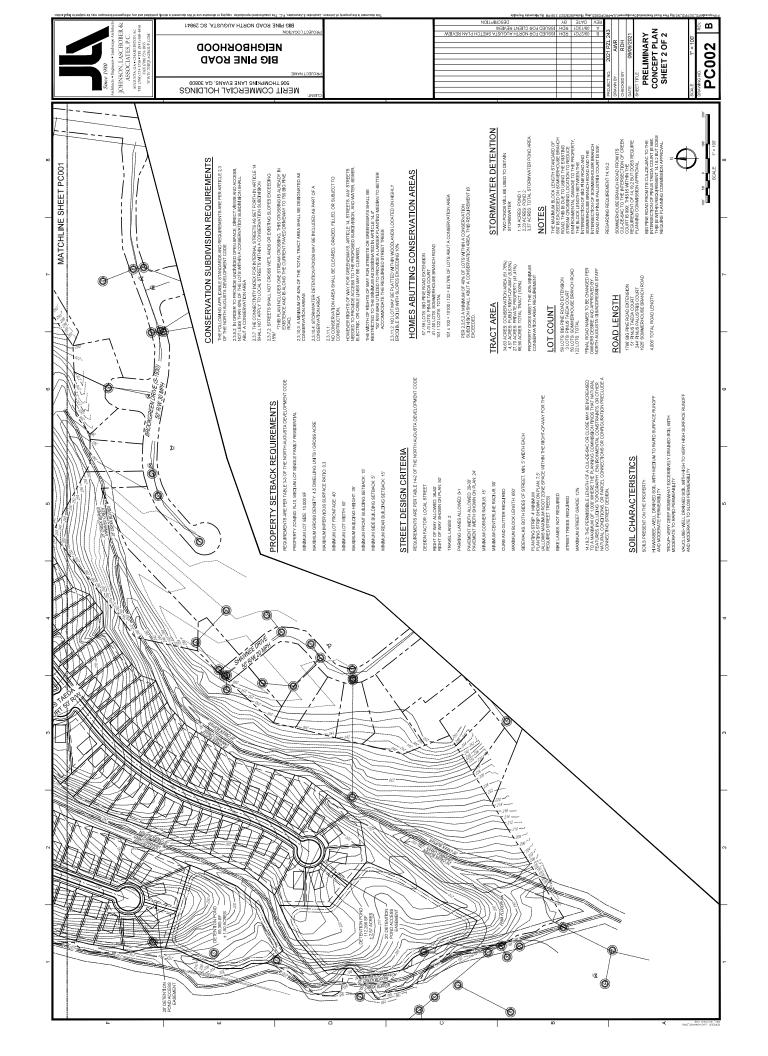
Call before you dig.

DWG. CG001 CV002 CV002 PC002 PC003











Long

ORDINANCE NO. 91-05 TO CHANGE THE CORPORATE LIMITS OF THE CITY OF NORTH AUGUSTA BY ANNEXING PROPERTY LOCATED ADJACENT TO CHANTICLEER SUBDIVISION OWNED BY BISHOP F. STRICKLAND

WHEREAS, Section 5-3-150 of the Code of Laws of the State of South Carolina provides that: "Any area or property which is contiguous to a city or town may be annexed to the city or town by filing with the municipal governing body a petition signed by seventy-five percent or more of the freeholders owning seventy-five percent or more of the assessed valuation of the real property in the area requesting annexation. Upon the agreement of the governing body to accept the petition and annex the area, and the enactment of an ordinance declaring the area annexed to the city or town, the annexation shall be complete;" and

WHEREAS, the Mayor and City Council of the City of North Augusta, by adoption of Resolution No. 91-03, dated March 4, 1991, wish to annex the below described property.

NOW, THEREFORE, BE IT ORDAINED by the Mayor and City Council of the City of North Augusta, South Carolina, in meeting duly assembled and by the authority thereof that:

The corporate limits of the City of North Augusta, South Carolina, shall be expanded by annexing the following property:

> All those pieces, parcels, or tracts of land with, improvements thereon, situate, lying and being in the County of Aiken, State of South Carolina, adjacent to the present City limits of North Augusta, containing 41.4 +/- acres, beginning at a point of intersection of the western right-of-way line of Big Pine Road and the present City limits, thence S 350 39' W 2,750 +/- feet along said City limits line, thence N 500 23' W 80 +/feet, thence N 41° 51' E 161 +/- feet, thence N 7° 6' E 181.2 +/- feet, thence N 0° , 40' E 287.7 +/- feet, thence N 50 46' E 222.10 +/- feet, thence N 110 9' E 122.3 +/- feet, thence N 00 17' W 147.4 +/- feet, thence N 230 32' E 175.1 +/- feet, thence N 380 49' E. 900.9 +/- feet, thence N 380 49' E 129.6 +/- feet, thence N 680 27' E 298.1 +/- feet, thence N 680 27' E 240.41 +/- feet, thence N 68° 50' E 380.0 +/- feet, thence S 240 44' E 236.02 +/- feet, thence S 240 44' E approximately 230.0 +/- feet along the western rightof-way line of Big Pine Road to the point of beginning.

Said property is shown on a plat identified as Exhibit "A", entitled "Plat of Property Sought to be Annexed to the City of North Augusta, South Carolina," dated February, 1991. Said property is further identified on a plat entitled "Property Located in Northwest Section of North Augusta" prepared by Joe L. Grant, dated March, 1970, from which a more complete and accurate description of the metes, bounds, and location of the property can be determined.

Said property is identified by the following Tax Map Parcel Numbers and Plat Reference Numbers.

 Plat Reference No.
 Tax Map Parcel No.

 1
 00-008-01-918

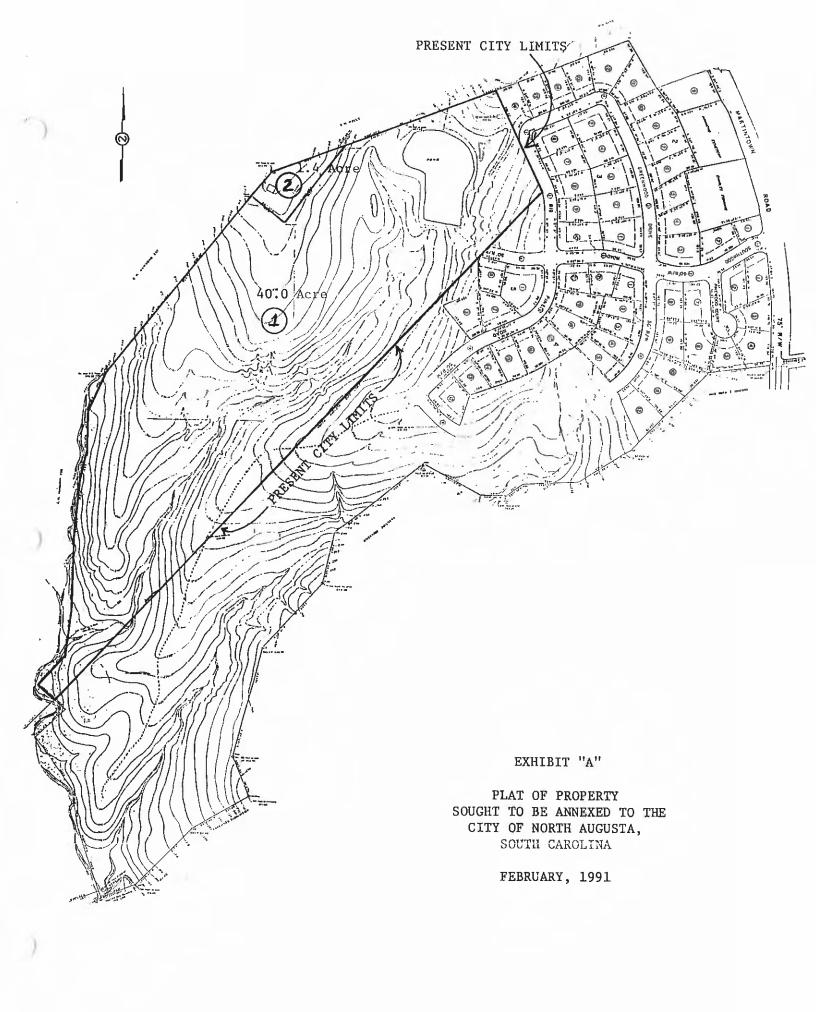
 2
 00-008-01-024

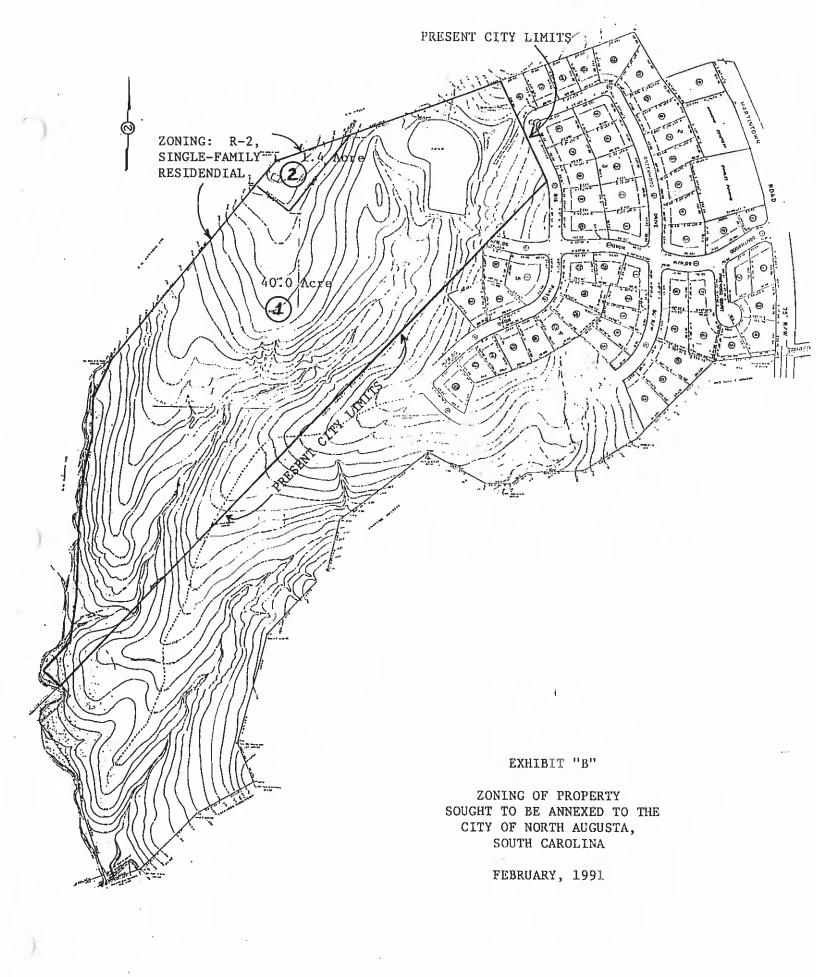
- II. In conformance with the City's Land Use & Development Plan, the property shall be zoned R-2, Single-Family Residential, under the official Zoning Ordinance of the City of North Augusta and shown on the official Zoning Map as same, as shown on a plat attached hereto marked Exhibit "B" entitled "Zoning of Property Sought to be Annexed to the City of North Augusta, South Carolina," dated February, 1991.
- III. This Ordinance shall become effective immediately upon its adoption on third reading.
- IV. All ordinances or parts of Ordinances in conflict herewith are, to the extent of such conflict, hereby repealed.

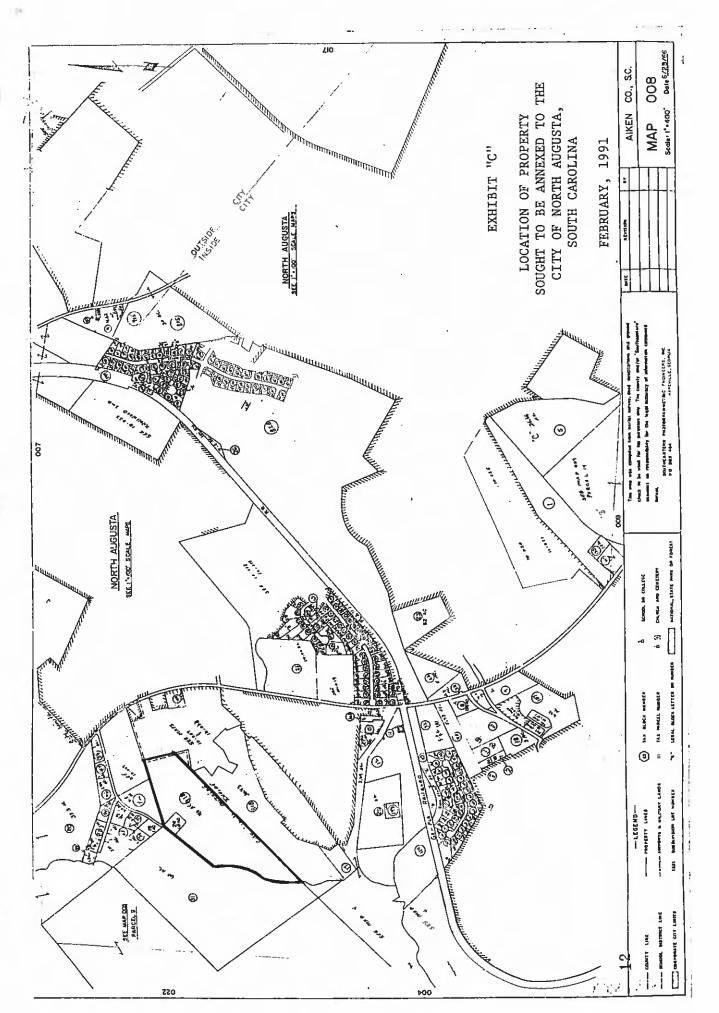
DONE, RATIFIED AND ADOPTED BY THE MAYOR AND CITY COUNCIL OF THE CITY OF NORTH AUGUSTA, SOUTH CAROLINA, ON THIS 18th DAY OF March, 1991.

First Reading 3-4-9/
Second Reading 3-4-9/
Third Reading 3-18-9/
ATTEST:

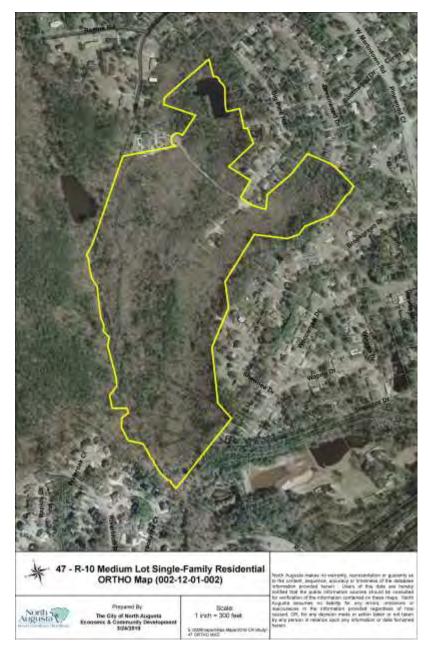
Leona J. Lewis, City Clerk







7.



Parcel Number: 002-12-01-002

Description: This 61-acre parcel is zoned Medium Lot Single-Family Residential, and it is located southwest of the Chanticleer subdivision and northeast of The Rapids subdivision. There is a pond and associated wetland on the northeastern section of the property which receives seepage, as well as drainage from homes and streets in Chanticleer. The pond drains into a streambed which crosses under Big Pine Road and flows to the south to merge with two other streams that flow along the eastern and western boundaries (see figure). The stream along the east originates with a spring that is located near the end of Greenwood Drive. The stream along the west is drainage from Hammond Pond, which is located on the adjacent parcel (#002-12-01-001). The area provides critical habitat for bottlebrush buckeye (Aesculus parviflora) and relict trillium (Trillium reliquum). Both of these are protected plant species mentioned in the Natural Resources section of the City's Comprehensive Plan for growth and development (see section 8.7, page 8-3). Portions of this parcel are also listed on the U.S. Fish and Wildlife Service's National Wetlands Inventory.

Recommendation: Development of this parcel is not recommended due to due to issues with drainage and critical wetland habitat.



Planning Commission



Minutes for the Thursday, October 21, 2021, Regular Meeting

Members of the Planning Commission

<u>Dr. Christine Crawford</u> <u>Chair</u>

Bob Bigger

Leonard Carter, Jr.

Bob Clark

Timothy V. Key

JoAnn McKie, Vice Chair

Larry Watts

CITIZEN ASSISTANCE: Individuals requiring special assistance or a sign interpreter to participate in the meeting are asked to please notify the Department of Planning and Development 48 hours prior to the meeting at 803-441-4221.

- **1.** Call to Order 7:00 p.m.
- 2. <u>Roll Call</u> Present at the meeting were Chairman Dr. Christine Crawford, commissioners Larry Watts, Bob Bigger, Bob Clark, Len Carter and Timothy Key.
- 3. Approval of Minutes October 21, 2021 Study Session and Regular Meeting
- 4. <u>Confirmation of Agenda</u> minutes were good with no changes
- 5. <u>Application MW21-003</u> Highland Springs Elementary/Middle School Landscaping Waiver—A request by Aiken County Public Schools for a waiver from the landscaping requirements of Article 10, Landscaping of the North Augusta Development Code on TPN 023-05-01-003, zoned P, Public Use.
 - a. Consideration of Application MW21-003 by Commission.
 Mr. Paradise said the school district wanted to see about some waivers on the land where school is being built. It is 51.2 acres and what the city requires for the landscape will not work for this acreage. The landscape ordnance is not designed for

50 acres. Chairman Mrs. Crawford said they would have to agree the criteria is acceptable and they will go thru each one.

Mr. Roger Davis architect for the school district presented the following things that they think will best fit for the landscape on this large piece of property.

- 1. Eliminate the small trees along Old Sudlow Lake because what you plant you have to irrigate and this site is to large. The large trees will stay as is.
- 2. Eliminate all rear buffer on lots 21 & 22 in front of Old Sudlow. There are power lines overhead and in the easement.
- 3. Eliminate the buffer planting on lot 8 near retaining wall and side because it sits 30 feet below school.
- 4. To waiver shrubs and trees leading to Old Sudlow Lake Rd. because it is an extremely long road.
- 5. Waiver to not plant trees and shrubs in back of school in parking lot. It would be too much to maintain.
- 6. Waiver to plat on street trees on the access dr.

 All the large trees will stay on property. There were no comments from anyone.

 Commissioner Larry Watts stated that it is very expensive to keep up with the care of plants and landscaping. The Aiken county schools have a hard keeping up with school grounds landscaping. It is a waste of tax payer's money to purchase landscaping due to not have enough staff to care for it. Plus, cut grass looks better than dead shrubbery. Chairman Mrs. Crawford read the 5 conditions that have to be meet to consider this plan on landscaping. Tim Key made the 1st motion and Len Carter 2nd motion and it was unanimous vote.
- 6. <u>Application PP21-003</u> Forrest Bluff, Section 1— A request by McKie Property Development, LLC for approval of a Major Subdivision Preliminary Plat for 29 single-family residential lots and 37 townhouse lots on TPNs 006-10-09-002, zoned R-7, Small Lot, Single-Family Residential.
 - a. Consideration of Application PP21-003 by Commission. Recusal from Mr. Bigger. Mr. Paradise stated is 51.53 acres for single family residential and townhouses. It was called Highland Bluff but has been changed since. The applicant has provided a traffic study and will take any questions. Mr. Jason Whinghter with Ivey Properties LLC. I'm here to answer any questions that anyone may have regarding this project. Larry Watts asked about access to the property and was told it is thru Knollwood only not another way to access. They are asking for public comments and questions. Ross Douglas brought up concerns in his neighborhood and how the new subdivision will effect it. Mr. Douglas is concerned that will it not be safe to walk, run or kids walk to school as it is now. That a traffic study was done during covid and it didn't show the real amount of traffic that the area has now. Also it would be adding more roads in the area for the neighborhood which would add more traffic. Also that the Greenway has flooding now when it

rains and if the trees are cut down it will make this worse. He wants to know why it can't be a continuing Knollwood neighborhood with fewer houses and larger lots instead of the plan they have now. He would like for everyone to consider his concerns and hope that they make the right decision for this neighborhood. Mr. Larry Hammett spoke with concerns about the elevation of the other lots and if there would be a barrier wall or privacy fences. Also concerned about the drainage problem because of the elevation on some of the lots.

Mr. Mason Raines spoke about the concerns of lot sizes. Mr. Raines compared them to trailer park lots because they are small lots. The traffic it will cause on his street Green forest would double which would create a safety concern due to the people who walk or ride bikes a lot. The concern that it would affect the Greenway and maybe it's future. Also he had that the city needs to consider the water, sewer and police coverage this area will need. In his closing remarks he asks the BZA to consider maintain the standard for Knollwood it has done for the last 30 years. Mr. Doug Melton spoke about the promise of an another exit in Knollwood and ask the commission to honor that. He is concerned about the traffic and the safety of people walking. Green forest is the street used to get to Greenway and that makes it busy now. He asked the city to deny the waiver at this time until there is another exit for Knollwood. Gena Russo she expressed her concerns with traffic with the schools and how hard it is to get out on the road now. Gena Russo thinks the traffic study done was done at a time when people were not going to school or work so it is not very accurate. Jason Whinghter is back to discuss the concerns the citizens had regarding this project. The traffic study was done by the City of North Augusta & DOT code requirements. The did adjust what was needed due to traffic being slower because of covid and people working from home. The elevation on the lots will be below and flat. There will detention ponds and retaining walls to keep flooding or water flowing into Knollwood. They will also replant to keep a buffer. The homes and townhomes will have HOA's to help maintain the grounds. The lots will be 7000 square foot as required. The discussion is to get another road to get out of neighborhood. Chairman Mrs. Crawford asked for a motion Commissioner Mr. Key gave the first motion to approve, Mr. Clark gave 2nd motion to approve and Mr. Carter gave a motion of no but 4 approved.

- 7. <u>Application CONPL21-002</u> Big Pine Subdivision— A request by JLA for a sketch plan review of a proposed Major Subdivision for 122 single-family residential lots on TPN 002-12-01-002, zoned R-10, Medium Lot, Single-Family Residential.
 - a. Consideration of Application CONPL21-002 by Commission.
 Mr. Paradise stated it is 69.9 acres proposed for a subdivision. It will have a couple of creeks and a bridge. It is an R-10 with medium lots. He has been talking with storm water division. It will also go thru another subdivision. He needs to know what his obstacles are before beginning his project. Mr. Watts asked about it being inside the

city limits. It is in city limits and comes thru at Big Pine. Alexander Reynolds spoke about the road being used is Chanticleer Rd. for subdivision. It will have a lot of an analysis open space and some left as conservation. The plan left the sensitive areas alone. It is 122 homes and R-10 zone. It fits in the development code. Only wavier is for max block link for Big Pine Rd and another connecting road. The development will have 2 cul de sacs. Mrs. Reynolds stated we don't want to cross the creek to disturb anything but it can be done if needed. There will be no development in the wetlands. The goal is to stay out of the creek and only have one crossing that being the bridge. It will be designed to what the zoning is on the property. The commissioner stated that they are still dealing with only one way in and out and said there are other subdivisions that are the same way. Chairman Mrs. Crawford stated that they are compassionate about connectivity & also traffic impact with a traffic study which they need see. Mrs. Reynolds said they wanted to get feedback on their plans before going forward. They have also looked at crossing the creek but were looking at the impact that would have on the land. Mr. Dan Holloway spoke that this project is a conservation subdivision. The area is zoned for R-10 which is houses and the lots would be 50 foot lots. But also that is connectivity is the issue they need to know before going forward with this plan. The discussion came up about townhouses being the best idea but it is not zoned for them. Mr. Paradise stated that it would need to be a R7 or R5 zoned for townhouses plus need variance for lots.

8. Staff Report

a. September Performance Report: Mr. Paradise stated that the Development rewrite was starting up. The staff was meeting with consultants. The staff would be discussing the conditional uses and maybe doing away with the. For example, if a neighborhood or highway or lake is that it is a conditional use but not really cause everything along that corridor is conditional use. Mr. Paradise stated we are looking for things to be particular to specific use. Mr. Paradise stated we are also looking to stop conditional use. By stating these are the conditions either meet them or don't. There are 5 chapters that were sent out to department heads to get their comments. This project and comprehensive plan are ongoing.

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9. Adjourn

Meeting was adjourned at 9:30pm

As Approved November 18, 2021

Respectfully Submitted,

the Punt

Thomas L. Paradise, Interim Director

Department of Planning and Development

Secretary to the Planning Commission

Department of Planning and Development



Project Staff Report

SP22-002 River Falls Apartments, Ph 2

Prepared by: Kuleigh Baker

Meeting Date: September 21, 2022

SECTION 1: PROJECT SUMMARY

Project Name	River Falls Apartments, Ph 2	
	•	
Applicant	Parker Augusta, LLC	
Engineer	ZEL/Ardurra/Cranston	
Address/Location	Off Compassion Way (FKA The Frontage Road) at West	
	Martintown Road	
Parcel Number	001-20-02-006	
Phase Development Size	± 8.71 acres	
Existing Zoning	R-5, Mixed Residential	
Overlay	N/A	
Traffic Impact Tier	2	
Proposed Use	132 Apartment units (Phase 2, 264 total units)	
Future Land Use	Mixed Use	

SECTION 2: PLANNING COMMISSION CONSIDERATION

Section 5.6 of the North Augusta Development Code (NADC) provides uniform approval procedures for site plans.

5.6.1 Purpose

The site plan review provisions and regulations of this section are intended to promote the safe, functional and aesthetic development of property and to ensure that new structures, utilities, streets, parking, circulation systems, yards and open spaces are developed in conformance with the standards of this Chapter. The site plan review considers the siting of structures and related site improvements to promote harmonious relationships with adjacent development.

5.6.2 Major and Minor Site Plans

The approval of a site plan is hereby required as a condition for the issuance of a building permit. No building permit shall be approved unless a site plan has been approved in accordance with the procedures prescribed in this section.

5.6.6 Major Site Plan Approval Procedure

Meeting Date: September 21, 2022

5.6.6.1 Generally – Approval of a major site plan is a two (2) step process. A pre-application conference is recommended. The first step is the submission of a preliminary site plan application and required information for review by the Department and the Planning Commission. The second step is the submission of a final site plan for review by the Department for compliance with the approval of the Planning Commission and other provisions of this Chapter.

5.6.6.2 Preliminary Site Plan -

- a. An application for approval of a site plan and required information shall be submitted to the Department. The Director shall determine whether the application for a preliminary site plan is complete as prescribed in Appendix B, Application Documents.
- b. If the site plan application is complete and conforms to this Chapter, the Director shall forward the application, along with conditional use permit application if applicable, to the Planning Commission within thirty (30) days of the determination of completeness. The Director's report to the Planning Commission on the application shall address compliance of the site development plan with the provisions of this Chapter, the suitability of plans proposed, and shall include a recommendation for approval or denial and any recommended waivers, conditions of approval or modifications to the site plan as submitted, if any, with reasons therefore.
- c. (omitted for brevity)
- d. A majority vote is required for the Planning Commission to approve, approve with conditions or waivers or both, if applicable, or deny a preliminary site plan application.
- e. A preliminary site plan approval by the Planning Commission must be processed and approved as a final site plan by the Director and City Engineer prior to the issuance of any building permit and before the vesting period provided for in §5.6.7.5 shall commence. (Adopt. 12-1-08; Ord. 2008-18)

5.6.6.3 Final Site Plan

After a final decision by the Planning Commission to approve a preliminary site plan and all required conditions of a conditional use permit, if applicable, the application may be processed for final site plan approval. The final site plan shall be prepared and submitted to the Director in the same manner as set forth in §5.6.6.2. If the final site plan conforms to the approval of the Planning Commission, the provisions of this Chapter and all required conditions or waivers or both, if applicable, the Director shall approve the site plan. If the final site plan is complete, but does not conform to the approval of the Planning Commission, the provisions of this Chapter and any conditions or waivers or both, if applicable, the Director shall deny the site plan and return to applicant for revision and resubmission. If the applicant disagrees with the decision of the Director, an appeal

SP22-002 River Falls Apartments, Ph 2

Prepared by: Kuleigh Baker

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may be filed in accordance with the procedures set forth in §18.4. (Rev. 12-1-08; Ord. 2008-18)

Final approval will be granted by staff when the plans are in substantial compliance with the requirements of the North Augusta Development Code and any proposed conditions.

SECTION 3: PUBLIC NOTICE

Per NADC Table 5-1, no public notice is required for a major site plan. A notice for the Planning Commission meeting was placed on the City website, www.northaugustasc.gov, on September 15, 2022.

SECTION 4: SITE HISTORY

The subject property was originally part of a Planned Development project for The Martin Group, LLC that would include self-storage units, a hotel, restaurants, retail outbuildings, and professional office buildings. The developer received a mine permit from SCDHEC in 2008 with multiple site, pond, and slope failures between 2008 and 2013. The SCDHEC mining permit was eventually terminated in 2013. The site was never developed as planned.

The property was sold in 2016 to I-20 Investors, LLC and rezoned from PD, Planned Development to R-5, Mixed Residential at the regular Planning Commission meeting of December 21, 2017 for use as an apartment complex.

The Planning Commission approved the Major Site Plan application for Phase 1 of River Falls Apartments on May 17, 2018. Some grading work has begun.

Prepared by: Kuleigh Baker

Meeting Date: September 21, 2022

SECTION 5: EXISTING SITE CONDITIONS

	Existing Land Use	<u>Future Land Use</u>	Zoning
Subject Parcel	Vacant	Mixed Use	R-5, Mixed Residential
North	I-20	Transportation	Transportation
South	Vacant	Mixed Use/Residential Single Family	PD, Planned Development
East	Commercial	Commercial	GC, General Commercial
West	Vacant	Mixed Use	PD, Planned Development

<u>Access</u> – The site currently has access from Compassion Way (FKA the Frontage Road) off of West Martintown Road

Topography – The subject property has significant slopes on site as a result of grading.

<u>Utilities</u> – Water and wastewater service to the proposed development will be provided from existing utilities along Martintown Road. The existing ten (10) inch water main and twenty-one (21) inch sanitary sewer have sufficient capacity to serve this development.

<u>Floodplain</u> – The subject property is not located within a designated floodplain as identified on the FIRM maps.

<u>Drainage Basin</u> – This site is located within the Pole Branch Drainage Basin as designated on the City of North Augusta Stormwater Management's Drainage Basin Map. The Stormwater Management Department has conducted an updated assessment of the basin and rates the overall quality as poor with water impairments found in the samples.

SECTION 6: WAIVER REQUEST

Section §5.6.6.2 states that the applicant may appeal to the Planning Commission for a waiver from a standard applicable to the site plan in accordance with §5.9.

Meeting Date: September 21, 2022

The applicant has requested a waiver from **NADC Section 11.3.1.1** which states open space shall be reserved at a ratio of one thousand twenty-four (1,024) square feet per dwelling unit for residential development, or that portion of mixed use development containing dwelling units.

An open space waiver was granted for Phase 1 of River Falls Apartments with the condition that the waiver apply only to that phase.

Per §5.9.1 Planning Commission Waivers, the Planning Commission may waive such standards where:

- 1) After obtaining the recommendation of the Director, the Planning Commission determines that the proposed waiver does not conflict with the goals and policies of the Comprehensive Plan or the purposes underlying the standard; and
 - The applicant state the waiver does not conflict with the goals and policies of the Comprehensive Plan or the purpose of the standard and that the goal of the plan is to provide useful and useable open space for the public. The site is not conductive to useable open space, especially in the Phase 2 area.
 - Staff notes that a waiver was granted for Phase 1 due to the same site constraints.
- 2) The applicant demonstrates, through documentation and/or studies, based on generally accepted engineering principles, that adherence to the standard provided by this Chapter would pose a threat to health and safety or would undermine a policy set forth in the Comprehensive Plan or the purposes underlying the standard; and
 - The applicant states that adherence to the standard could pose a threat to the health, safety and welfare of the public by expecting residence to traverse a steep and impractical existing slope. The applicant also states that use of the open space in this area could destabilize the slope and cause significant soil erosion.
 - Staff notes that there are significant slope issues on site that have been identified through the Stormwater review process. The available land on site is being utilized for Stormwater management.
- 3) The applicant consents to an alternative standard, and the Planning Commission finds that such standard is consistent with the Comprehensive Plan, will protect the public health, safety and general welfare, and is consistent with the purposes underlying the standard; and

SP22-002 River Falls Apartments, Ph 2

Prepared by: Kuleigh Baker

Meeting Date: September 21, 2022

The applicant will include as much open space as shown on the submitted site plan and enhance landscaping where possible.

4) The economic burden imposed on the applicant to comply with the generally applicable standard outweighs the public purpose for such standard; and

The applicant states that underground detention is a possibility with significant cost and feasibility implications and that the financial burden would eliminate the benefit of the development of an apartment complex for varied housing stock.

Staff notes that the economic burden is not the primary purpose of this application through strict adherence to the standard reduces the amount of land that may be profitably developed.

5) Compliance with the generally applicable standard is impracticable due to unique topographical or other site conditions.

The applicant states that the site has severe slopes and the useable land is required for Stormwater management. The required location of the stormwater treatment area has increased slopes on site and those slopes are unsuitable for open space as described in the NADC.

Staff notes that there are significant slopes on the Western portion of the site that limit development.

SECTION 7: STAFF EVALUATION AND ANALYSIS

- 1) Multi-family residential uses are permitted within the R-5, Mixed Residential zoning district.
- 2) The future land use classification for the site is Mixed Use. The proposed use is appropriate for the future land use classification.
- 3) The site plan proposes access from Compassion Way (FKA the Frontage Road). The current proposed access drive exceeds the expected trip generation of the multi-family use. Traffic mitigation plans have been reviewed by SCDOT and will be required prior to final staff approval.

SP22-002 River Falls Apartments, Ph 2

Prepared by: Kuleigh Baker

Meeting Date: September 21, 2022

- 4) The maximum number of proposed multi-family units anticipated for this development is 264.
- 5) Parking calculations for the proposed multi-family development must be a minimum 1.5 parking spaces per unit. The developer has indicated through the site plans that parking will be designated in lots surrounding each apartment building. One guest parking spot per every 4 units is required. Parking for the club house is required at the rate of 1 space per 300 sf. The total required parking for the development is 470 spaces. The minimum required parking has been provided.
- 6) The sample architectural elevations provided for the proposed detached multi-family units are included in the attached backup. The materials appear to be horizontal siding (unclear if vinyl or fiber/cementious), wood accents and glass windows. The materials are appropriate for residential structures.
- 7) The final landscape plan must comply with the development standards for screening, buffering and street trees as specified in Article 10, Landscaping, in the NADC. The final, detailed landscape plan will require details regarding the species and buffer points for the individual buffer areas to confirm compliance with the development standards. A waiver is requested for the open space requirements for Phase 2. A waiver was granted by the Planning Commission for Phase 1.
- 8) The Stormwater management department must approve the sediment and erosion control plans. The applicant must satisfactorily resolve the discharge of the captured stormwater on the site and appropriately treat the storm water (water quality) on site as part of the final site plan.
- 9) Staff recommends approval of the site plan and waiver request assuming all other development code standards are met.

Project Staff Report

SP22-002 River Falls Apartments, Ph 2

Prepared by: Kuleigh Baker

Meeting Date: September 21, 2022

SECTION 8: ATTACHMENTS

Aerial Map
Topography
Current Zoning
Future Land Use
Application Materials
Site Plans
Waiver Request
Traffic Impact Analysis

cc Parker Augusta, LLC, via email

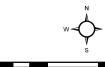
ZEL/Ardurra, via email

Cranston Engineering Group, PC, via email

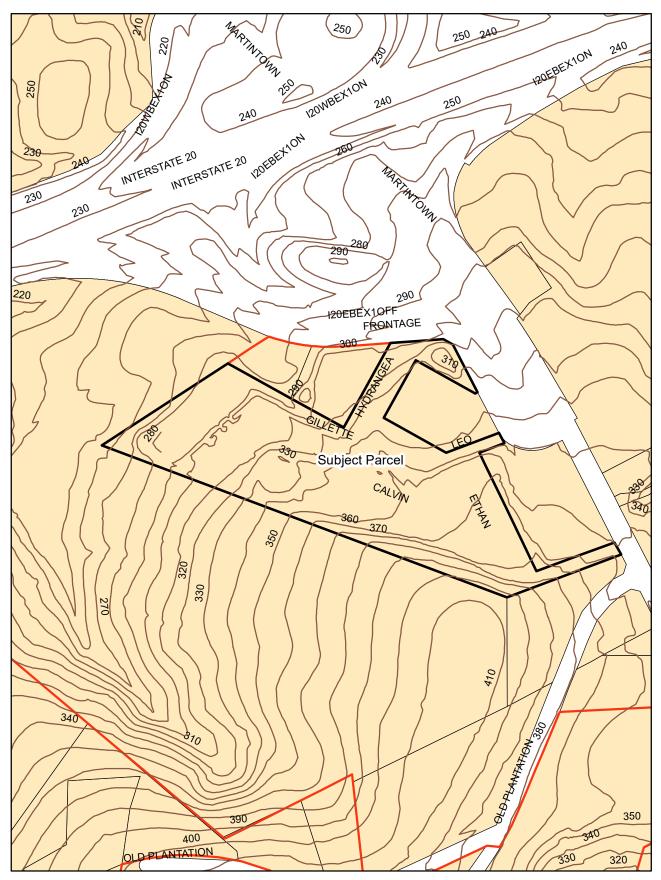




Aerial Map SP22-002 River Falls Ph 2 Approx. 16 ac zoned R-5, Mixed Residential

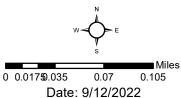


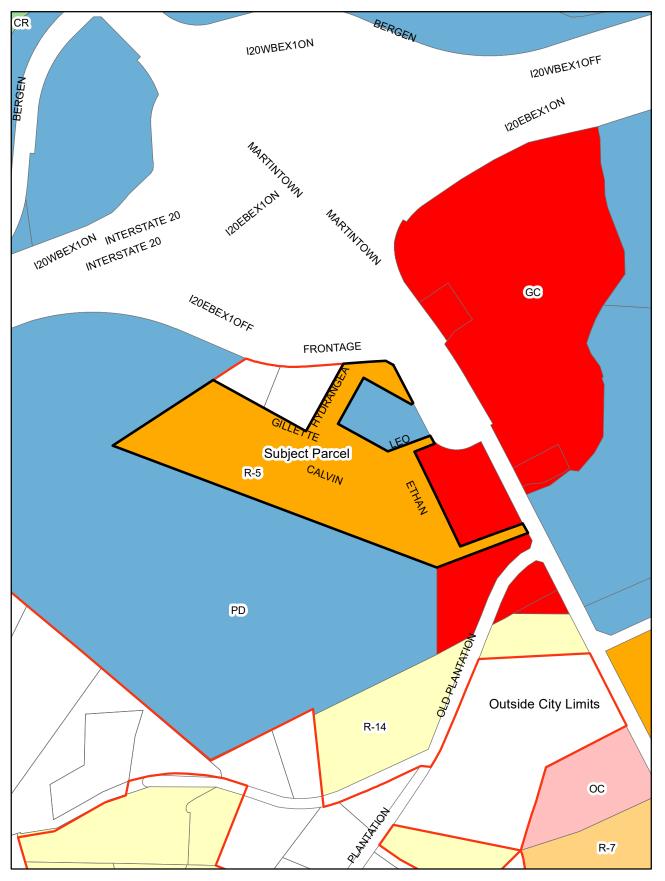
0 0.02750.055 0.11 0.10 Date: 9/12/2022





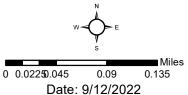
Topography Map SP22-002 River Falls Ph 2 Approx. 16 ac zoned R-5, Mixed Residential







Zoning Map SP22-002 River Falls Ph 2 Approx. 16 ac zoned R-5, Mixed Residential



Application for Development Approval

Please type or print all information



	Staff Use	
Ap	plication Number	Date Received
Review Fee Date Paid		Pate Paid
1.	Project Name River Falls Apartments Phase II	
	Project Address/Location Off of Frontage Road @ I-20, Exit 1	
	Total Project Acreage 8.71 Acres Cur	rent Zoning R-5
	Tax Parcel Number(s) 001-20-02-006	
2.		plicant Phone 645-532-2453
	Mailing Address 10 East 53rd Street, 18th Floor	
	City New York ST NY Zip 10022	Email bill@capefearcommercial.com
	Is there a Designated Agent for this project? $\frac{X}{Y}$ Yes If Yes, attach a notarized Designation of Agent form. (require	No ed if Applicant is not property owner)
4.	Engineer/Architect/Surveyor Jonathan Heald	License No. <u>23970</u>
	Firm Name Zimmerman, Evans and Leopold, Inc. Firm	Phone 843-318-1807
	Firm Mailing Address 973 Broad St. Suite A	
		Email jheald@ardurra.com
	Signature Jonathan W Heald, PE Digitally signed by Jonathan W Heald, PE Date: 2022.06.24 13:05:05 -04'00' Date	<u>06/24/2022</u>
5.	Is there any recorded restricted covenant or other private agree prohibits the use or activity on the property that is the subject of (Check one.)	· · · · · · · · · · · · · · · · · · ·
6.	In accordance with Section 5.1.2.3 of the North Augusta Deve of North Augusta review the attached project plans. The do Augusta, as outlined in Appendix B of the North Augusta Develoreview for completeness. The applicant acknowledges that all complete to initiate the compliance review process.	ocuments required by the City of North opment Code, are attached for the City's
7.		06/24/2022
	Applicant or Designated Agent Signature Kenneth Wardenski	Date
	Print Applicant or Agent Name	

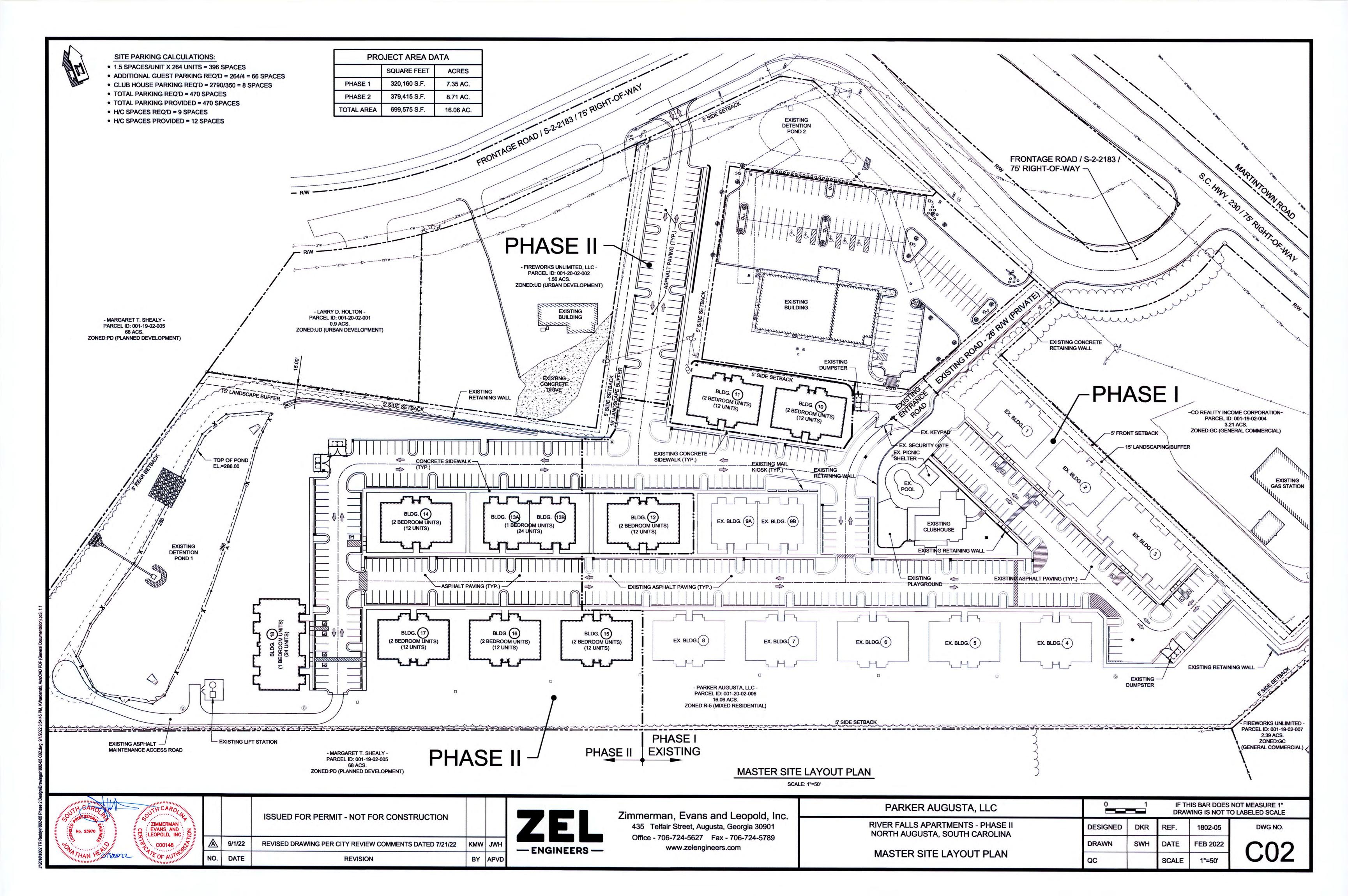
Designation of Agent

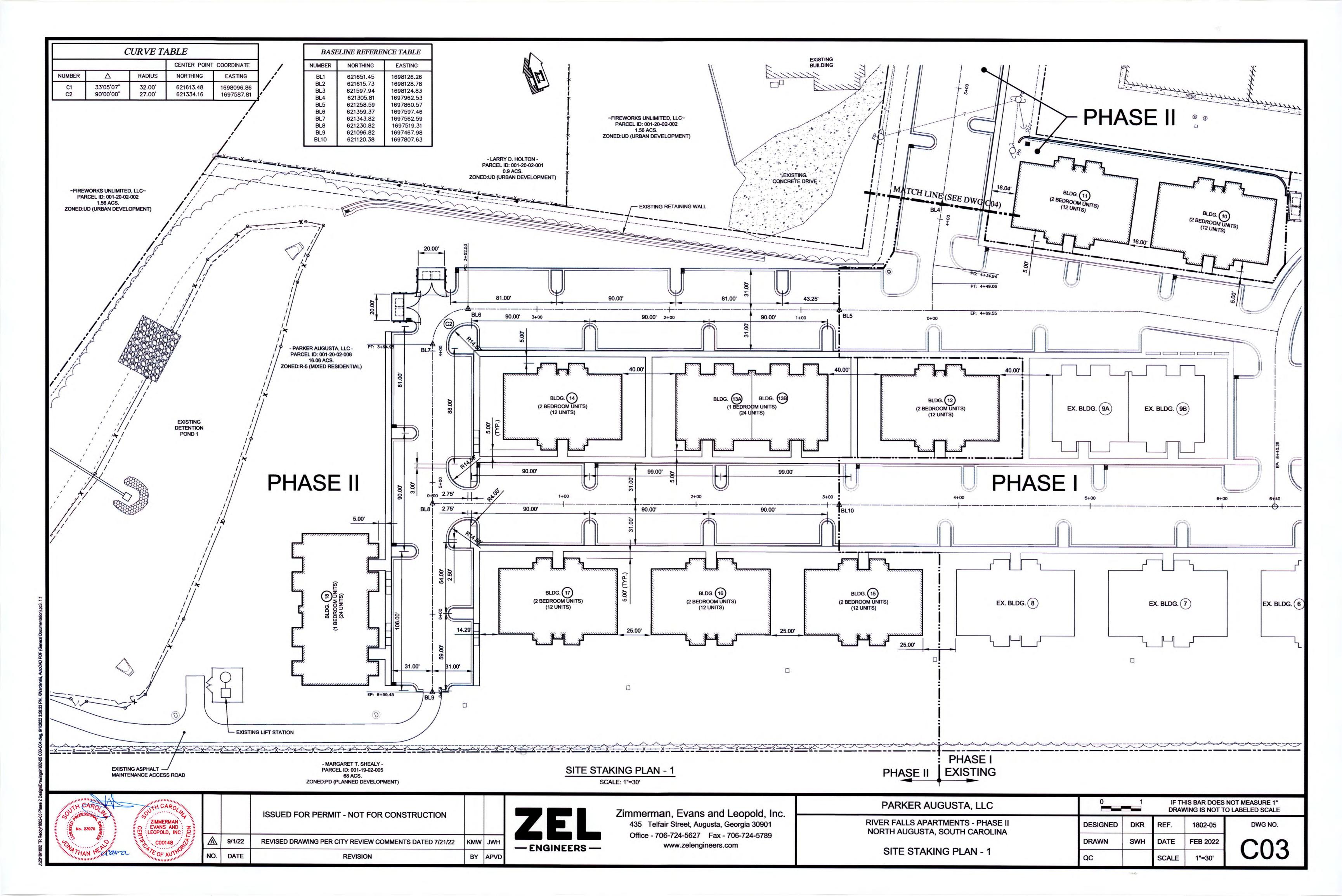
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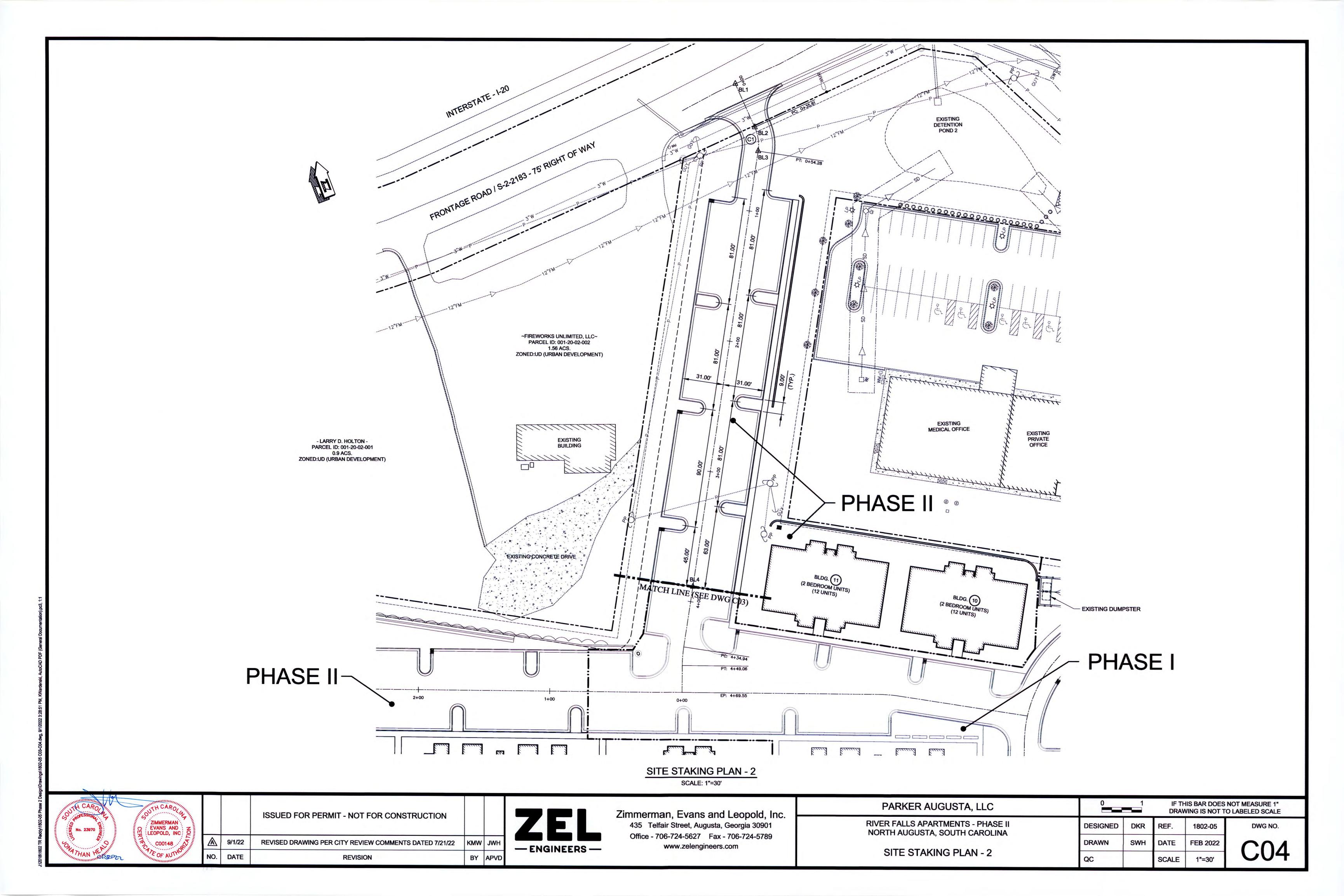


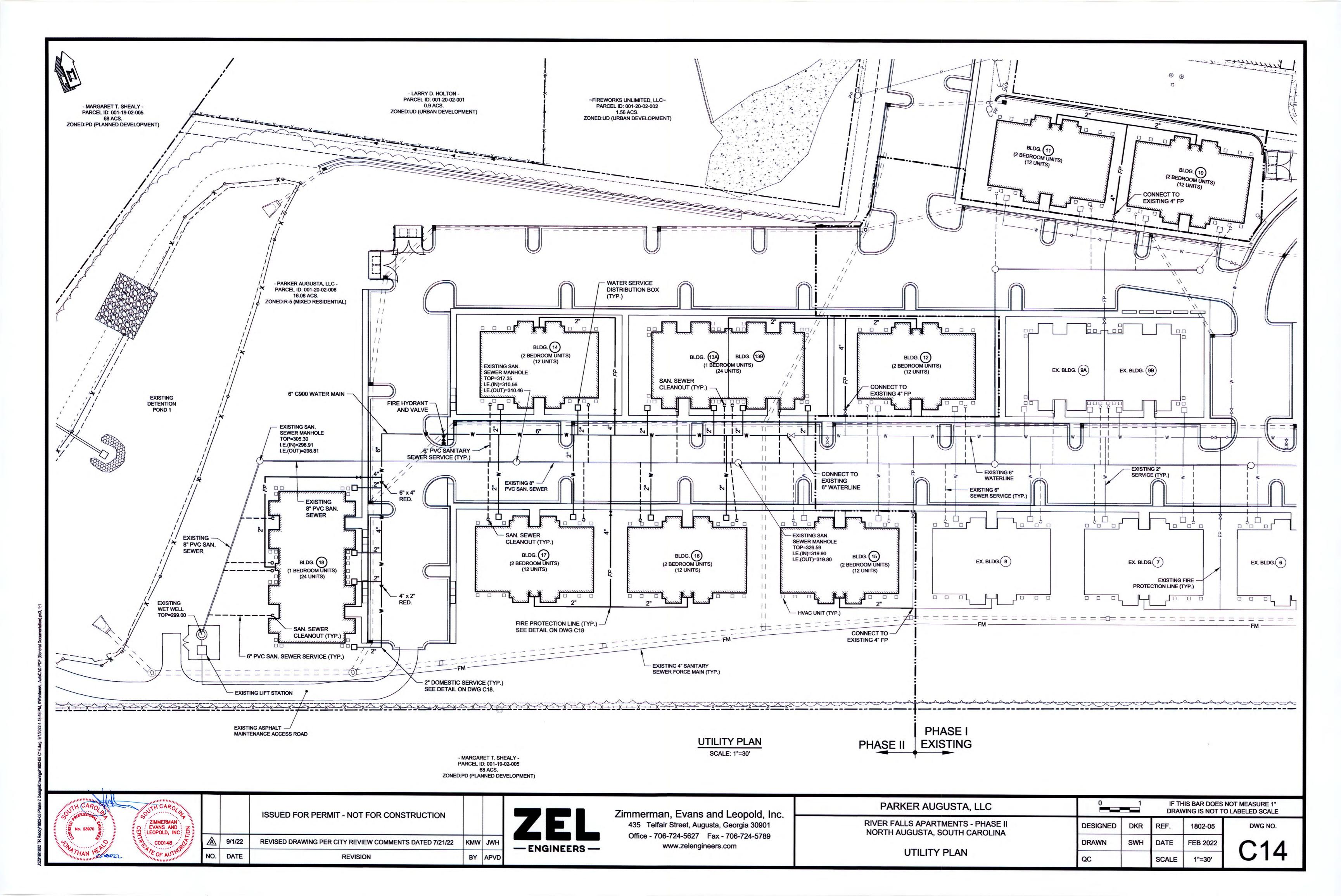
This form is required if the property owner is not the applicant.

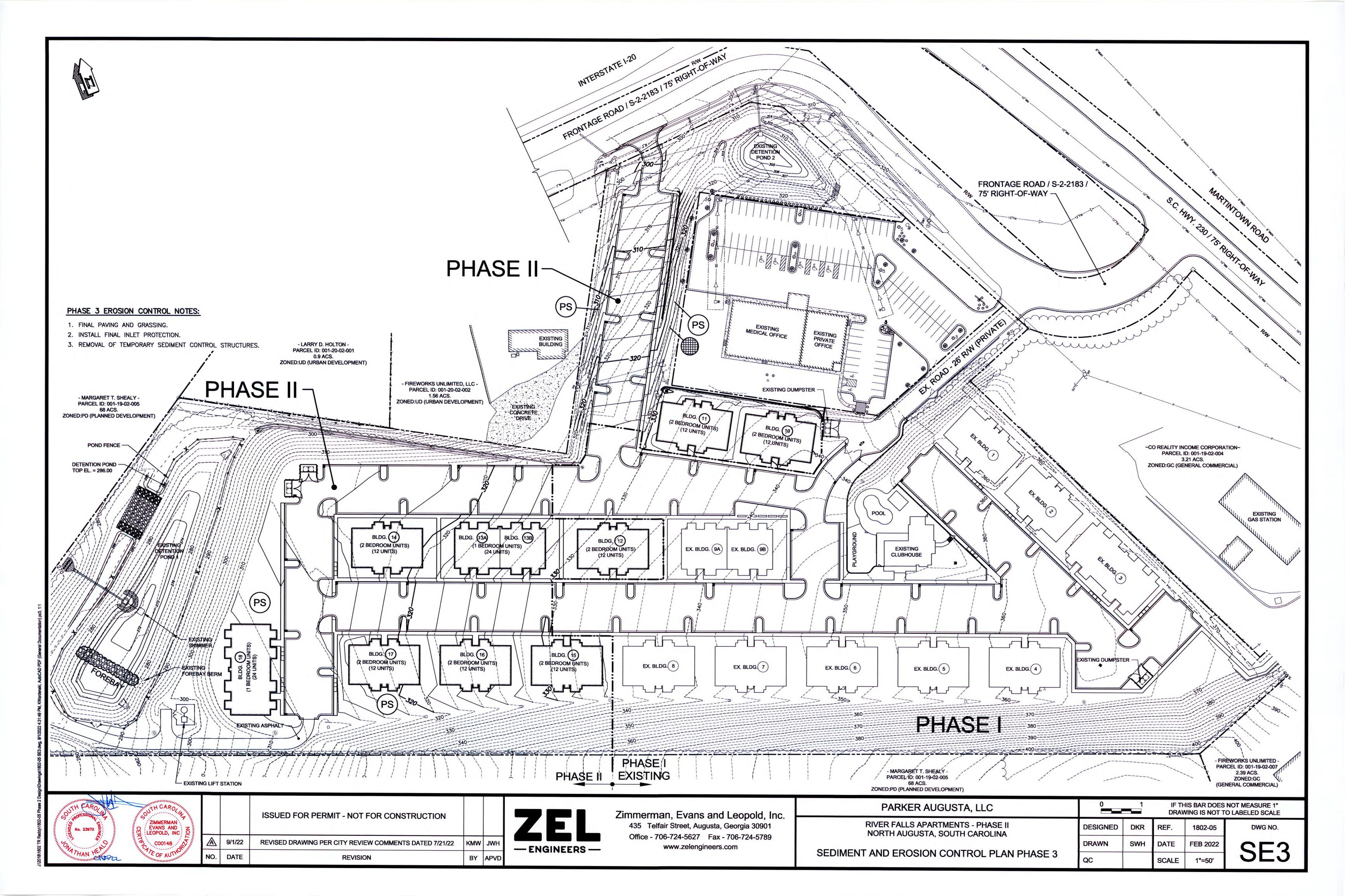
	Staff Use Only				
Ар	plication Number Date Received				
1. Project Name River Falls Apartments Phase II					
	Project Address/Location Off of Frontage Road at I-20, Exit 1				
	Project Parcel Number(s) 001-20-02-006				
2.	Property Owner Name Parker Augusta, LLC Owner Phone 645-532-2453				
	Mailing Address 10 East 53rd Street, 18th Floor				
	City New York st NY zip 10022 Email bill@capefearcommercial.com				
3.	Designated Agent Kenneth Wardenski				
	Relationship to Owner Engineering Consultant				
	Firm Name Zimmerman, Evans and Leopold, Inc. Phone 706-394-2404				
	Agent's Mailing Address 973 Broad St. Suite A				
	City Augusta ST GA Zip 30901 Email kwardenski@ardurra.com				
	Agent's Signature Semett Wardert Date 06/21/2022				
4.	I hereby designate the above-named person (Line 3) to serve as my agent and represent me in the referenced application.				
	Owner Signature $\frac{6/21/22}{Date}$				
5.	Sworn and subscribed to before the on this 24 day of June, 20 25.				
	Notary Public KARLA M. WESTPHAL Notary Public Commission Explanation Explan				











Application for Development Approval

Please type or print all information



Staff Use
Application Number <u>SP22-002</u> Date Received <u>9-7-22</u>
Review Fee 50.00 Date Paid 9-7-22
1. Project Name PIVER FAUS PH. 2
Project Address/Location 1/22 W MAPTINTOWN POAD
Total Project Acreage 16.06 Current Zoning 2-5
Tax Parcel Number(s)
2. Applicant/Owner Name CRANSTON Applicant Phone 706 840 3076
Mailing Address 452 Eugs 57 Eug
City AUGUSTA ST GA Zip 3090 Email LCHEELY @ CRANSTONENO WELL (No.CA
3. Is there a Designated Agent for this project? Yes No If Yes, attach a notarized Designation of Agent form. (required if Applicant is not property owner)
4. Engineer/Architect/Surveyor CPANSTON License No. 1392
Firm Name LANCE CHELY 7 Firm Phone 766 840 3076
Firm Mailing Address 452 EUIS ST.
City AUGUSTA ST GA ZIP 3090 Email _ CHEELY @ CHANSTON ENGINE
Signature 2 Date 9/6/2022
5. Is there any recorded restricted covenant or other private agreement that is contrary to, conflicts with or
prohibits the use or activity on the property that is the subject of the application? (Check one.) yes no
6. In accordance with Section 5.1.2.3 of the North Augusta Development Code, I hereby request the City of North Augusta review the attached project plans. The documents required by the City of North Augusta, as outlined in Appendix B of the North Augusta Development Code, are attached for the City's review for completeness. The applicant acknowledges that all required documents must be correct and complete to initiate the compliance review process.
7. Java - Cheer 9/6/2022
Applicant or Designated Agent Signature Date
LANCE CHEELY Print Applicant or Agent Name

Designation of Agent

Please type or print all information



This form is required if the property owner is not the applicant.

	Staff Use Only
Αŗ	oplication Number <u>SP22-002</u> Date Received <u>9-7-22</u>
1.	Project Name River Falls Apts Phase II
	Project Address/Location 1122 W Martintown Road
	Project Parcel Number(s) 001-20-02-006
2.	Property Owner Name Parker Augusta LLC Owner Phone 910-880-0063
	Mailing Address 10 east 53rd Street, 18th Floor
	City New York ST NY Zip 10022 Email bill@capefearcommercial.com
3.	Designated Agent Lance Cheely
	Relationship to Owner Consultant
	Firm Name Cranston Engineering Phone 706-288-3022
	Agent's Mailing Address 452 Ellis Street
	City Augusta ST GA Zip 30901 Email Icheely@cranstonengineering.com
	Agent's Signature Date 9/6/2022
4.	I hereby designate the above-named person (Line 3) to serve as my agent and represent me in the referenced application.
	1/2/2022
	Owner Signature Date 9/7/2022 Date Sworn and subscribed to before me on this day of Sevender 20 22
5.	Sworn and subscribed to before me on this day of
	Notary Public KARLA M. WESTPHAL
	Notary Public Commission Expression Expressi



CranstonEngineering.com

452 Ellis Street Augusta, Georgia 30901 PO Box 2546 Augusta, Georgia 30903 706.722.1588

September 6, 2022

North Augusta Planning and Zoning 100 Georgia Avenue North Augusta, SC 29841

Attn: Mr. Tommy Paradise

RE: River Falls Phase Two

North Augusta, SC

Cranston File No.: 2022-0001

Dear Mr. Paradise:

On behalf of the owner, Cranston requests a waiver from the open space requirement from NADC 11.3.1.1 based on the following criteria.

- 5.9.1.1 After obtaining the recommendation of the Director, the Planning Commission determines that the proposed waiver does not conflict with the goals and policies of the Comprehensive Plan or the purposes underlying the standard.
 - a. The proposed waiver does not conflict with the goals of the Comprehensive Plan. The goal of the plan is to provide useful and useable open space for the public. This site is not conducive to useable open space, especially in the phase two area. A waiver was granted for phase one, likely due to the same issues.
- 5.9.1.2 The applicant demonstrates, through documentation and/or studies, based on generally accepted engineering principles, that adherence to the standard provided by this Chapter would pose a threat to health and safety or would undermine a policy set forth in the Comprehensive Plan or the purposes underlying the standard; and
 - b. Adherence to the standard could pose a threat to health, safety, and welfare of the public in two ways. First, the public would be expected to transverse a steep and impractical existing slope to use the portion of the site that would be left. Second, the use of the open space in this area could destabilize the slope and cause a source of significant soil erosion.

River Falls Phase Two September 7, 2022 Page 2 of 2

- 5.9.1.3 The applicant consents to an alternative standard, and the Planning Commission finds that such standard is consistent with the Comprehensive Plan, will protect the public health, safety and general welfare, and is consistent with the purposes underlying the standard; and
 - c. The applicant will include as much open space as shown on the submitted site plan and consider enhanced landscape where possible.
- 5.9.1.4 The economic burden imposed on the applicant to comply with the generally applicable standard outweighs the public purpose for such standard; and
 - d. To be compliant with the applicable standard the owner would have to develop the site at a lesser density to provide the amount of open space required. Another option would be for the site to use underground detention to treat stormwater leaving the detention pond area for open space. This too has significant cost and feasibility implications. Either instance of financial burden could eliminate the benefit of the development to the Owner and terminate the project leaving the area with less housing options.
- 5.9.1.5 Compliance with the generally applicable standard is impracticable due to unique topographical or other site conditions.
 - e. This site is not conducive to useable open space, especially in the phase two area. The site slopes off severely and the useable land is required for stormwater treatment. The required location of the stormwater treatment area makes the slopes even steeper and more unsuitable for open space as described in the NADC.

We respectfully request that the Planning Commission approve the development with a waiver from the open space requirement as stated in NADC 11.3.1.1.

Sincerely,

CRANSTON LLC

Lance Cheely, PLA, MBA

PLANT CALCULATIONS **BUFFER 2:** TYPE-B (15' WIDTH) LENGTH- L' POINTS REQUIRED: 0.7/LF * 400'=280 TREES REQUIRED: LARGE: 1+ L/50 =9 SMALL: 1+ L/50 = 9 PROVIDED: @10 PTS 90 PTS 9 L.T. @ 5 PTS 9 S.T. 45 PTS + 58 SHR. @ 2.5 PTS 145 PTS 280 PTS **BUFFER 3:** TYPE-B (15' WIDTH) LENGTH- L' POINTS REQUIRED: 0.7/LF * 369'=258 TREES REQUIRED: LARGE: 1+ L/50 =8 SMALL: 1+ L/50 = 8 PROVIDED: 8 L.T. @10 PTS 80 PTS @ 5 PTS 40 PTS 8 S.T. + 66 SHR. @ 2.5 PTS 165 PTS 285 PTS **BUFFER 4:** TYPE-B (15' WIDTH) LENGTH- L' POINTS REQUIRED: 0.7/LF * 304'=213 TREES REQUIRED: 1+ L/50 =7 SMALL: 1+ L/50 = 7 PROVIDED: 7 L.T. @10 PTS 70 PTS @ 5 PTS 35 PTS 7 S.T. @ 2.5 PTS 108 PTS + 43 SHR. 213 PTS **BUFFER 5**: TYPE-B (15' WIDTH) LENGTH- L' POINTS REQUIRED: 0.7/LF * 249'=174 TREES REQUIRED: LARGE: 1+ L/50 =6 SMALL: 1+ L/50 = 6 PROVIDED: 6 L.T. @10 PTS 60 PTS 6 S.T. @ 5 PTS 30 PTS 84 PTS + <u>34 SHR</u>. <u>@ 2.5 PTS</u> 174 PTS STREET BUFFER TYPE-B (15' WIDTH) LENGTH- L' POINTS REQUIRED: 0.7/LF * 150'=105 TREES REQUIRED: LARGE: 1 + 1/60 = 3

SMALL: 1 + 1/40 = 4SHRUB: 1+ 1/5=31

PARKING LOT: 1 LARGE TREES, 2 SMALL TREES, AND 8 SHRUBS PER 10 PARKING SPACES 220 PARKING SPACES PROVIDED

REQUIRED:

22 LARGE TREES 44 SMALL TREES 176 SHRUBS REQUIRED

PROVIDED:

32 LARGE TREES , 44 SMALL TREES, 210 SHRUBS

PARKING LOT PERIMETER:

1 SMALL TREE / 40 LF 1 SHRUB / 5 LF

1 LARGE TREE / 60 LF (ADJACENT TO STREET ONLY)

TREE CANOPY:

REQUIRED:

NET LOT AREA: 360, 588 TOTAL LOT SF - 48,720 SF BLDG 20% CANOPY REQUIREMENT: 62,373 SF

EXISTING CANOPY CREDIT: 32,845 SF LARGE TREE CREDIT: 400 SF EA. X 60 TREES= 24,000 SF

SMALL TREE CREDIT: 200 SF EA. X 118 TREES= 23,600 SF

PROVIDED:

80,445 SF CANOPY PROVIDED

BUILDING PERIMETER PLANTINGS:

1 SHRUB / 5 LF

OPEN SPACE (TABLE 11-1):

REQUIRED:

1,024 SF/UNIT*132= 135,168 SF

EDUCATION FOOD SALES 89 FOOD SERVICE **HEALTH CARE** 168

LODGING RETAIL AND SERVICE OFFICE

225 PUBLIC ASSEMBLY RELIGIOUS WORSHIP WAREHOUSE AND STORAGE 50

OTHER

22,113 SF NATURAL AREAS WAIVER REQUIRED

EXTERIOR SEATING:

REQUIRED:

3,215 SF X 1 LF OF SEATING/ 50 SF OPEN SPACE = 64 LINEAR FOOT OF EXTERIOR SEATING

3,215 SF OPEN SPACE- PLAYGROUND (PREVIOUS PHASE)

L102

PROVIDED:

L101

11 BENCHES X 6 FEET PER BENCH = 66 LF EXTERIOR

SEATING PROVIDED (BY OWNER)

L104

BUFFER 2-TYPE 'B' 400 LF

BUFFER 1-DESIGNED IN PH. 1

Thuja plicata Existing Western Red Cedar LARGE TREES | COMMON NAME BOTANICAL NAME CONT. CAL. HEIGHT American Elm Ulmus americana `Princeton` B&B 3"Cal 14`-18` Eastern Red Cedar Juniperus virginiana 3"Cal 14`-18` Wynstar Willow Oak Quercus phellos 'QPMTF' TM B&B 3"Cal 14`-18` SMALL TREES | COMMON NAME BOTANICAL NAME CONT. CAL. HEIGHT Emerald Knight Fringetree Chionanthus virginicus `Emerald Knight` B & B 2"Cal 8` MIN. Eriobotrya japonica 2"Cal 8' MIN. Wax Myrtle Myrica cerifera B & B 2"Cal 8' MIN. BOTANICAL NAME SIZE HT. SPREAD SPACING SHRUBS COMMON NAME Blue Cascade Distylium Distylium x 'PIIDIST-II' TM 3 gal 48" o.c. 3 gal Chinese Fringe Flower Loropetalum chinense 24" o.c. Flirt Heavenly Bamboo 3 gal 18" o.c. Nandina domestica 'Murasaki' TM Illicium parviflorum 7 gal 72" o.c. Lemon Lime Heavenly Bamboo 3 gal 18" o.c. Nandina domestica 'Lemon Lime' Nellie R. Stevens Holly Ilex x 'Nellie R. Stevens' 7 gal 48" o.c. Muhlenbergia capillaris Pink Muhly Grass 3 gal 36" o.c. 237 Viburnum suspensum 7 gal 60" o.c. Sandankwa Viburnum Shishigashira Camellia Camellia hiemalis 'Shishigashira' 3 gal 42" o.c. Osmanthus fragrans 15 gal 60" o.c. Sweet Olive Variegated Japanese Pittosporum | Pittosporum tobira 'Variegata' 3 gal 60" o.c. Vintage Jade Distylium Distylium x 'Vintage Jade' 3 gal 36" o.c.

BOTANICAL NAME

CONT.

CAL. HEIGHT

PLANT SCHEDULE

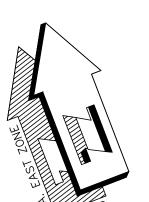
COMMON NAME

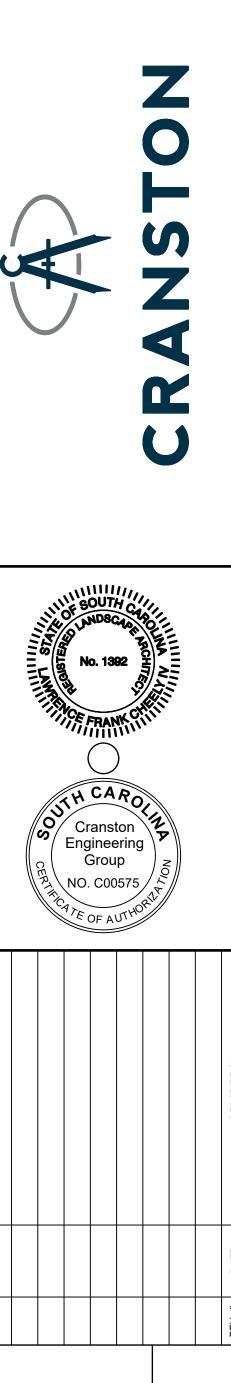
REFER	REFERENCE NOTES SCHEDULE			
SYMBOL	DESCRIPTION	QTY	DETAIL	
1	Parking Spaces	220		
	PLANTING ACCESSORIES			
SYMBOL	DESCRIPTION	QTY	DETAIL	
32-95	Sod-Bermuda	16,778 sf	5/L-201	
	INTERIOR PLANTS AND PLANTERS			
SYMBOL	DESCRIPTION	QTY	DETAIL	
32-98	Mulch, Hardwood	244.65 cy		

HORIZONTAL SCALE 1"=100' SCALE IN FEET

L103

GENERAL NOTES: 1. NOTES 2. NOTES 3. MORE NOTES





PHASE FPLAN RIVER FALLS P

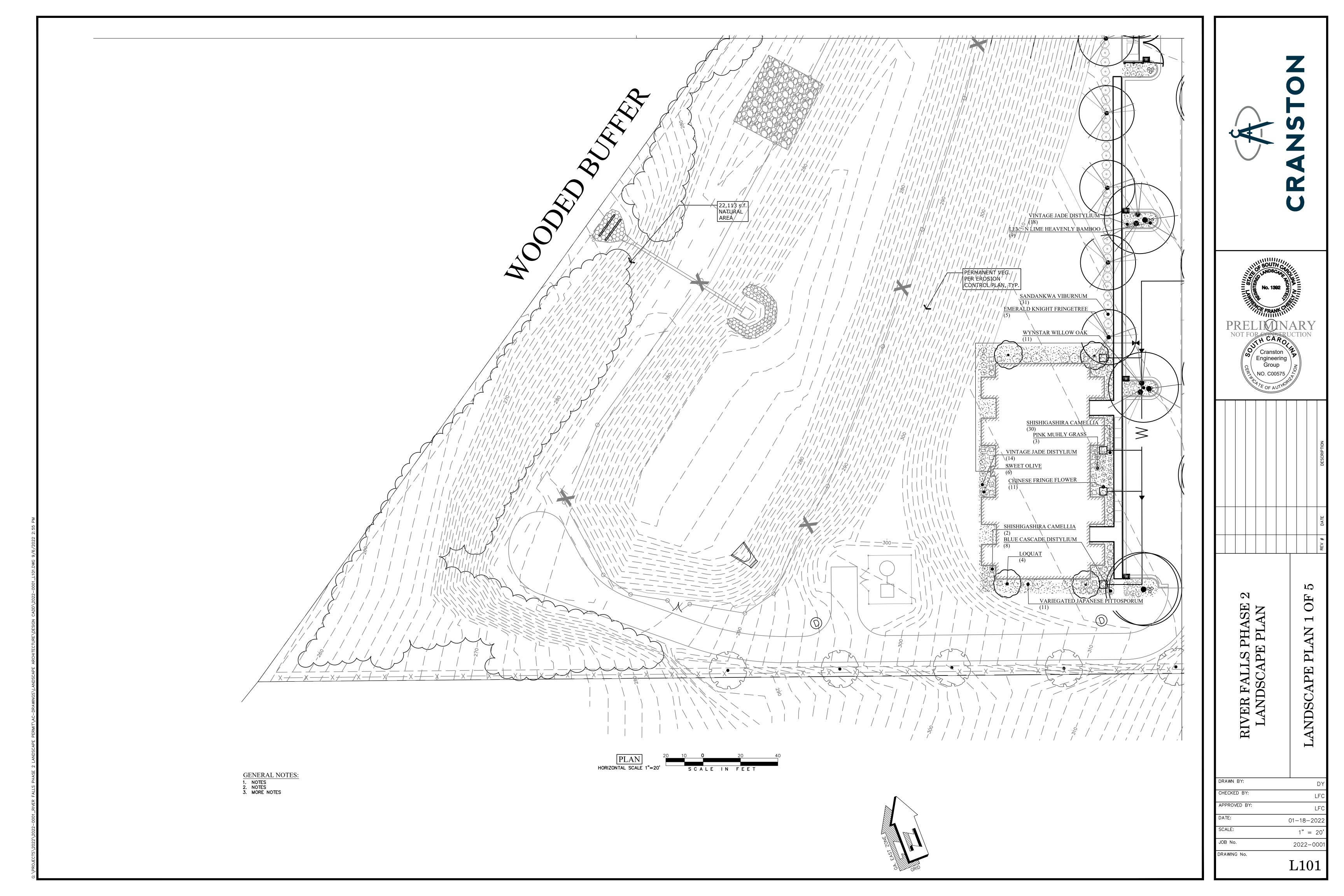
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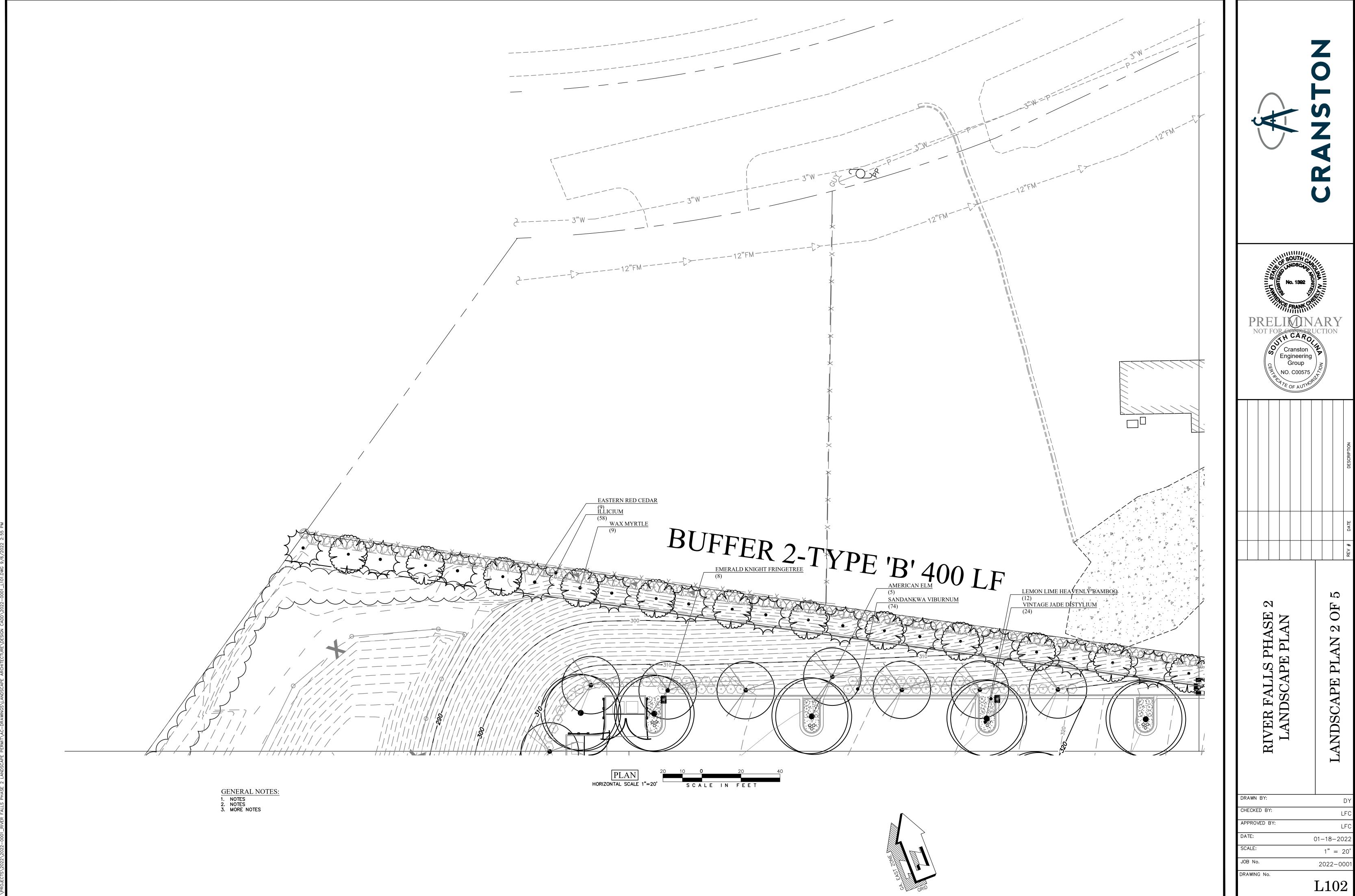
CHECKED BY: APPROVED BY: 01-18-202 SCALE: 1" = 100

DRAWING No.

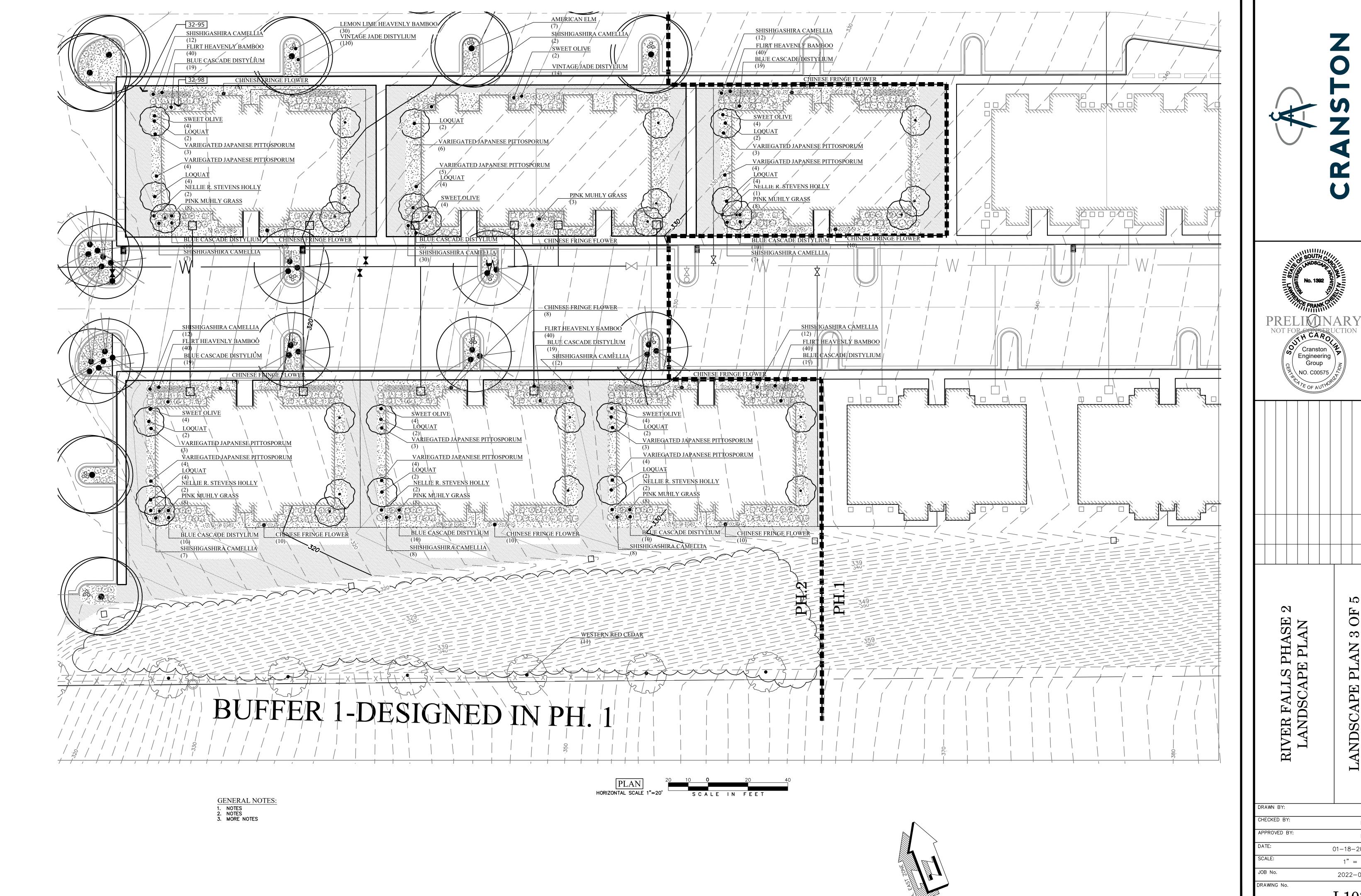
L100

2022-000





BY:	DY
ED BY:	LFC
VED BY:	LFC
(01-18-2022
	1" = 20'
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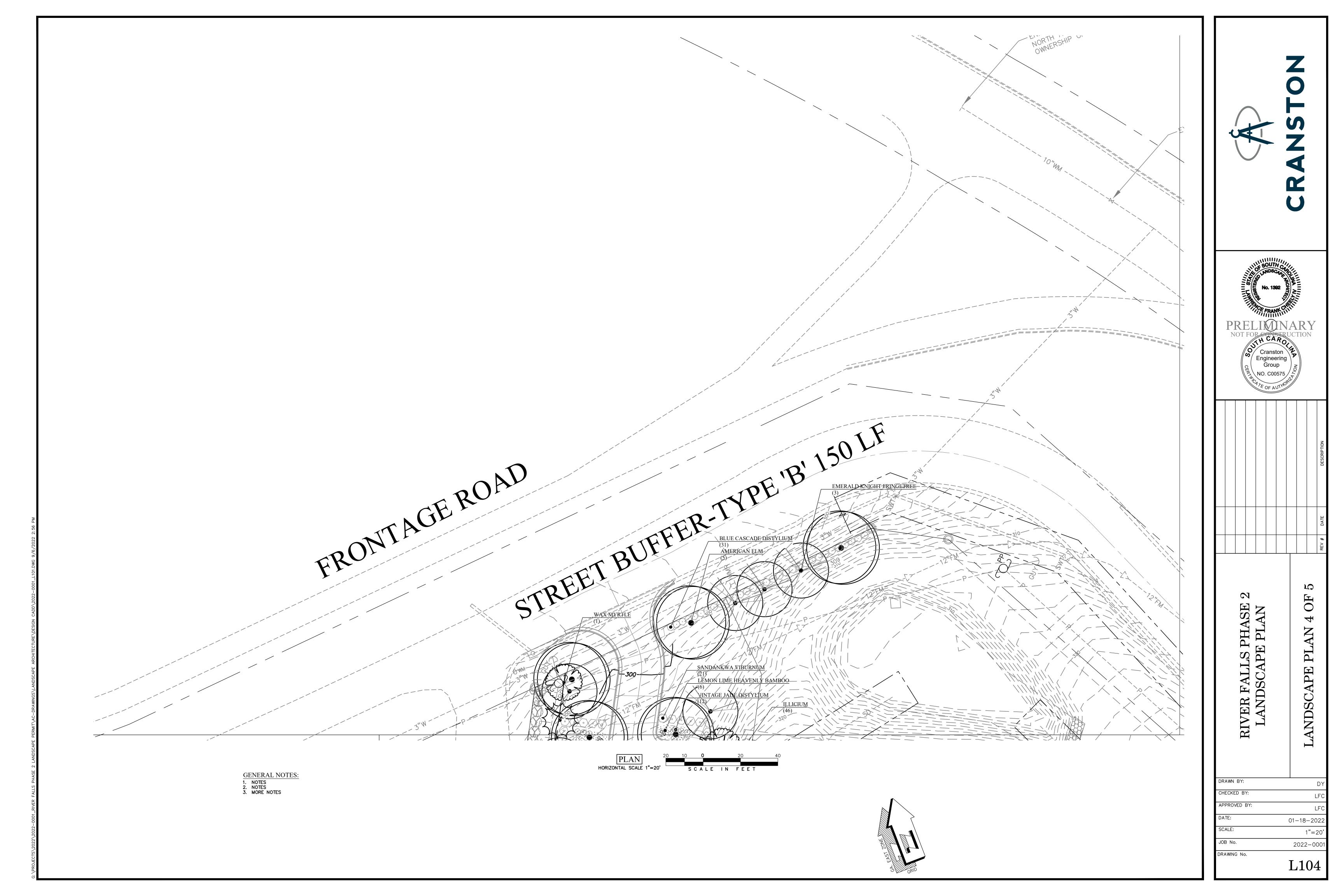


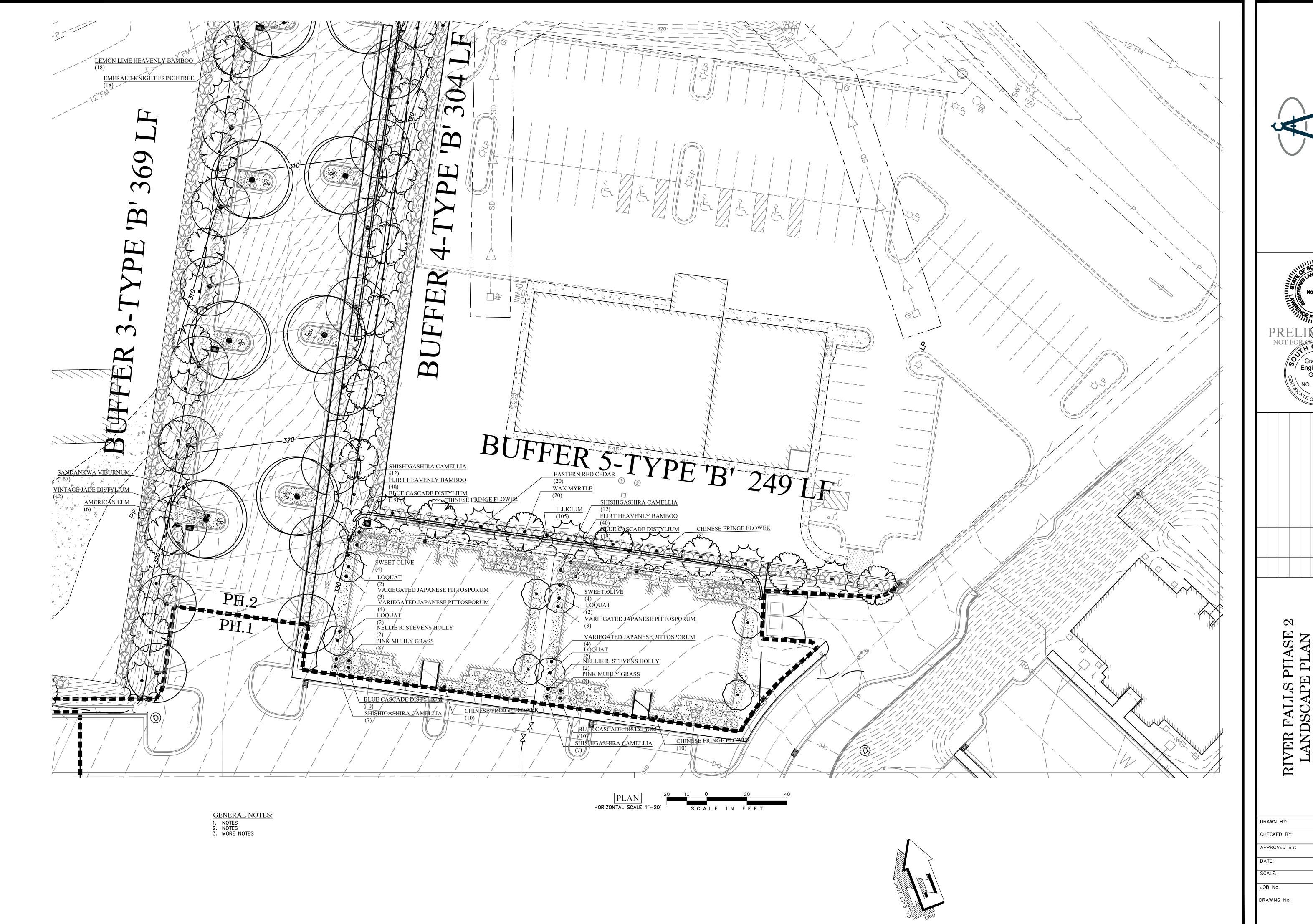




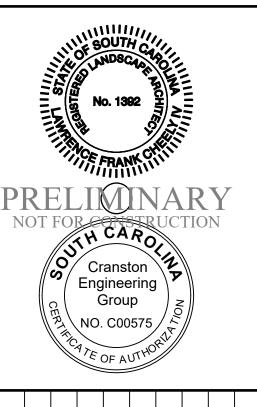
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LANDSCAPE PLAN 5
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BY:	DY
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	01-18-2022
	1" = 20'
	2022-0001
No.	

L105

THE PARKER AUGUSTA

TRAFFIC IMPACT STUDY FRONTAGE ROAD @ W. MARTINTOWN ROAD (SC-230)

Prepared for:

JH Cleveland 618 Ponder Place Dr Evans, GA 30809

Prepared by:



100 GRACE HOOPER LN, SUITE 3751 AUGUSTA, GA 30901

SUBMITTED: MAY 2022



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EXECUTIVE SUMMARY

Introduction

The proposed development for The Parker Augusta (formerly River Falls Apartments) is located near the intersection of W. Martintown Road (SC-230) and Frontage Road in North Augusta, South Carolina. The Parker Augusta project is situated on the 16-acre tract located on Frontage Road behind Wacky Waynes Fireworks. The River Falls Apartment Traffic Impact Study for Phase 1 was submitted to the SCDOT District 7 and approved in 2021. The property has since been transferred to new ownership and the revised development plan anticipates building the entire site at once. The project proposes a single construction phase to include 18 buildings comprised of 1, 2, and 3-bedroom units totaling 264 dwelling units. Since the previous Study was already approved, we have built off that approved Phase 1 of construction and projected full occupancy by 2025. The purpose of this study is to analyze the access plan and traffic impacts associated with this full buildout of this proposed development.

Existing Conditions

The Martintown Road corridor is classified as a Tier II roadway by the City of North Augusta (CoNA) Development Plan. Per the North Augusta Development Code, a development is responsible for roadway improvements for any project that creates a Level of Service (LOS) of D or worse. The existing roadways are sufficient with the exception of the I-20 WB off-ramp left turn and the Frontage Road approach to Martintown Road. These both experience LOS F in the AM and PM peak hours and require improvements, regardless of the traffic from proposed site.

Proposed Development

The anticipated traffic generated by The Parker Augusta Apartments is approximately 1,650 trips a day. Due to the high volume of traffic on Martintown Road, left hand turns exiting the development experienced high delay times (LOS F) in both the open year-build and design year analysis scenarios. Due to the close proximity to the existing traffic signal at the eastbound I-20 off-ramp, a traffic signal was deemed to be unfeasible at this location. Therefore, all traffic exiting the development would need to exit southbound on Martintown Road and make a U-turn to get north to the I-20 interchange. Northbound traffic turning left to enter the proposed development still operates at acceptable levels.

Recommendations

ClearCourse recommends that the intersection of Martintown Road at Frontage Road be revised to a right-out only for traffic coming from Frontage Road. Road widening along northbound Martintown Road will be required at the U-turn location to allow for the design vehicle turning movement. It is anticipated that a signal will be needed at the Knobcone Avenue intersection in the near future and therefore the U-turn at this intersection is desirable. Any traffic desiring to travel north exiting the site will be required to exit south on Martintown Road and make a U-turn at the Knobcone Avenue intersections.



INTRODUCTION

This report analyzes the existing and projected traffic volumes associated with the revised layout for The Parker Augusta (formerly River Falls Apartments) development at the intersection of W. Martintown Road (SC-230) and Frontage Road in North Augusta, South Carolina. The Parker Augusta project contains a single construction phase situated on a 16-acre tract located on Frontage Road behind Wacky Waynes Fireworks. The development will be 18 buildings comprised of 1, 2, and 3-bedroom units.

LOCATION

The site is located in the western corner of Aiken County, within the North Augusta city limits. It falls within the City's Traffic Impact Tier 2 and is just south of I-20 Exit 1. See Figure 1 for the Vicinity Map and Figure 2 for the Project Site Map. This report is submitted to the South Carolina Department of Transportation (SCDOT) and North Augusta Engineering & Planning and Development Departments for review on behalf of the developer, JH Cleveland.

Existing traffic conditions were analyzed for the intersection to determine the need for potential improvements to accommodate the future traffic volumes and allow efficient ingress and egress to the site. Capacity issues are not anticipated on Frontage Road due to minimal traffic that currently utilizes Frontage Road. Therefore, the focus of this study will be on the capacity and delay associated with the additional traffic entering and exiting onto W. Martintown Rd (SC-230) during the peak hours and passing through the two I-20 Exit 1 interchange intersections. The methodology to assess operations and the study findings are summarized in the sections that follow.



Figure 1: Vicinity Map



CAPACITY ANALYSIS METHODOLOGY

The methodology used for evaluating intersection traffic operations is based on criteria set forth in the Transportation Research Board's <u>Highway Capacity Manual</u>, 6th Edition (HCM). The capacity of an intersection is described in terms of Level of Service (LOS), which ranges from A to F and corresponds to average control delay per vehicle.

In general, the LOS may be defined as a measure of operating conditions within a traffic stream and the perception of the conditions by the general motoring public. The six levels of service are briefly described, as follows:

- LOS A Little or no traffic delays;
- LOS B Minimal to short traffic delays;
- LOS C Average traffic delays;
- LOS D Relatively long traffic delays;
- LOS E Intersections are at or near the maximum capacity and traffic experiences long delays; and
- LOS F Intersections are operating above their maximum capacity and traffic delays are long and unstable.

For signalized intersections, one overall intersection LOS is reported. At unsignalized intersections, the LOS for each controlled approach or movement (side-streets and main-street left-turns) is reported. Table 1 presents LOS criteria for signalized and unsignalized intersections.

Table 1 Level of Service Criteria						
	Average Control	Delay (sec / veh)				
LOS	Signalized Intersections	Unsignalized Intersections				
А	≤ 10	≤10				
В	> 10 and ≤20	> 10 and ≤ 15				
С	> 20 and ≤35	> 15 and ≤ 25				
D	> 35 and ≤55	> 25 and ≤ 35				
Е	> 55 and ≤80	> 35 and ≤ 50				
F	> 80	> 50				

A volume-to-capacity ratio (v/c) is also computed for each lane group and at signalized intersections an overall v/c ratio is reported. The capacity of the intersection is calculated based on the geometry and traffic control. Intersection capacity is then compared to the volumes entering the intersection. A v/c ratio of less than 1.0 indicates that there is sufficient capacity for the traffic demand. A v/c ratio of more than 1.0 generally indicates the need for intersection improvements.



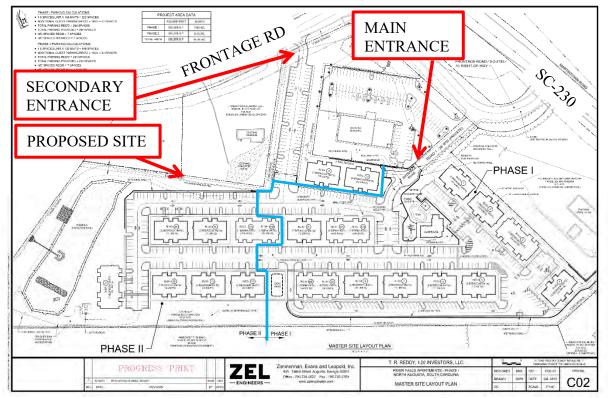


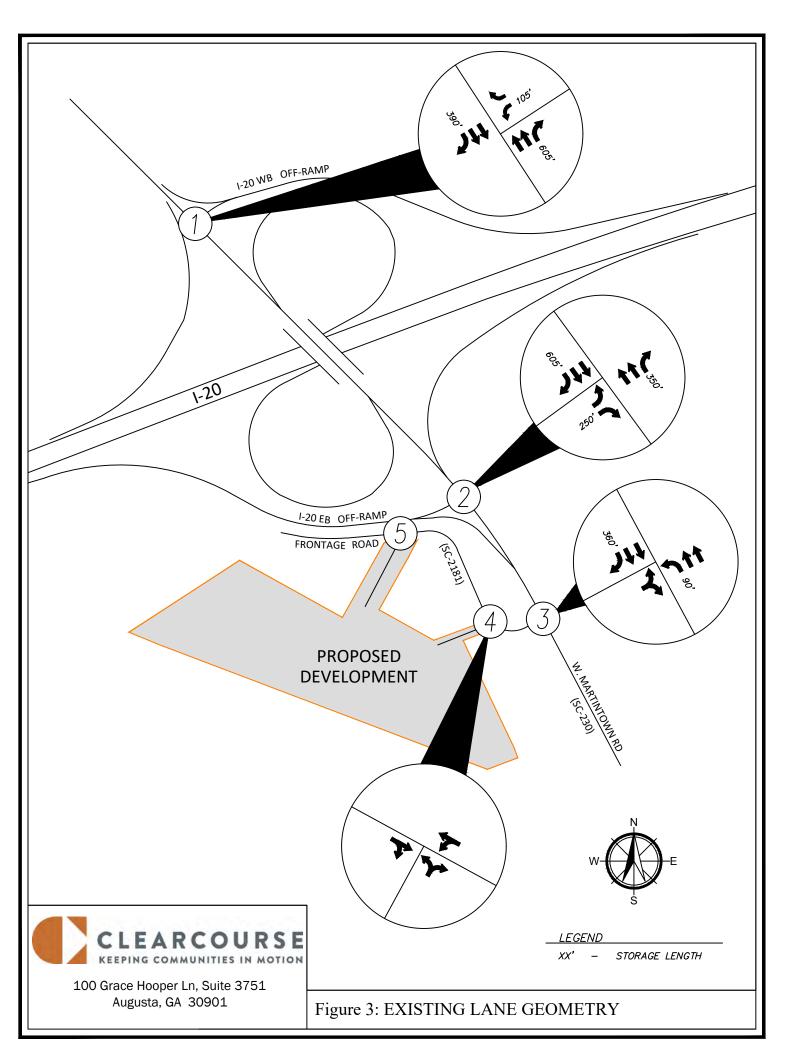
Figure 2: Project Site Map

EXISTING CONDITIONS SURVEY

An evaluation of existing conditions was performed to document existing operations and provide a basis for relative comparison of future conditions. The following paragraphs describe the existing roadway facilities, traffic volumes, and intersection operations.

The study area for this project includes Frontage Road, W. Martintown Road, and the EB and WB I-20 Exit 1 off-ramps. W. Martintown Road is a state route (SC-230) that connects Edgefield County to North Augusta's Central Business District. Frontage Road intersects W. Martintown Road just south of the I-20 interchange (Exit 1). W. Martintown Road carries the majority of traffic volume while Frontage Road is the minor side road. W. Martintown Road is a 5-lane section that includes a center two-way left turn lane. The Frontage Road approach to the intersection is a single lane with a shared left turn and right turn lane with a stop condition. A newly installed traffic signal is located at the intersection of W. Martintown Road and the eastbound I-20 off-ramp. For the purposes of this study, Frontage Road is the east/west movement and W. Martintown Road is north/south. Figure 3 shows the existing lane geometry for the intersections in the study area.





Existing Conditions

This development is proposed near the I-20 Exit 1 interchange that intersects Martintown Road in North Augusta, South Carolina. The Martintown Rd corridor is largely underdeveloped at the interchange. It was observed that the existing roadways adequately maintain the existing traffic volume with several intersections experiencing a long delay for the minor approaches during the peak hours. However, there are several projects ongoing in the surrounding areas and are summarized in the West Martintown Road Corridor Study, adopted by the City of North Augusta in April 2021.

EXISTING TRAFFIC VOLUMES

Turning movement counts were performed for the 2-hour peak times on March 22, 2022 from 7:00 am to 9:00 am and from 4:00 pm to 6:00 pm. The four consecutive 15-minute interval volumes that summed to the highest volume during the morning and evening peak periods were determined at each intersection. Tube counts were also conducted to establish the average daily traffic (ADT) volume, as shown in Table 2.

	Table : Traffic in the S	_	l		
Route	Location	2022 ADT	Average Annual Growth	2025 ADT (100% Capacity)	2030 ADT (Design Year)
W. Martintown Road	North of Frontage Road	23,730	2.00%	25,182	27,803
Frontage Road	Between CSRA Pain Management driveway and W. Martintown Road	313	2.00%	332	367

Historical traffic data from SCDOT line counts show a 2.0% growth rate in the study area. The traffic study done for the I-20 project showed growth rates from 1.2% - 1.83% at the interchange. The historical line count data was used for this report as it was the more conservative estimate. The growth rate was applied to the existing volumes over three and eight years to give the 2025 (base year) and 2030 (design year) traffic volume projections.

Existing intersection operations were analyzed to establish current traffic conditions and identify areas of existing deficiencies that should be addressed. The opening year existing peak hour counts and current intersection geometries were used in the analysis. The results are summarized in Table 3 and the estimated opening year, No-Build volumes are illustrated in Figure 4.



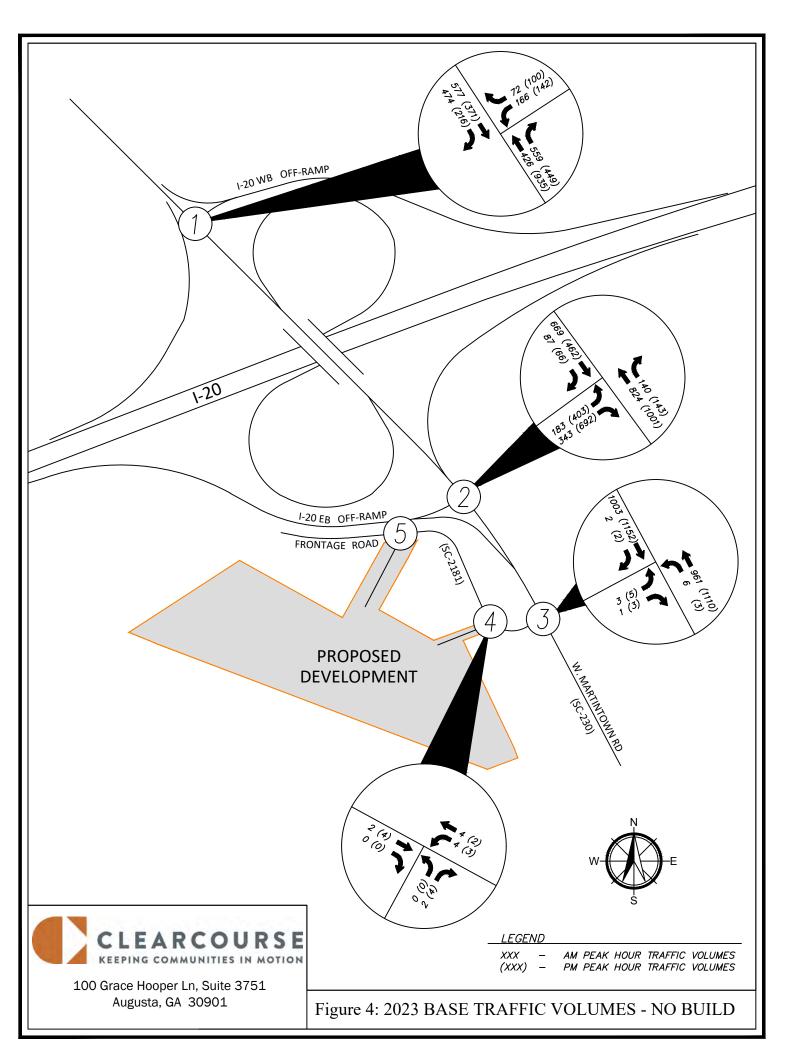


	Table 3			_		
Existing Intersection	on Operat	ions – Bas	e Year (20	23)		
	A.	M. Peak H	lour	P.1	Л. Peak H	our
Intersection	Delay (sec)	LOS	v/c	Delay (sec)	LOS	v/c
W. Martintown Road @ I-20 WB Off-ramp						
westbound left-turn	58.4	F	0.82	194.7	F	1.18
westbound right-turn	10.5	В	0.12	14.0	В	0.22
W. Martintown Road @ I-20 EB Off-ramp*	np*					
Eastbound approach	10.8	В	0.40	12.1	В	0.57
W. Martintown Road @ Frontage Road						
northbound left-turn	10.9	В	0.01	11.2	В	0.01
eastbound approach	66.6	F	0.22	63.5	F	0.18
Site Driveway #1 @ Frontage Road						
- westbound left-turn	7.2	Α	0.00	7.2	Α	0.00
- northbound approach	8.3	Α	0.00	8.3	А	0.00

^{*} Denotes a signalized intersection

The westbound off-ramp experiences failing delays (LOS F) in the AM and PM peak hours for the left-turn movement. The Frontage Road approach at W. Martintown Road also operates at LOS F during the morning and evening peak hours. The northbound left-turn operates at LOS B in the AM and PM peak hours. The proposed site entrance projects to operate at LOS A for AM and PM peak hours. All approaches are below capacity for the total traffic volume carried and do not warrant additional capacity, except for the westbound off-ramp, which has a capacity over 1.0 in the PM peak hour.

Under the opening year No Build traffic conditions, the existing roadway geometry and traffic control in the study area is failing to serve existing demand with a surplus of capacity. Mitigation measures have been identified in the West Martintown Road Corridor Study for these intersections. However, there is currently no plan or ongoing design for these improvements.

Proposed Build Traffic Conditions

The proposed apartment development will access Frontage Road and move through the Martintown Road intersection. The apartment complex is proposed to have a single phase with 264 total apartments constructed by 2024. The traffic analysis is broken into the open year scenario (50% occupancy by 2023); the 100% occupancy scenario (by 2025); and the design year scenario (2030). A design period of 5 years is used to evaluate the short-term growth of the study area. The existing traffic volumes were given a 2.0% growth rate projection for the proposed traffic analysis. Trip generations were calculated for the apartments using the number of units based on the use of the proposed building. Proposed traffic volumes used in this analysis are made up of the projected 2023, 2025 and 2030 traffic volumes plus the addition of projected site-generated traffic. Projections for trip generation and traffic assignment are detailed in the following sections.



Trip Generation

Traffic that will be generated by the apartment development is projected based on trip generation characteristics for similar land uses nationwide. The trip generation rates used in this study were taken from the 10th edition of the Institute of Transportation Engineers' (ITE) <u>Trip Generation Manual</u> report. Trip generations were based on *ITE Land Use 220 – Multifamily Housing (Low Rise)*. Due to the nature of this site, pass-by reductions were deemed not applicable.

Gross trip generations for the proposed development are presented in Table 4.

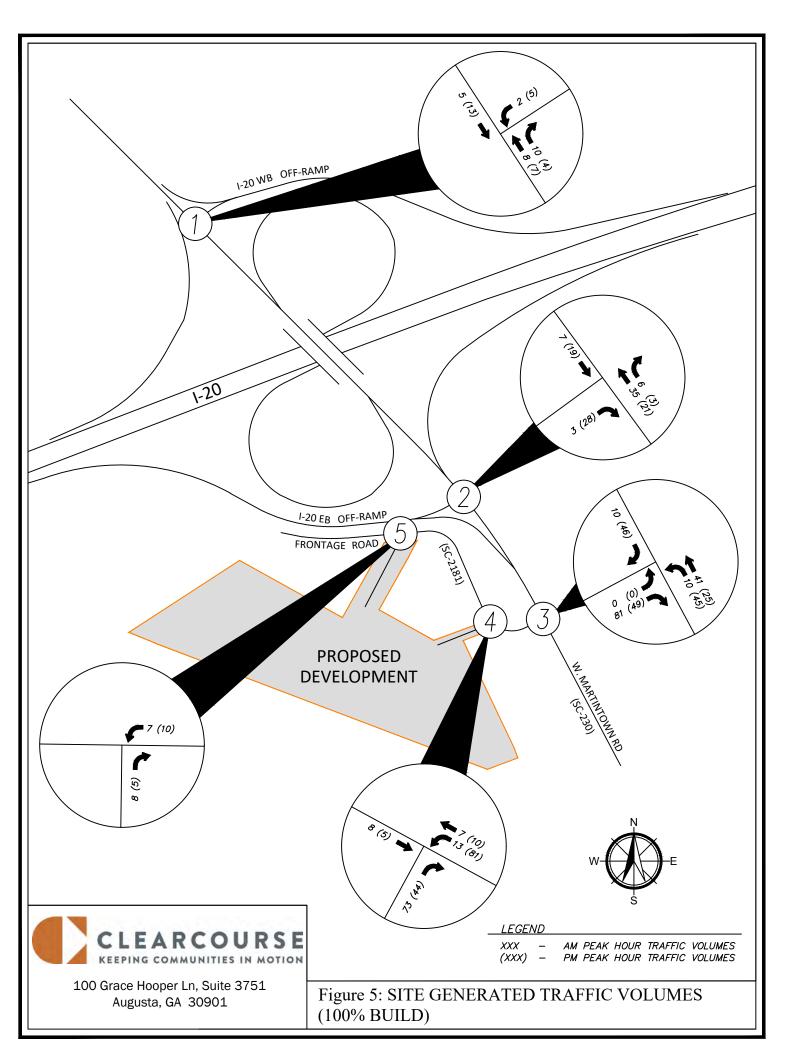
	Table 4 Trip Generation								
	A.M.	. Peak H	our	P.M	. Peak H	our	Avera	ge Daily	Trips
Land Use	Enter	Exit	Total	Enter	Exit	Total	Enter	Exit	Total
220 – Multifamily Housing – 2023 50% Occupied (132 Units)	11	43	54	46	25	71	416	417	833
220 – Multifamily Housing – 2025 100% Occupied (264 Units)	20	81	101	91	49	140	833	833	1666
Pass-by Reductions	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
New Driveway Volumes (100% Occupied)	20	81	101	91	49	140	833	833	1666

Traffic Assignment and Trip Distribution

The arriving/departing percentages for Trip Assignment were determined by the proposed building uses based on the historical data of the building uses, per the Trip Generation Manual. Traffic Distribution describes the direction drivers will be coming from/going to when they turn into and depart from the site. The breakdown of the assigned trips generated by the site is shown in Table 5. The trip distribution volumes of the arrivals and departures for this site onto Martintown Road is presented in Figure 5. Both the arriving and departing trip percentages were calculated based on the existing turning movements due at each interchange intersection and on Frontage Road. The resulting traffic that will be generated by these calculations was added to the study area based on these distributions.

Table 5 Trip Generation Percentages							
D. W. alley	A.M. Peak Hour P.M. Peak Hour						
Building Use	Arrivals	Departures	Arrivals	Departures			
220 – Multifamily Housing (Low-Rise)	20%	80%	65%	35%			





Site Access

The site will have two driveways connected to Frontage Road. Due to the layout of the parking lot, it is assumed most traffic will flow through the main entrance on the east side of the site. The other entrance will connect to Frontage Road on the north side of the site. This second driveway has been included in the analysis of Frontage Road for this report. The existing roadway geometry will be used in the initial analysis of the intersection to determine if auxiliary storage lengths are adequate and if further improvements are needed for acceptable traffic operations.

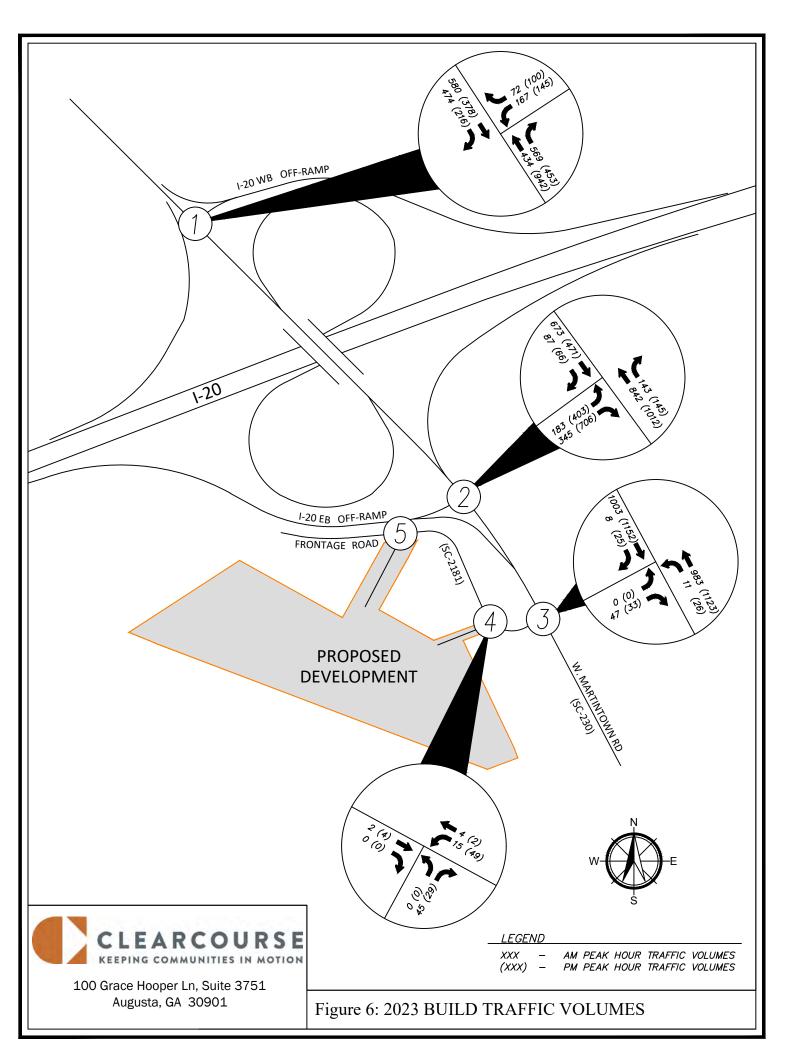
Proposed Intersection Operations

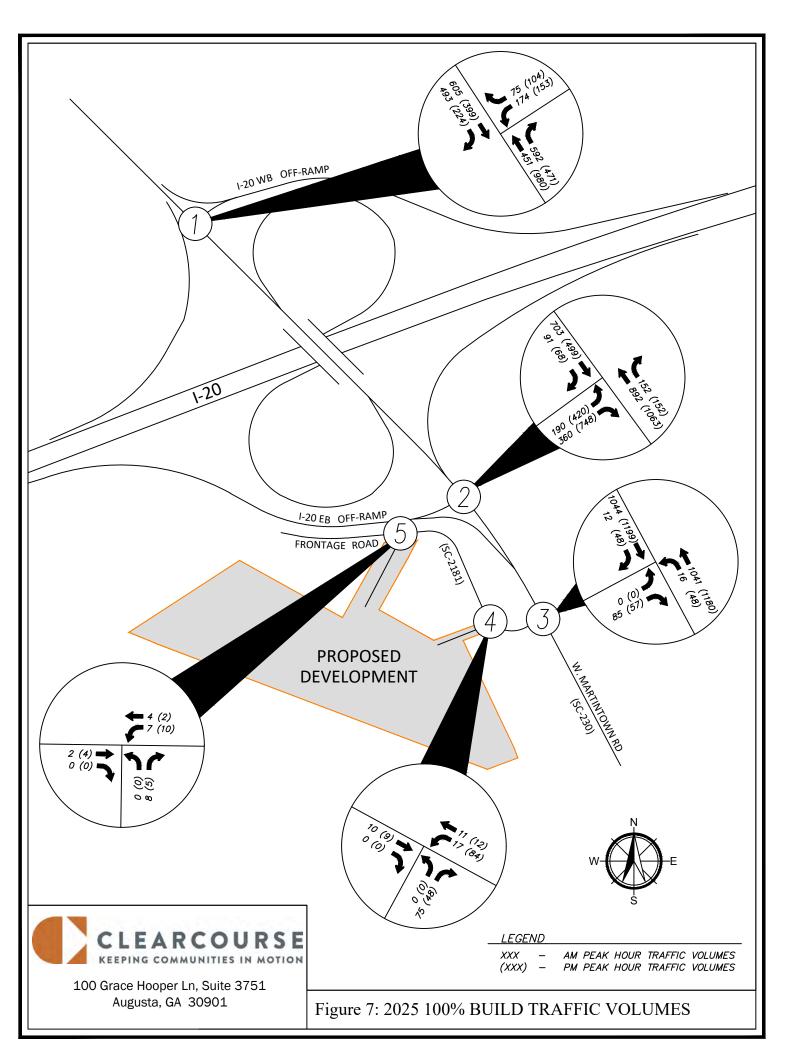
Using the proposed traffic volumes (shown in Figures 6, 7 and 8) a capacity analysis was performed for the peak hours at the study area intersection. Results of the analysis for the 100% occupied-year and a 5-year design scenarios are presented below in Table 6.

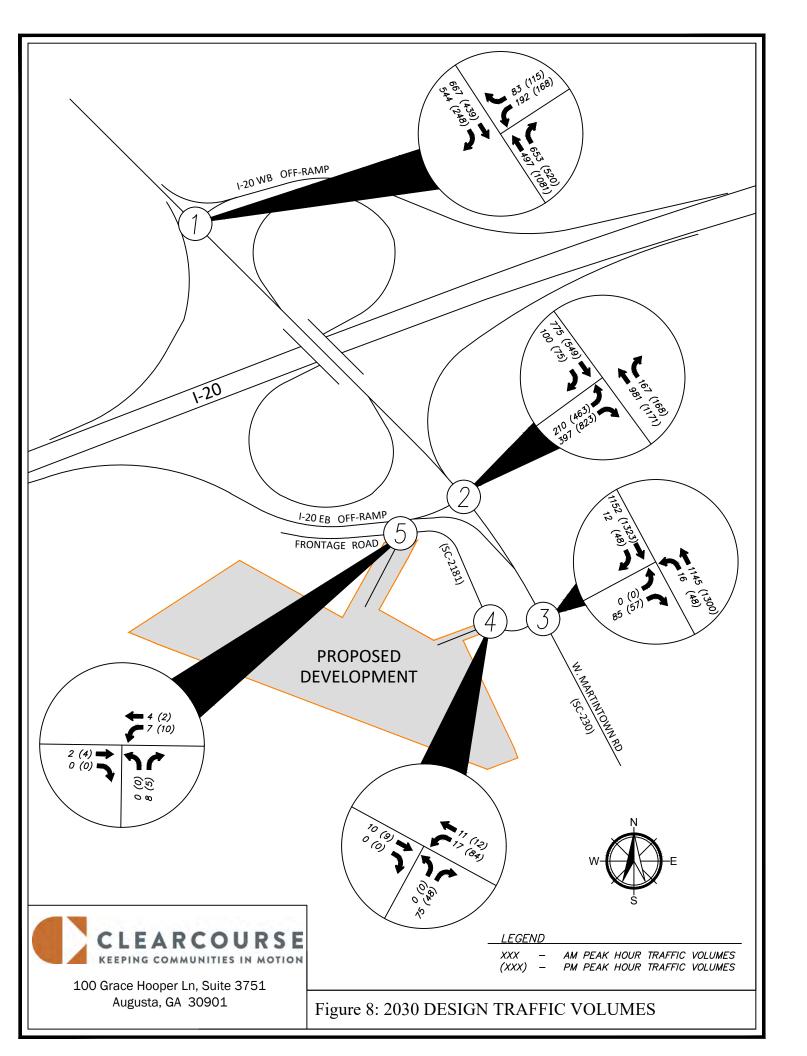
The northbound left-turn movement from Martintown Road provides adequate capacity for all design periods analyzed and the delay is no worse than the LOS B. The storage length of the existing left-turn lane was observed to be approximately 100 feet long with a 50-foot taper length. This was adequate based on the maximum queue length remaining under 50 feet. The minor approach to the intersection experiences significant delay due to the increased exiting left-turn volumes. With the initial construction phase already approved and underway, it is recommended that Frontage Road be improved to a right out only. Making this improvement changes the approach from LOS F in both the AM and PM Build scenario to a LOS E in the AM peak and LOS C in the PM peak during the Design year scenario. The summary of each movement is provided below in Table 6.

Intersectio	Table 6 on Operations Summa	arv				
inci sectio	<u> </u>	л. у И. Peak Н	Hour	P.M. Peak Hour		
Intersection	Delay (sec)	LOS	v/c	Delay (sec)	LOS	v/c
2025 Build						
W. Martintown Road @ I-20 WB Off-ramp						
- westbound left-turn	62.4	F	0.84	210.7	F	1.22
- westbound right-turn	10.5	В	0.13	14.0	В	0.23
W. Martintown Road @ I-20 EB Off-ramp*	5.4	Α		8.0	А	
- Eastbound approach	11.0	В	0.40	12.2	В	0.57
W. Martintown Road @ Frontage Road						
- northbound left-turn	10.9	В	0.02	11.6	В	0.05
- eastbound approach	819.5	F	2.54	182.7	F	0.88
Site Driveway #1 @ Frontage Road						
- westbound left-turn	8.5	Α	0.04	8.4	Α	0.03
- northbound approach	7.2	Α	0.01	7.3	Α	0.03
Site Driveway #2 @ Frontage Road						
- westbound left-turn	0.0	Α	0.00	0.0	Α	0.00
- northbound approach	0.0	Α	0.00	0.0	Α	0.00
2030 Build w/ Improvments						
W. Martintown Road @ I-20 WB Off-ramp						
- westbound left-turn	163.1	F	1.18	164.2	F	1.1
- westbound right-turn	11	В	0.15	13.7	В	0.22
W. Martintown Road @ I-20 EB Off-ramp*	6.0	Α		7.8	Α	
- Eastbound approach	12.1	В	0.45	11.9	В	0.56
W. Martintown Road @ Frontage Road						
- northbound left-turn	12.0	В	0.04	12.6	В	0.13
- eastbound approach (Right Only)	41.7	E	0.81	15.8	C	0.23
Site Driveway #1 @ Frontage Road						
- westbound left-turn	8.6	Α	0.08	8.5	Α	0.05
- northbound approach	7.3	Α	0.01	7.4	Α	0.06
Site Driveway #2 @ Frontage Road						
- westbound left-turn	7.2	Α	0.01	7.2	Α	0.01
- northbound approach	8.4	Α	0.01	8.4	Α	0.01









STUDY FINDINGS

Existing Conditions

The following points summarize analysis of the existing conditions within the study area:

- Existing operations along W. Martintown Road (SC-230) at Frontage Road are mostly within acceptable ranges of delay. However, the Frontage Road approach already experiences a long delay (LOS F) due to the high traffic volumes on Martintown Road.
- The westbound I-20 off-ramp left turn movement experiences LOS F in both the AM and PM peak hours and is over capacity in the PM peak hour.
- Improvements were identified to mitigate the current and projected traffic volumes in the West Martintown Road Corridor Study, adopted by the City of North Augusta in April 2021. There are no currently no projects programed for these improvements.

Proposed Development

The anticipated traffic impacts of The Parker Augusta Apartments are summarized below:

- The proposed Open Year (50% occupancy) for the apartment complex off Frontage Road is projected to introduce 833 new trips to W. Martintown Road on a daily basis. Approximately 54 of these new trips will occur during the morning peak hour and 71 new trips will occur during the evening peak hour.
- The proposed Open Year (100% occupancy) for the apartment complex off Frontage Road is projected to introduce 1,650 new trips to W. Martintown Road on a daily basis. Approximately 101 of these new trips will occur during the morning peak hour and 140 new trips will occur during the evening peak hour.
- Trip distribution was based on travel patterns associated with the existing traffic volumes on Martintown Road. This data indicates that there is a 53/47 split of traffic arriving from/departing to the north/south direction in both the morning and in the afternoon.
- There are two access drives from the site to Frontage Road and both will funnel the proposed traffic through the analyzed intersection at W. Martintown Road. The existing lane geometry at the proposed driveway is sufficient for the anticipated volumes generated by the apartment complex.
- The delay for traffic exiting the site at the Frontage Road intersection is failing due to the high volume of cross traffic on W. Martintown Road not allowing for gaps. A signal warrant was recommended to analyze the intersection with a signal control. However, due to the proximity of the existing signal recently installed as part of the I-20 widening project at the I-20 Exit 1 eastbound exit ramp, a signal was not deemed feasible.

STUDY FINDINGS (CONT.)

Future Traffic Operations

Future build condition analyses were prepared for The Parker Augusta Apartments. Results of these analyses are summarized as follows:

- The un-signalized intersections at Frontage Road and I-20 westbound off-ramp will operate with extended delays on the existing, stop-controlled T-intersection regardless of when the apartment complex opens.
- Requiring traffic on Frontage Road to make a right turn only onto Martintown Road will reduce the delay to allowable levels. Construction of a concrete median will help guide traffic to exit safely. Widening to allow for the U-turn movement at Knobcone Avenue intersection will be necessary to allow for the U-turns leaving the proposed site.
- Left turns onto Frontage from Martintown Road operate at acceptable levels and can remain. If a raised median is installed in the future, it is recommended that this left turn be maintained.

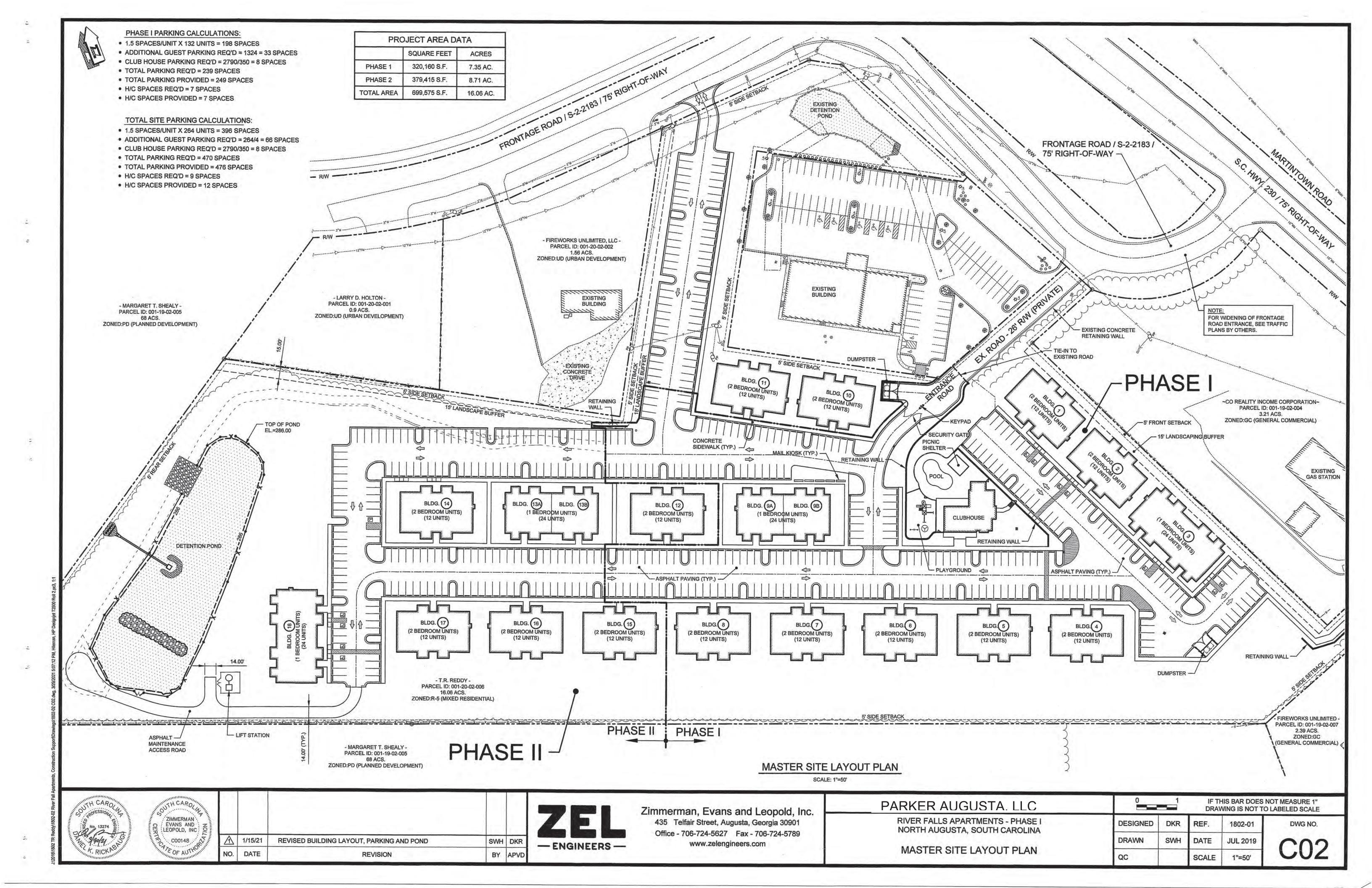


APPENDICES



APPENDIX A PROPOSED SITE LAYOUT PLAN





APPENDIX B TRAFFIC VOLUME WORKSHEETS



Vehicle Trip Ends vs: Occupied Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

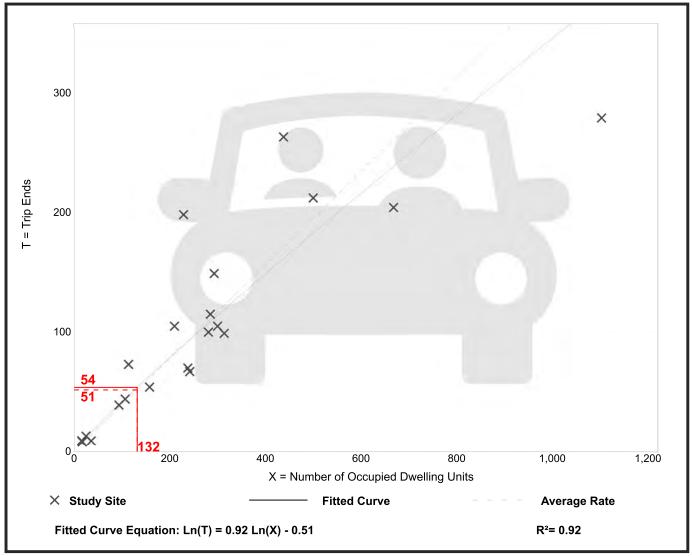
Setting/Location: General Urban/Suburban

Number of Studies: 21 Avg. Num. of Occupied Dwelling Units: 270

Directional Distribution: 20% entering, 80% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate	Range of Rates	Standard Deviation			
0.39	0.25 - 0.86	0.15			



Vehicle Trip Ends vs: Occupied Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

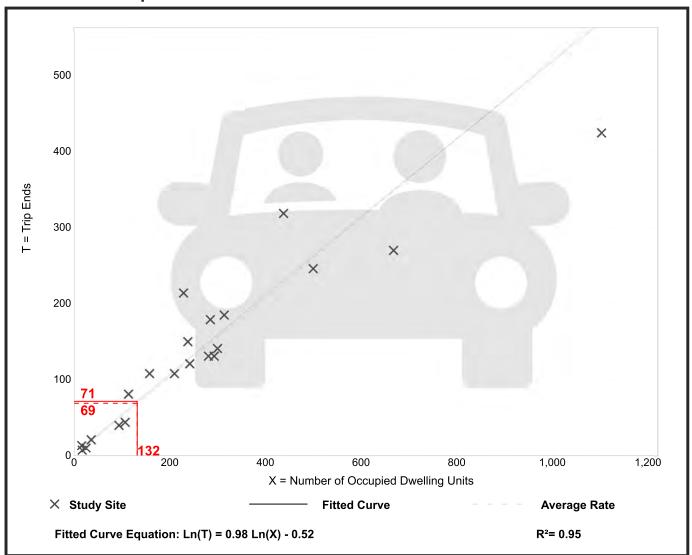
Setting/Location: General Urban/Suburban

Number of Studies: 21 Avg. Num. of Occupied Dwelling Units: 270

Directional Distribution: 65% entering, 35% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.52	0.38 - 0.93	0.14



Vehicle Trip Ends vs: Occupied Dwelling Units

On a: Weekday

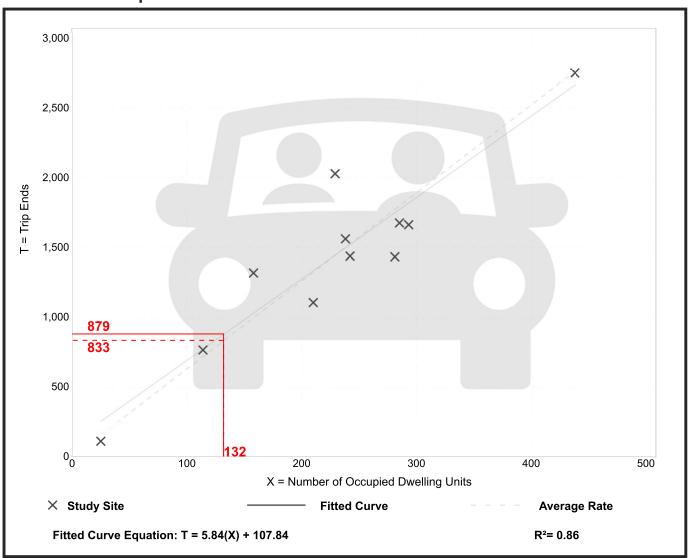
Setting/Location: General Urban/Suburban

Number of Studies: 11 Avg. Num. of Occupied Dwelling Units: 228

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
6.31	4.36 - 8.86	1.17



Vehicle Trip Ends vs: Occupied Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

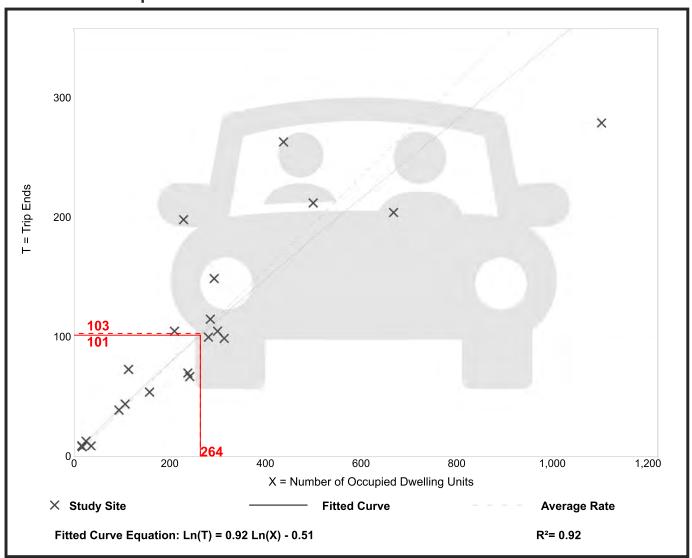
Number of Studies: 21

Avg. Num. of Occupied Dwelling Units: 270

Directional Distribution: 20% entering, 80% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate	Range of Rates	Standard Deviation				
0.39	0.25 - 0.86	0.15				



Vehicle Trip Ends vs: **Occupied Dwelling Units**

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

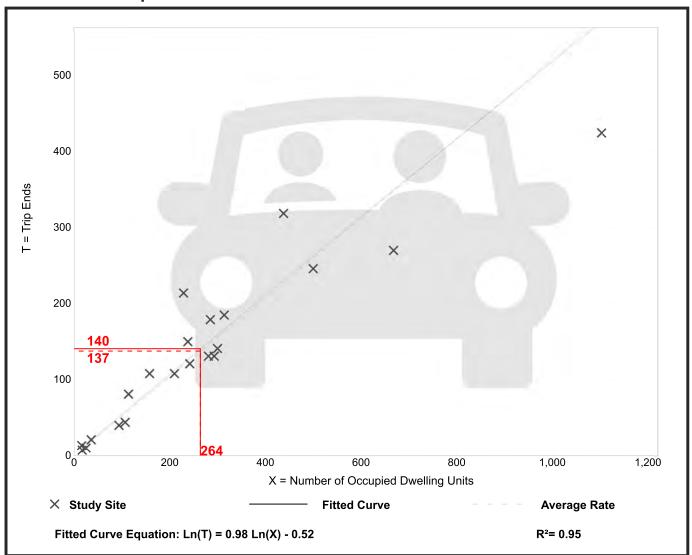
Setting/Location: General Urban/Suburban

Number of Studies: 21 Avg. Num. of Occupied Dwelling Units: 270

Directional Distribution: 65% entering, 35% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate		Range of Rates	Standard Deviation			
	0.52	0.38 - 0.93	0.14			



Vehicle Trip Ends vs: Occupied Dwelling Units

On a: Weekday

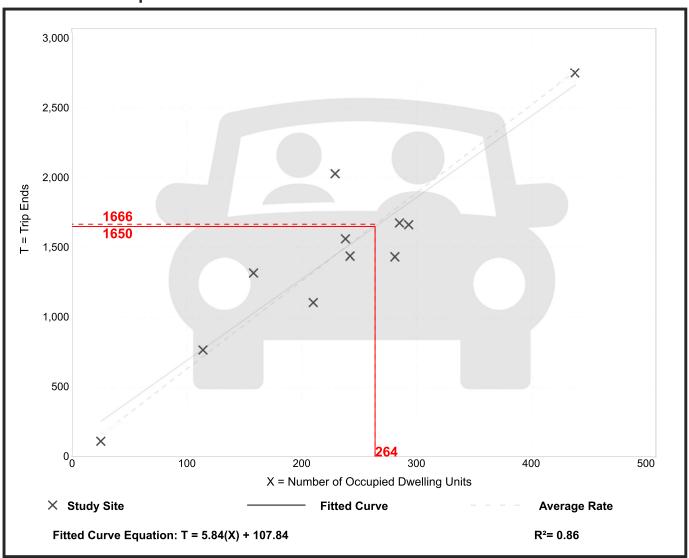
Setting/Location: General Urban/Suburban

Number of Studies: 11 Avg. Num. of Occupied Dwelling Units: 228

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Occupied Dwelling Unit

Average Rate	Range of Rates	Standard Deviation				
6.31	4.36 - 8.86	1.17				



APPENDIX C EXISTING TRAFFIC OPERATIONS



Intersection												
Int Delay, s/veh	8.3											
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4₽	7		414	7		4			र्स	7
Traffic Vol, veh/h	0	565	464	0	417	548	0	0	0	162	0	70
Future Vol, veh/h	0	565	464	0	417	548	0	0	0	162	0	70
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0
Veh in Median Storage	-, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	88	88	92	87	87	92	92	92	76	76	76
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	642	527	0	479	630	0	0	0	213	0	92
Major/Minor N	Major1		ľ	Major2		N	/linor1		ľ	Minor2		
Conflicting Flow All	479	0	-	642	0	0	882	1121	321	800	1121	240
Stage 1	-	-	-	-	-	-	642	642	-	479	479	-
Stage 2	-	-	-	-	-	-	240	479	-	321	642	-
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32
Pot Cap-1 Maneuver	1080	-	0	939	-	0	241	205	675	276	205	761
Stage 1	-	-	0	-	-	0	429	467	-	537	553	-
Stage 2	-	-	0	-	-	0	742	553	-	665	467	-
Platoon blocked, %		-			-							
Mov Cap-1 Maneuver	1080	-	-	939	-	-	212	205	675	276	205	761
Mov Cap-2 Maneuver	-	-	-	-	-	-	212	205	-	276	205	-
Stage 1	-	-	-	-	-	-	429	467	-	537	553	-
Stage 2	-	-	-	-	-	-	652	553	-	665	467	-
, and the second second												
Approach	SE			NW			NE			SW		
HCM Control Delay, s	0			0			0			39		
HCM LOS				- 0			A			E		
TOW LOO							,,					
Minor Lanc/Major Muse	+ ^	JEL n1	NIMA	NIMT	CEL	CETC	\// n10	٠١٨/١ م				
Minor Lane/Major Mvm	it P	NELn1	NWL	NWT	SEL		WLn1S					
Capacity (veh/h)		-	939	-	1080	-	276	761				
HCM Carried Pales (a)		-	-	-	-		0.772					
HCM Control Delay (s)		0	0	-	0	-	51.4	10.4				
HCM Lane LOS		Α	A	-	A	-	F	В				
HCM 95th %tile Q(veh)		-	0	-	0	-	5.8	0.4				

	>	→	74	•	←	*_	\	×	4	*	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	7	↑	77	ሻሻ	₽		7	ተ ኈ		ሻ	^	
Traffic Volume (veh/h)	179	1	336	0	0	0	0	655	0	0	944	0
Future Volume (veh/h)	179	1	336	0	0	0	0	655	0	0	944	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	229	1	0	0	0	0	0	712	0	0	1137	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	584	328		544	328	0	272	1722	0	272	2474	0
Arrive On Green	0.18	0.18	0.00	0.00	0.00	0.00	0.00	0.48	0.00	0.00	0.48	0.00
Sat Flow, veh/h	1781	1870	2790	2748	1870	0	495	3647	0	738	5274	0
Grp Volume(v), veh/h	229	1	0	0	0	0	0	712	0	0	1137	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1374	1870	0	495	1777	0	738	1702	0
Q Serve(g_s), s	3.2	0.0	0.0	0.0	0.0	0.0	0.0	3.4	0.0	0.0	3.9	0.0
Cycle Q Clear(g_c), s	3.2	0.0	0.0	0.0	0.0	0.0	0.0	3.4	0.0	0.0	3.9	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	584	328		544	328	0	272	1722	0	272	2474	0
V/C Ratio(X)	0.39	0.00		0.00	0.00	0.00	0.00	0.41	0.00	0.00	0.46	0.00
Avail Cap(c_a), veh/h	1484	1273		1932	1273	0	463	3090	0	556	4440	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	10.3	9.0	0.0	0.0	0.0	0.0	0.0	4.4	0.0	0.0	4.5	0.0
Incr Delay (d2), s/veh	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.1	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.0
Unsig. Movement Delay, s/veh												3.5
LnGrp Delay(d),s/veh	10.8	9.0	0.0	0.0	0.0	0.0	0.0	4.6	0.0	0.0	4.7	0.0
LnGrp LOS	В	A	0.0	A	A	A	A	A	A	A	A	A
Approach Vol, veh/h		230	А	, , , , , , , , , , , , , , , , , , ,	0			712			1137	
Approach Delay, s/veh		10.7	7.		0.0			4.6			4.7	
Approach LOS		В			0.0			Α.			Α.	
Approach E03											A	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		17.3		9.1		17.3		9.1				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		5.9		5.2		5.4		0.0				
Green Ext Time (p_c), s		6.9		0.5		4.2		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			5.3									
HCM 6th LOS			Α									
Notes												

Unsignalized Delay for [EBR] is excluded from calculations of the approach delay and intersection delay.

Intersection												
Int Delay, s/veh	0.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7	1	ΦÞ		ሻ	^	7
Traffic Vol, veh/h	2	0	0	0	0	0	5	942	0	0	983	1
Future Vol, veh/h	2	0	0	0	0	0	5	942	0	0	983	1
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	25	25	25	92	92	92	85	85	85	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	8	0	0	0	0	0	6	1108	0	0	1092	1
Major/Minor N	Minor2		ľ	Minor1		N	/lajor1		N	/lajor2		
Conflicting Flow All	1658	2212	546	-	-	554	1093	0	0	1108	0	0
Stage 1	1092	1092	-	-	-	-	-	-	-	-	-	-
Stage 2	566	1120	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94		-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	64	43	482	0	0	476	634	-	-	626	-	-
Stage 1	229	289	-	0	0	-	-	-	-	-	-	-
Stage 2	476	280	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	64	43	482	-	-	476	634	-	-	626	-	-
Mov Cap-2 Maneuver	64	43	-	-	-	-	-	-	-	-	-	-
Stage 1	227	289	-	-	-	-	-	-	-	-	-	-
Stage 2	471	277	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	69.1			0			0.1			0		
HCM LOS	F			A								
Minor Lane/Major Mvm	t	NBL	NBT	NBR E	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		634	-	-		-	626	-	-			
HCM Lane V/C Ratio		0.009	-	-	0.125	-	-	-	-			
HCM Control Delay (s)		10.7	-	-		0	0	-	-			
HCM Lane LOS		В	-	-	F	A	A	-	-			
HCM 95th %tile Q(veh)		0	-	-	0.4	-	0	-	-			

Intersection													
Int Delay, s/veh	17												
		CET	CED	NI\A/I	NIMIT	MMD	NIEI	NET	NED	CIVII	CMT	CIMD	
Movement	SEL	SET	SER 7	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
Lane Configurations	0	₹ †		Λ	€ ↑	140	٥	- ♣	٥	120	4	98	
Fraffic Vol, veh/h uture Vol, veh/h	0	363 363	211 211	0	916 916	440 440	0	0	0	139 139	0	98 98	
Conflicting Peds, #/hr	0	303	0	0	910	440	0	0	0	139	0	98	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Free	-	-	Free	- -	310p -	None	Jiop -	Jiop -	Yield	
Storage Length	_	_	480	_	_	900	_	_	- INOTIC	_	_	0	
/eh in Median Storage		0	-	_	0	-	_	0	_	_	0	-	
Grade, %	-	0	_	_	0	_	_	0	_	_	0	-	
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
/lvmt Flow	0	403	234	0	974	468	0	0	0	162	0	114	
Major/Minor	Major1		N	Major2		ı	/linor1		N	Minor2			
Conflicting Flow All	974	0	ľ	403	0	0	890	1377	202	1176	1377	487	
Stage 1	9/4	-	-	403	-	-	403	403	202	974	974	407	
Stage 2	_		_	_	_	_	487	974	-	202	403	_	
Critical Hdwy	4.14	_	-	4.14	-	_	7.54	6.54	6.94	7.54	6.54	6.94	
Critical Hdwy Stg 1	-	_	_	-	_	_	6.54	5.54	-	6.54	5.54	-	
Critical Hdwy Stg 2	_	_	_	_	_	_	6.54	5.54	_	6.54	5.54	_	
follow-up Hdwy	2.22	_	_	2.22	_	_	3.52	4.02	3.32	3.52	4.02	3.32	
Pot Cap-1 Maneuver	704	-	0	1152	-	0	237	144		~ 147	144	526	
Stage 1	-	-	0	-	-	0	595	598	-	270	328	-	
Stage 2	-	-	0	-	-	0	531	328	-	781	598	-	
Platoon blocked, %		-			-								
Nov Cap-1 Maneuver	704	-	-	1152	-	-	186	144	805	~ 147	144	526	
Nov Cap-2 Maneuver	-	-	-	-	-	-	186	144	-	~ 147	144	-	
Stage 1	-	-	-	-	-	-	595	598	-	270	328	-	
Stage 2	-	-	-	-	-	-	416	328	-	781	598	-	
pproach	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			102			
ICM LOS							Α			F			
/linor Lane/Major Mvm	nt N	VELn1	NWL	NWT	SEL	SETS	WLn1S	SWLn2					
Capacity (veh/h)		_	1152	-	704		147	526					
CM Lane V/C Ratio		-	-	-	-	_		0.217					
ICM Control Delay (s)		0	0	-	0	-	164.2	13.7					
ICM Lane LOS		A	A	-	A	-	F	В					
HCM 95th %tile Q(veh)	-	0	-	0	-	8.8	0.8					
Votes													
: Volume exceeds ca	nacity	¢. Do	lay ove	eeds 3	nne	+: Com	nutation	Not D	ofinad	*. AII	maiory	rolumo i	n platoon
volume exceeds ca	pacity	⊅; D∈	elay exc	eeus 3	005	+. Cuili	pulaliul	ו ואטניטו	enneu	. All	major \	volume I	ii piatuuil

	>	→	-	4	←	*_	\	×	4	1	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	14.54	₽		ሻ	∱ }		ሻ	ተተተ	
Traffic Volume (veh/h)	395	2	678	0	0	0	0	452	0	0	1121	0
Future Volume (veh/h)	395	2	678	0	0	0	0	452	0	0	1121	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	407	2	0	0	0	0	0	491	0	0	1260	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	723	538		422	538	0	211	1594	0	211	2290	0
Arrive On Green	0.29	0.29	0.00	0.00	0.00	0.00	0.00	0.45	0.00	0.00	0.45	0.00
Sat Flow, veh/h	1781	1870	2790	2745	1870	0	440	3647	0	906	5274	0
Grp Volume(v), veh/h	407	2	0	0	0	0	0	491	0	0	1260	0
Grp Sat Flow(s),veh/h/ln	1781	1870	1395	1373	1870	0	440	1777	0	906	1702	0
Q Serve(g_s), s	7.2	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	6.2	0.0
Cycle Q Clear(g_c), s	7.2	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	6.2	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	723	538		422	538	0	211	1594	0	211	2290	0
V/C Ratio(X)	0.56	0.00		0.00	0.00	0.00	0.00	0.31	0.00	0.00	0.55	0.00
Avail Cap(c_a), veh/h	1151	987		1082	987	0	311	2397	0	416	3444	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.2	8.7	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	6.9	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.8	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.0	0.0
Unsig. Movement Delay, s/veh	1											
LnGrp Delay(d),s/veh	11.9	8.7	0.0	0.0	0.0	0.0	0.0	6.1	0.0	0.0	7.1	0.0
LnGrp LOS	В	Α		Α	Α	Α	Α	Α	Α	Α	Α	Α
Approach Vol, veh/h		409	А		0			491			1260	
Approach Delay, s/veh		11.9			0.0			6.1			7.1	
Approach LOS		В						Α			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		19.8		14.3		19.8		14.3				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		8.2		9.2		5.0		0.0				
Green Ext Time (p_c), s		7.1		0.8		2.7		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			7.8									
HCM 6th LOS			Α									
Notes												

Intersection	
Int Delay, s/veh 0.3	
Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SE	T SBR
Lane Configurations 🚓 🏌 🏌 🏌	
Traffic Vol, veh/h 4 0 2 0 0 0 2 1088 0 0 112	
Future Vol, veh/h 4 0 2 0 0 0 2 1088 0 0 112	
Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0	0 0
Sign Control Stop Stop Stop Stop Stop Free Free Free Free Free	e Free
RT Channelized None None -	- None
Storage Length 0 80 200	- 0
Veh in Median Storage, # - 0 0 0	0 -
Grade, % - 0 0 0	0 -
Peak Hour Factor 58 58 58 92 92 92 92 92 97 97	7 97
Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2	2 2
Mvmt Flow 7 0 3 0 0 0 2 1183 0 0 116	4 1
Major/Minor Minor2 Minor1 Major1 Major2	
Conflicting Flow All 1760 2351 582 592 1165 0 0 1183	0 0
Stage 1 1164 1164	
Stage 2 596 1187	
Critical Hdwy 7.54 6.54 6.94 6.94 4.14 4.14	
Critical Hdwy Stg 1 6.54 5.54	
Critical Hdwy Stg 2 6.54 5.54	
Follow-up Hdwy 3.52 4.02 3.32 3.32 2.22 2.22	
Pot Cap-1 Maneuver 54 35 456 0 0 449 595 586	
Stage 1 207 267 - 0 0	
Stage 2 457 260 - 0 0	
Platoon blocked, %	
Mov Cap-1 Maneuver 54 35 456 449 595 586	
Mov Cap-2 Maneuver 54 35	
Stage 1 206 267	
Stage 2 455 259	
Approach EB WB NB SB	
HCM Control Delay, s 59.7 0 0 0	
HCM LOS F A	
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR	
Capacity (veh/h) 595 76 - 586	
HCM Lane V/C Ratio 0.004 0.136	
HCM Control Delay (s) 11.1 59.7 0 0	
HCM Lane LOS B F A A	
HCM 95th %tile Q(veh) 0 0.4 - 0	

APPENDIX D No-Build Traffic Operations



Intersection												
Int Delay, s/veh	9.4											
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		414	7		414	7		4			सी	7
Traffic Vol, veh/h	0	577	474	0	426	559	0	0	0	166	0	72
Future Vol, veh/h	0	577	474	0	426	559	0	0	0	166	0	72
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0
Veh in Median Storage,	, # -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	88	88	88	87	87	87	92	92	92	76	76	76
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	656	539	0	490	643	0	0	0	218	0	95
	/lajor1		N	Major2		N	/linor1		N	Minor2		
Conflicting Flow All	490	0	-	656	0	0	901	1146	328	818	1146	245
Stage 1	-	-	-	-	-	-	656	656	-	490	490	-
Stage 2	-	-	-	-	-	-	245	490	-	328	656	-
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32
Pot Cap-1 Maneuver	1070	-	0	927	-	0	233	198	668	268	198	755
Stage 1	-	-	0	-	-	0	421	460	-	529	547	-
Stage 2	-	-	0	-	-	0	737	547	-	659	460	-
Platoon blocked, %	1070	-		007	-		004	100	//0	0.40	100	755
Mov Cap-1 Maneuver	1070	-	-	927	-	-	204	198	668	268	198	755
Mov Cap-2 Maneuver	-	-	-	-	-	-	204	198	-	268	198	-
Stage 1	-	-	-	-	-	-	421	460	-	529	547	-
Stage 2	-	-	-	-	-	<u>-</u>	645	547	-	659	460	-
Approach	SE			NW			NE			SW		
HCM Control Delay, s	0			0			0			43.9		
HCM LOS							Α			E		
Minor Lane/Major Mvmt	tN	VELn1	NWL	NWT	SEL	SETS	WLn1S	WL _{n2}				
Capacity (veh/h)		-	927		1070	-	268	755				
HCM Lane V/C Ratio		-	-	-	-	-	0.815					
HCM Control Delay (s)		0	0	-	0	-	58.4	10.5				
HCM Lane LOS		Α	Α	-	Α	-	F	В				
HCM 95th %tile Q(veh)		-	0	-	0	-	6.5	0.4				

	>	→	¬₄	•	•	*_	\	\mathbf{x}	4	•	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	1414	1>		ሻ	↑ ↑		ሻ	ተተተ	
Traffic Volume (veh/h)	183	2	343	0	0	0	0	669	0	0	944	0
Future Volume (veh/h)	183	2	343	0	0	0	0	669	0	0	944	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	235	3	0	0	0	0	0	727	0	0	1137	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	591	338		540	338	0	270	1713	0	270	2462	0
Arrive On Green	0.18	0.18	0.00	0.00	0.00	0.00	0.00	0.48	0.00	0.00	0.48	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	495	3647	0	728	5274	0
Grp Volume(v), veh/h	235	3	0	0	0	0	0	727	0	0	1137	0
Grp Sat Flow(s),veh/h/ln	1781	1870	1395	1371	1870	0	495	1777	0	728	1702	0
Q Serve(g_s), s	3.3	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.0	0.0
Cycle Q Clear(g_c), s	3.3	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.0	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	591	338		540	338	0	270	1713	0	270	2462	0
V/C Ratio(X)	0.40	0.01		0.00	0.00	0.00	0.00	0.42	0.00	0.00	0.46	0.00
Avail Cap(c_a), veh/h	1472	1262		1896	1262	0	458	3065	0	547	4403	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	10.3	9.0	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	4.6	0.0
Incr Delay (d2), s/veh	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.1	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
Unsig. Movement Delay, s/veh	1											
LnGrp Delay(d),s/veh	10.8	9.0	0.0	0.0	0.0	0.0	0.0	4.7	0.0	0.0	4.7	0.0
LnGrp LOS	В	Α		А	Α	Α	Α	Α	Α	Α	Α	Α
Approach Vol, veh/h		238	А		0			727			1137	
Approach Delay, s/veh		10.7			0.0			4.7			4.7	
Approach LOS		В						Α			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		17.4		9.3		17.4		9.3				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (q_c+l1), s		6.0		5.3		5.6		0.0				
Green Ext Time (p_c), s		6.9		0.5		4.2		0.0				
Intersection Summary		0.7		0.0		1.2		0.0				
HCM 6th Ctrl Delay			5.4									
HCM 6th LOS			3.4 A									
Notes												

New Name N
Traffic Vol, veh/h
Traffic Vol, veh/h
Traffic Vol, veh/h 3 0 1 0 0 12 6 961 0 1003 2 Future Vol, veh/h 3 0 1 0 0 12 6 961 0 0 1003 2 Conflicting Peds, #/hr 0
Future Vol, veh/h 3 0 1 0 0 12 6 961 0 0 103 2 Conflicting Peds, #/hr 0
Conflicting Peds, #/hr O O O O O O O O O
Sign Control Stop Stop Stop Stop Stop Stop Free None Story Empty - - 0 - - 0 - - 0 - - 0 - - - - - - - - - - - - - - - - - - - <
RT Channelized - None - 0 - 0 - 0 - 0 - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - 1 0 0 1114 1 2 2 2 2 2 2 2 2 2 2 2
Storage Length - - - - 0 80 - 200 - 0 Veh in Median Storage, # - 0 - - 0 90
Weh in Median Storage, # 0
Peak Hour Factor 25 25 25 92 92 92 85 85 85 90 90 90 Heavy Vehicles, % 2
Heavy Vehicles, % 2
Mymt Flow 12 0 4 0 0 13 7 1131 0 0 1114 2 Major/Minor Minor2 Minor1 Major1 Major2 Stage 1 Major2 Stage 1 Major2 Major2 Major2 Major2 Major2 Major2 Major3 Major3 Major3 Major3 Major3 Major4 Major3 Major4 Major3 Major4 Major3 Major4 Major3 Major4 Major4 Major4 Major4 Major4 Major3 Major4
Major/Minor Minor2 Minor1 Major1 Major2 Conflicting Flow All 1694 2259 557 - - 566 1116 0 0 1131 0 0 Stage 1 1114 1114 -
Conflicting Flow All 1694 2259 557 - - 566 1116 0 0 1131 0 0 Stage 1 1114 1114 -
Conflicting Flow All 1694 2259 557 566 1116 0 0 1131 0 0 Stage 1 1114 1114
Conflicting Flow All 1694 2259 557 - - 566 1116 0 0 1131 0 0 Stage 1 1114 1114 -
Stage 1 1114 1114 - <
Stage 2 580 1145 - <t< td=""></t<>
Critical Hdwy 7.54 6.54 6.94 - - 6.94 4.14 - - 4.14 - - 4.14 - - 4.14 - - 4.14 - - 4.14 - - 4.14 - <t< td=""></t<>
Critical Hdwy Stg 2 6.54 5.54 -<
Follow-up Hdwy 3.52 4.02 3.32 3.32 2.22 2.22 Pot Cap-1 Maneuver 60 41 474 0 0 467 622 613 Stage 1 222 282 - 0 0 Stage 2 467 272 - 0 0 Platoon blocked, % 467 622 613
Pot Cap-1 Maneuver 60 41 474 0 0 467 622 - - 613 - - Stage 1 222 282 - 0 0 -
Stage 1 222 282 - 0 0 - <th< td=""></th<>
Stage 2 467 272 - 0 0 - <th< td=""></th<>
Platoon blocked, %
Mov Cap-1 Maneuver 58 41 474 - - 467 622 - - 613 - - Mov Cap-2 Maneuver 58 41 -
Mov Cap-2 Maneuver 58 41
Stane 1 770 787
o de la companya de
Stage 2 449 269
Approach EB WB NB SB
HCM Control Delay, s 66.6 12.9 0.1 0
HCM LOS F B
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR
Capacity (veh/h) 622 74 467 613
HCM Lane V/C Ratio 0.011 0.216 0.028
HCM Control Delay (s) 10.9 66.6 12.9 0
HCM Lane LOS B F B A
HCM 95th %tile Q(veh) 0 0.8 0.1 0

Intersection						
Int Delay, s/veh	3.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥			र्स	Þ	
Traffic Vol, veh/h	0	2	4	4	2	0
Future Vol, veh/h	0	2	4	4	2	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e, # 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	2	4	4	2	0
WWW.CT IOW		_	•	•	_	· ·
	Minor2		Major1		/lajor2	
Conflicting Flow All	14	2	2	0	-	0
Stage 1	2	-	-	-	-	-
Stage 2	12	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	1005	1082	1620	-	_	-
Stage 1	1021	-	-	-		_
Stage 2	1011	_	_	_	-	_
Platoon blocked, %	1011			_	_	_
Mov Cap-1 Maneuver	1003	1082	1620	_	_	_
Mov Cap-1 Maneuver	1003	1002	1020		-	-
Stage 1	1019	-	-	-	-	-
· ·	1019	-		•	-	-
Stage 2	1011	-	-	-	-	-
Approach	EB		NB		SB	
HCM Control Delay, s	8.3		3.6		0	
HCM LOS	Α					
NA'	. 1	NDI	NDT	EDL1	CDT	CDD
Minor Lane/Major Mvm	10	NBL	MRI	EBLn1	SBT	SBR
Capacity (veh/h)		1620	-	1082	-	-
HCM Lane V/C Ratio		0.003		0.002	-	-
				0.0		
HCM Control Delay (s)		7.2	0	8.3	-	-
		7.2 A 0	O A	8.3 A 0	-	-

Intersection													
Int Delay, s/veh	20												
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
Lane Configurations		414	7		414	7		4			र्स	7	
Traffic Vol, veh/h	0	371	216	0	935	449	0	0	0	142	0	100	
Future Vol, veh/h	0	371	216	0	935	449	0	0	0	142	0	100	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield	
Storage Length	-	-	480	_	-	900	_	-	-	-	-	0	
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	_	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	412	240	0	995	478	0	0	0	165	0	116	
		.,_			.,,	.,,				.00			
Major/Minor N	/lajor1		N	Major2		N	/linor1			Minor2			
Conflicting Flow All	995	0		412	0	0	910	1407	206	1201	1407	498	
Stage 1	770	-	-	412	-	-	412	412	200	995	995	470	
•	-	-	-	-	-	-	412	995	-	206	412	-	
Stage 2 Critical Hdwy	4.14		-	4.14			7.54	6.54	6.94	7.54	6.54	6.94	
<i>,</i>	4.14	-	-	4.14	-	-	6.54	5.54		6.54	5.54		
Critical Hdwy Stg 1	-	-	-	-	-	-			-			-	
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-	
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32	
Pot Cap-1 Maneuver	691	-	0	1143	-	0	230	138		~ 140	138	518	
Stage 1	-	-	0	-	-	0	588	593	-	262	321	-	
Stage 2	-	-	0	-	-	0	523	321	-	777	593	-	
Platoon blocked, %	101	-		4440	-		470	100	000	1.10	400	E40	
Mov Cap-1 Maneuver	691	-	-	1143	-	-	178	138		~ 140	138	518	
Mov Cap-2 Maneuver	-	-	-	-	-	-	178	138		~ 140	138	-	
Stage 1	-	-	-	-	-	-	588	593	-	262	321	-	
Stage 2	-	-	-	-	-	-	406	321	-	777	593	-	
Approach	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			120			
HCM LOS							Α			F			
Minor Lane/Major Mvm	<u>t </u>	VELn1	NWL	NWT	SEL	SETS	WLn1S	SWLn2					
Capacity (veh/h)		-	1143	-	691	-	140	518					
HCM Lane V/C Ratio		-	-	-	-	-	1.179	0.224					
HCM Control Delay (s)		0	0	-	0	-	194.7	14					
HCM Lane LOS		Α	Α	-	Α	-	F	В					
HCM 95th %tile Q(veh)		-	0	-	0	-	9.6	0.9					
Notes													
~: Volume exceeds cap	acity	\$. Do	elay exc	eeds 3	00s	+: Com	nutatio	n Not D	efined	*. ∆II	maiory	nluma i	in platoon
. Volume exceeds cap	acity	ψ. De	nay thu	ccus 3	003	i. Cull	palaliul	ים זטור ד	CIIIICU	. <i>H</i> III	major \	rolume I	η ριαισση

	*	→	-	~	←	*_	\	\mathbf{x}	4	•	*	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	Į.	†	77	1,1	f)		Ť	∱ }		¥	ተተተ	
Traffic Volume (veh/h)	403	3	692	0	0	0	0	462	0	0	1144	0
Future Volume (veh/h)	403	3	692	0	0	0	0	462	0	0	1144	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	415	3	0	0	0	0	0	502	0	0	1285	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	726	545		414	545	0	207	1598	0	207	2296	0
Arrive On Green	0.29	0.29	0.00	0.00	0.00	0.00	0.00	0.45	0.00	0.00	0.45	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	430	3647	0	896	5274	0
Grp Volume(v), veh/h	415	3	0	0	0	0	0	502	0	0	1285	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1371	1870	0	430	1777	0	896	1702	0
Q Serve(g_s), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.1	0.0	0.0	6.4	0.0
Cycle Q Clear(g_c), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.1	0.0	0.0	6.4	0.0
Prop In Lane	1.00	0.0	1.00	1.00	0.0	0.00	1.00	5.1	0.00	1.00	0.4	0.00
Lane Grp Cap(c), veh/h	726	545	1.00	414	545	0.00	207	1598	0.00	207	2296	0.00
V/C Ratio(X)	0.57	0.01		0.00	0.00	0.00	0.00	0.31	0.00	0.00	0.56	0.00
Avail Cap(c_a), veh/h	1130	969		1036	969	0.00	298	2352	0.00	397	3379	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.4	8.7	0.0	0.00	0.00	0.00	0.0	6.1	0.00	0.00	7.0	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0
%ile BackOfQ(50%),veh/ln	1.9	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.0	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.0	0.0
LnGrp Delay(d),s/veh	12.1	8.7	0.0	0.0	0.0	0.0	0.0	6.2	0.0	0.0	7.2	0.0
LnGrp LOS	12.1 B	Α	0.0	Α	Α	Α	Α	0.2 A	Α	Α	Α.2	Α
	D		٨		0			502			1285	
Approach Vol, veh/h		418	А									
Approach LOS		12.1			0.0			6.2			7.2	
Approach LOS		В						Α			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		20.1		14.6		20.1		14.6				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+I1), s		8.4		9.5		5.1		0.0				
Green Ext Time (p_c), s		7.2		0.8		2.8		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			7.9									
HCM 6th LOS			Α									
Notos												

Intersection												
Int Delay, s/veh	0.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7	ሻ	ħβ		ሻ	^	7
Traffic Vol, veh/h	5	0	3	0	0	0	3	1110	0	0	1152	2
Future Vol, veh/h	5	0	3	0	0	0	3	1110	0	0	1152	2
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	:,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	58	58	58	92	92	92	92	92	92	97	97	97
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	0	5	0	0	0	3	1207	0	0	1188	2
Major/Minor N	Minor2		ľ	Minor1		N	Major1		N	Major2		
Conflicting Flow All	1798	2401	594	-	-	604	1190	0	0	1207	0	0
Stage 1	1188	1188	-	-	-	-	-	-	-	-	-	-
Stage 2	610	1213	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-		-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	50	33	448	0	0	441	582	-	-	574	-	-
Stage 1	200	260	-	0	0	-	-	-	-	-	-	-
Stage 2	448	253	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	50	33	448	-	-	441	582	-	-	574	-	-
Mov Cap-2 Maneuver	50	33	-	-	-	-	-	-	-	-	-	-
Stage 1	199	260	-	-	-	-	-	-	-	-	-	-
Stage 2	446	252	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	63.5			0			0			0		
HCM LOS	F			Α								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		582	-	-	75	-	574	-				
HCM Lane V/C Ratio		0.006	_		0.184	_	- 374	_	_			
HCM Control Delay (s)		11.2	-	_	63.5	0	0	_	_			
HCM Lane LOS		В	_	_	F	A	A	_	_			
HCM 95th %tile Q(veh))	0	-	-	0.6	-	0	-	-			
/ 5 / 5 6 (V 011)					3.0							

Intersection						
Int Delay, s/veh	4.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	₩.	LDI	NDL	<u>₩</u>		אטכ
Traffic Vol, veh/h	T	4	3	식 2	1 >	0
Future Vol, veh/h	0	4	3	2	4	0
·	0	0	0	0	0	0
Conflicting Peds, #/hr				Free		
Sign Control RT Channelized	Stop -	Stop None	Free		Free	Free
			-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	4	3	2	4	0
Major/Minor I	Minor2		Major1	N	/lajor2	
Conflicting Flow All	12	4	4	0		0
Stage 1	4	_	·	-	_	-
Stage 2	8	_	_	_	_	_
Critical Hdwy	6.42	6.22	4.12	_		_
Critical Hdwy Stg 1	5.42	-	-	_		_
Critical Hdwy Stg 2	5.42	_	_	_	_	_
Follow-up Hdwy	3.518	3.318		_	_	_
Pot Cap-1 Maneuver	1008	1080	1618			
Stage 1	1019	1000	1010			
Stage 2	1019			-	-	
	1015	-	-	-		-
Platoon blocked, %	100/	1000	1/10	-	-	-
Mov Cap-1 Maneuver	1006	1080	1618	-	-	-
Mov Cap-2 Maneuver	1006	-	-	-	-	-
Stage 1	1017	-	-	-	-	-
Stage 2	1015	-	-	-	-	-
Approach	EB		NB		SB	
HCM Control Delay, s	8.3		4.3		0	
HCM LOS	A		1.0		U	
TIOWI LOO						
Minor Lane/Major Mvm	nt	NBL		EBLn1	SBT	SBR
Capacity (veh/h)		1618	-	1080	-	-
HCM Lane V/C Ratio		0.002	-	0.004	-	-
HCM Control Delay (s)		7.2	0	8.3	-	-
HCM Lane LOS		Α	Α	Α	-	-
HCM 95th %tile Q(veh))	0	-	0	-	-

APPENDIX E PROPOSED BUILD TRAFFIC OPERATIONS



Intersection												
Int Delay, s/veh	10											
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		414	7		414	7		4			र्स	7
Traffic Vol, veh/h	0	580	474	0	434	569	0	0	0	167	0	72
Future Vol, veh/h	0	580	474	0	434	569	0	0	0	167	0	72
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0
Veh in Median Storage	.,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	88	88	88	87	87	87	92	92	92	76	76	76
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	659	539	0	499	654	0	0	0	220	0	95
Major/Minor N	Major1			Major2		N	/linor1		ľ	Minor2		
Conflicting Flow All	499	0	-	659	0	0	909	1158	330	829	1158	250
Stage 1	-	-	-	-	-	-	659	659	-	499	499	-
Stage 2	-	-	-	-	-	-	250	499	-	330	659	-
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32
Pot Cap-1 Maneuver	1061	-	0	925	-	0	230	195	666	263	195	750
Stage 1	-	-	0	-	-	0	419	459	-	522	542	-
Stage 2	-	-	0	-	-	0	732	542	-	657	459	-
Platoon blocked, %		-			-							
Mov Cap-1 Maneuver	1061	-	-	925	-	-	201	195	666	263	195	750
Mov Cap-2 Maneuver	-	-	-	-	-	-	201	195	-	263	195	-
Stage 1	-	-	-	-	-	-	419	459	-	522	542	-
Stage 2	-	-	-	-	-	-	640	542	-	657	459	-
Approach	SE			NW			NE			SW		
HCM Control Delay, s	0			0			0			46.8		
HCM LOS	- 0						A			40.0 E		
110.11 200							,,					
Minor Long/Maior M		JEL1	NIVAZI	NIME	CEL	CETC	\\/I - 10	1\A/L = 2				
Minor Lane/Major Mvm	it ľ	VELn1	NWL	NWT	SEL		WLn1S					
Capacity (veh/h)		-	925	-	1061	-	263	750				
HCM Lane V/C Ratio		-	-	-	-		0.836					
HCM Control Delay (s)		0	0	-	0	-	62.4	10.5				
HCM Lane LOS		Α	A	-	A	-	F	В				
HCM 95th %tile Q(veh)		-	0	-	0	-	6.8	0.4				

	>	→	74	4	←	*_	\	×	4	+	*	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	ሻሻ	₽		ሻ	∱ ∱		ሻ	ተተተ	
Traffic Volume (veh/h)	183	2	345	0	0	0	0	673	0	0	986	0
Future Volume (veh/h)	183	2	345	0	0	0	0	673	0	0	986	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	235	3	0	0	0	0	0	732	0	0	1188	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	584	337		527	337	0	263	1743	0	263	2504	0
Arrive On Green	0.18	0.18	0.00	0.00	0.00	0.00	0.00	0.49	0.00	0.00	0.49	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	472	3647	0	724	5274	0
Grp Volume(v), veh/h	235	3	0	0	0	0	0	732	0	0	1188	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1371	1870	0	472	1777	0	724	1702	0
Q Serve(g_s), s	3.4	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.2	0.0
Cycle Q Clear(g_c), s	3.4	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.2	0.0
Prop In Lane	1.00	0.0	1.00	1.00	0.0	0.00	1.00	0.0	0.00	1.00	1.2	0.00
Lane Grp Cap(c), veh/h	584	337	1.00	527	337	0	263	1743	0.00	263	2504	0.00
V/C Ratio(X)	0.40	0.01		0.00	0.00	0.00	0.00	0.42	0.00	0.00	0.47	0.00
Avail Cap(c_a), veh/h	1437	1232		1840	1232	0	429	2991	0.00	518	4298	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	10.6	9.2	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	4.6	0.0
Incr Delay (d2), s/veh	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.1	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
LnGrp Delay(d),s/veh	11.0	9.2	0.0	0.0	0.0	0.0	0.0	4.6	0.0	0.0	4.8	0.0
LnGrp LOS	В	Α.	0.0	Α	Α	Α	Α	4.0 A	Α	Α	4.0 A	Α
Approach Vol, veh/h	ט	238	А		0			732			1188	
		11.0	А		0.0			4.6			4.8	
Approach LOS					0.0							
Approach LOS		В						А			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		17.9		9.4		17.9		9.4				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		6.2		5.4		5.6		0.0				
Green Ext Time (p_c), s		7.2		0.5		4.3		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			5.4									
HCM 6th LOS			Α									
Notes												

Intersection													
Int Delay, s/veh	62.2												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		4				7		ħβ		ች	^	7	
Traffic Vol, veh/h	35	0	12	0	0	0	11	983	0	0	1003	8	
Future Vol, veh/h	35	0	12	0	0	0	11	983	0	0	1003	8	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0	
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	25	25	25	92	92	92	85	85	85	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	140	0	48	0	0	0	13	1156	0	0	1114	9	
Major/Minor	Minor2		ľ	/linor1		N	Major1		N	Major2			
Conflicting Flow All	1718	2296	557		_	578	1123	0		1156	0	0	
Stage 1	1114	1114	-	_	_	-	-	-	-	-	-	-	
Stage 2	604	1182	_	_	_	_	_		_	_	_	_	
Critical Hdwy	7.54	6.54	6.94	_	_	6.94	4.14	-		4.14	_	-	
Critical Hdwy Stg 1	6.54	5.54	- 0.71	_	_	-			_		_	_	
Critical Hdwy Stg 2	6.54	5.54	-	_	_	_	_	_	_	_	_	_	
Follow-up Hdwy	3.52	4.02	3.32	_	_	3.32	2.22		_	2.22	_	_	
Pot Cap-1 Maneuver	~ 58	38	474	0	0	459	618	_	-	600	_	_	
Stage 1	222	282	-	0	0	-	-	_	-	-	_	_	
Stage 2	452	262	-	0	0	_	_	_	_	_	_	_	
Platoon blocked, %	102	202						_	_		_	_	
Mov Cap-1 Maneuver	~ 57	37	474	_	_	459	618	_	-	600	_	_	
Mov Cap-2 Maneuver	~ 57	37	-	_	_	-	-	_		-	_		
Stage 1	217	282	-	-	-	-	-	-	-	_	-	-	
Stage 2	442	256	-	-	-	-	-	-		-	-	-	
2.250 2		_00											
Approach	EB			WB			NB			SB			
HCM Control Delay, s				0			0.1			0			
HCM LOS	F F			A			0.1			U			
TICIVI LOS	ı												
Minor Lane/Major Mvn	nt	NBL	NBT	MRR	EBLn1V	VRI n1	SBL	SBT	SBR				
			HUI	NUN			600	301	JUK				
Capacity (veh/h) HCM Lane V/C Ratio		618 0.021	-	-	74 2.541	-		-	-				
	\		-			-	_	-	-				
HCM Control Delay (s) HCM Lane LOS		10.9	-		819.5	0	0	-	-				
)	B	-	-	F 10 1	А	A	-	-				
HCM 95th %tile Q(veh	l)	0.1	-	-	18.1	-	0	-	-				
Notes													
~: Volume exceeds ca	pacity	\$: De	elay exc	eeds 30	00s	+: Com	putatior	Not De	efined	*: All	major v	olume i	in platoon

Intersection						
Int Delay, s/veh	7.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥			4	4	05.1
Traffic Vol, veh/h	0	45	15	4	2	0
Future Vol, veh/h	0	45	15	4	2	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	_	-	_	-
Veh in Median Storage		-	_	0	0	_
Grade, %	0	_	_	0	0	_
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	0	49	16	4	2	0
IVIVIII I IOVV	U	77	10	-		U
	Minor2		Major1		/lajor2	
Conflicting Flow All	38	2	2	0	-	0
Stage 1	2	-	-	-	-	-
Stage 2	36	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	974	1082	1620	-	-	-
Stage 1	1021	-	-	-	-	-
Stage 2	986	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	964	1082	1620	-	-	-
Mov Cap-2 Maneuver	964	-	-	-	-	-
Stage 1	1011	-	-	-	-	-
Stage 2	986	_	-	-	-	-
5 15 gt =						
Annraaah	ΓВ		ND		CD	
Approach	EB		NB		SB	
HCM Control Delay, s	8.5		5.7		0	
HCM LOS	А					
Minor Lane/Major Mvm	nt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)		1620		1082	_	
HCM Lane V/C Ratio		0.01		0.045	_	_
HCM Control Delay (s)		7.2	0	8.5	_	_
HCM Lane LOS		Α.2	A	Α	_	_
HCM 95th %tile Q(veh)	0	-	0.1	_	_
HOW FOR FORME Q(VCH)	,	U		0.1		

Intersection						
Int Delay, s/veh	0					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1>	LUK	VVDL	₩ <u>₩</u>	₩.	אטוז
Traffic Vol, veh/h	2	0	0	4	0	0
Future Vol, veh/h	2	0	0	4	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	310p	None
Storage Length		-	_	-	0	-
Veh in Median Storage, #	# 0	_	-	0	0	_
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	2	0	0	4	0	0
IVIVIIIL FIOW	Z	U	U	4	U	U
Major/Minor Ma	ajor1	N	Major2	1	Vinor1	
Conflicting Flow All	0	0	2	0	6	2
Stage 1	-	-	-	-	2	-
Stage 2	-	-	-	-	4	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	_	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	0.540	3.318
Pot Cap-1 Maneuver	-	_	1620	_	1015	1082
Stage 1	-			-	1021	-
Stage 2	-	_	_	_	1019	_
Platoon blocked, %	_	_		_	1017	
Mov Cap-1 Maneuver	_	_	1620	-	1015	1082
Mov Cap-1 Maneuver	_		1020	_	1015	1002
Stage 1	-			_	1013	-
ů .		-	-		1021	
Stage 2	-	-	-	-	1019	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		0		0	
HCM LOS					Α	
Minor Long/Major M. mat	N	IDI n1	EDT	EDD	WDI	WDT
	ľ	VBLn1	EBT	EBR	WBL	WBT
Minor Lane/Major Mvmt				-	1620	-
Capacity (veh/h)		-	-			
Capacity (veh/h) HCM Lane V/C Ratio		-	-	-	-	-
Capacity (veh/h) HCM Lane V/C Ratio HCM Control Delay (s)		0	-	-	0	-
Capacity (veh/h) HCM Lane V/C Ratio			-	-	-	

Intersection													
Int Delay, s/veh	21.8												
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
Lane Configurations		414	1		414	7		4			स	1	
Traffic Vol, veh/h	0	378	216	0	942	453	0	0	0	145	0	100	
Future Vol, veh/h	0	378	216	0	942	453	0	0	0	145	0	100	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-		
Storage Length	_	_	480	_	_	900	_	_	-	_	_	0	
Veh in Median Storage	.# -	0	-	-	0	-	_	0	_	-	0	-	
Grade, %	-	0	_	_	0	_	_	0	_	_	0	_	
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Nymt Flow	0	420	240	0	1002	482	0	0	0	169	0	116	
WIVIIII I IOW	U	720	240	U	1002	702	U	U	U	107	U	110	
Major/Minor	Najor1		n	Major2			liner1		, n	/liner?			
	/lajor1	^		Major2	^		Minor1	1400		Minor2	1400	F04	
Conflicting Flow All	1002	0	-	420	0	0	921	1422	210	1212	1422	501	
Stage 1	-	-	-	-	-	-	420	420	-	1002	1002	-	
Stage 2	-	-	-	-	-	-	501	1002	-	210	420	-	
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94	
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-	
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-	
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32	
Pot Cap-1 Maneuver	687	-	0	1136	-	0	225	135	796	~ 138	135	515	
Stage 1	-	-	0	-	-	0	581	588	-	260	318	-	
Stage 2	-	-	0	-	-	0	521	318	-	773	588	-	
Platoon blocked, %		-			-								
Mov Cap-1 Maneuver	687	-	-	1136	-	-	174	135		~ 138	135	515	
Mov Cap-2 Maneuver	-	-	-	-	-	-	174	135	-	~ 138	135	-	
Stage 1	-	-	-	-	-	-	581	588	-	260	318	-	
Stage 2	-	-	-	-	-	-	403	318	-	773	588	-	
Approach	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			130.4			
HCM LOS							A			F			
Minor Lane/Major Mvm	t N	NELn1	NWL	NWT	SEL	SETS	SWLn1S	:\\\\ n2					
	t ľ	VL LIII				JLIS							
Capacity (veh/h)		-	1136	-	687	-	138	515					
HCM Cantral Palov (a)		-	-	-	-		1.222						
HCM Control Delay (s)		0	0	-	0	-	210.7	14					
HCM Lane LOS		Α	A	-	A	-	F	В					
HCM 95th %tile Q(veh)		-	0	-	0	-	10.1	0.9					
Notes													
~: Volume exceeds cap	acity	\$: De	lay exc	eeds 3	00s	+: Com	putatior	Not D	efined	*: All	major v	/olume i	in platoon

	>	→	74	4	←	*_	\	×	4	*	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	ሻሻ	₽		ሻ	∱ ∱		ሻ	ተተተ	
Traffic Volume (veh/h)	403	3	706	0	0	0	0	471	0	0	1157	0
Future Volume (veh/h)	403	3	706	0	0	0	0	471	0	0	1157	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	415	3	0	0	0	0	0	512	0	0	1300	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	724	544		412	544	0	206	1605	0	206	2306	0
Arrive On Green	0.29	0.29	0.00	0.00	0.00	0.00	0.00	0.45	0.00	0.00	0.45	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	424	3647	0	888	5274	0
Grp Volume(v), veh/h	415	3	0	0	0	0	0	512	0	0	1300	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1371	1870	0	424	1777	0	888	1702	0
Q Serve(g_s), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.2	0.0	0.0	6.6	0.0
Cycle Q Clear(q_c), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.2	0.0	0.0	6.6	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	724	544		412	544	0	206	1605	0	206	2306	0
V/C Ratio(X)	0.57	0.01		0.00	0.00	0.00	0.00	0.32	0.00	0.00	0.56	0.00
Avail Cap(c_a), veh/h	1123	963		1025	963	0	293	2337	0	389	3358	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.5	8.8	0.0	0.0	0.0	0.0	0.0	6.1	0.0	0.0	7.1	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.9	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.1	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•••	0.0
LnGrp Delay(d),s/veh	12.2	8.8	0.0	0.0	0.0	0.0	0.0	6.3	0.0	0.0	7.3	0.0
LnGrp LOS	В	Α	0.0	Α	A	A	Α	Α	Α	Α	7.5 A	Α
Approach Vol, veh/h		418	А		0			512			1300	
Approach Delay, s/veh		12.2	٨		0.0			6.3			7.3	
Approach LOS		12.2 B			0.0			۸			7.3 A	
Approach LOS		D						А			А	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		20.3		14.7		20.3		14.7				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+I1), s		8.6		9.5		5.2		0.0				
Green Ext Time (p_c), s		7.2		8.0		2.9		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			8.0									
HCM 6th LOS			Α									
Notes												

Intersection												
Int Delay, s/veh	4.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7	ች	ħβ		*	^	7
Traffic Vol, veh/h	21	0	12	0	0	0	26	1123	0	0	1152	25
Future Vol, veh/h	21	0	12	0	0	0	26	1123	0	0	1152	25
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	58	58	58	92	92	92	92	92	92	97	97	97
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	36	0	21	0	0	0	28	1221	0	0	1188	26
Major/Minor I	Minor2		ľ	Minor1		N	/lajor1		N	Major2		
Conflicting Flow All	1855	2465	594	-	-	611	1214	0	0	1221	0	0
Stage 1	1188	1188	-	-	-	-	-	-	-	-	-	-
Stage 2	667	1277	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	46	30	448	0	0	437	570	-	-	567	-	-
Stage 1	200	260	-	0	0	-	-	-	-	-	-	-
Stage 2	414	236	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	44	29	448	-	-	437	570	-	-	567	-	-
Mov Cap-2 Maneuver	44	29	-	-	-	-	-	-	-	-	-	-
Stage 1	190	260	-	-	-	-	-	-	-	-	-	-
Stage 2	394	224	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	182.7			0			0.3			0		
HCM LOS	F			A								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR E	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		570	-	-	65	-	567	-	-			
HCM Lane V/C Ratio		0.05	-	-	0.875	-	-	-	-			
HCM Control Delay (s)		11.6	-		182.7	0	0	-	-			
HCM Lane LOS		В	-	-	F	Α	Α	-	-			
HCM 95th %tile Q(veh))	0.2	-	-	4.1	-	0	-	-			

SBT	SBR
	SBR
	ODIN
-	
4	0
4	0
0	0
	Free
	INOTIC
	_
	-
	92
	2
4	0
Major2	
_	0
-	-
-	-
-	-
_	_
-	_
-	_
-	_
_	_
_	_
_	_
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-	-
	-
-	-
-	-
SB	
0	
CDT	CDD
	SBR
	-
	-
-	-
-	-
	Free 0 0 92 2 4 Major2

Intersection						
Int Delay, s/veh	0					
	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations		LDK	WDL			NDK
Traffic Vol, veh/h	♣	0	0	र्स 2	¥	0
Future Vol, veh/h	4	0	0	2	0	0
·	0	0	0	0	0	0
Conflicting Peds, #/hr		Free	Free	Free		
Sign Control RT Channelized	Free	None		None	Stop -	Stop
	-		-			None
Storage Length		-	-	-	0	-
Veh in Median Storage, a		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	0	0	2	0	0
Major/Minor Ma	ajor1	N	Major2	1	Vinor1	
Conflicting Flow All	0	0	4	0	6	4
Stage 1	-	-	-	-	4	-
Stage 2	-	-	-	-	2	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	_	_	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	3.318
Pot Cap-1 Maneuver	-	-	1618	_	1015	1080
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	_	_	1021	-
Platoon blocked, %	-			-		
Mov Cap-1 Maneuver	_	_	1618	-	1015	1080
Mov Cap-2 Maneuver	_	_	-	_	1015	-
Stage 1	_	_	_	_	1019	_
Stage 2	_	_	_	_	1021	_
Stage 2					1021	
Approach	EB		WB		NB	
HCM Control Delay, s	0		0		0	
HCM LOS					Α	
Minor Lane/Major Mvmt	N	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	<u>'</u>	-	-		1618	-
HCM Lane V/C Ratio		-	-	-	1010	-
HCM Control Delay (s)		0	-	_	0	
HCM Lane LOS		A	-	-	A	-
HCM 95th %tile Q(veh)		А	-	-	0	-
1101VI 73111 /01118 (2(VEII)		_	-	-	U	-

APPENDIX F PROPOSED BUILD TRAFFIC OPERATIONS WITH IMPROVEMENTS



Intersection												
Int Delay, s/veh	10											
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		414	7		414	7		4			र्स	7
Traffic Vol, veh/h	0	580	474	0	434	569	0	0	0	167	0	72
Future Vol, veh/h	0	580	474	0	434	569	0	0	0	167	0	72
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0
Veh in Median Storage	.,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	88	88	88	87	87	87	92	92	92	76	76	76
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	659	539	0	499	654	0	0	0	220	0	95
Major/Minor N	Major1			Major2		N	/linor1		ľ	Minor2		
Conflicting Flow All	499	0	-	659	0	0	909	1158	330	829	1158	250
Stage 1	-	-	-	-	-	-	659	659	-	499	499	-
Stage 2	-	-	-	-	-	-	250	499	-	330	659	-
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-
Follow-up Hdwy	2.22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32
Pot Cap-1 Maneuver	1061	-	0	925	-	0	230	195	666	263	195	750
Stage 1	-	-	0	-	-	0	419	459	-	522	542	-
Stage 2	-	-	0	-	-	0	732	542	-	657	459	-
Platoon blocked, %		-			-							
Mov Cap-1 Maneuver	1061	-	-	925	-	-	201	195	666	263	195	750
Mov Cap-2 Maneuver	-	-	-	-	-	-	201	195	-	263	195	-
Stage 1	-	-	-	-	-	-	419	459	-	522	542	-
Stage 2	-	-	-	-	-	-	640	542	-	657	459	-
Approach	SE			NW			NE			SW		
HCM Control Delay, s	0			0			0			46.8		
HCM LOS	- 0						A			40.0 E		
110.11 200							,,					
Minor Long/Maior M		JEL1	NIVAZI	NIME	CEL	CETC	\\/I - 10	·\\// 2				
Minor Lane/Major Mvm	it ľ	VELn1	NWL	NWT	SEL		WLn1S					
Capacity (veh/h)		-	925	-	1061	-	263	750				
HCM Lane V/C Ratio		-	-	-	-		0.836					
HCM Control Delay (s)		0	0	-	0	-	62.4	10.5				
HCM Lane LOS		Α	A	-	A	-	F	В				
HCM 95th %tile Q(veh)		-	0	-	0	-	6.8	0.4				

	>	→	74	4	←	*_	\	×	4	+	*	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	ሻሻ	₽		ሻ	∱ ∱		ሻ	ተተተ	
Traffic Volume (veh/h)	183	2	345	0	0	0	0	673	0	0	986	0
Future Volume (veh/h)	183	2	345	0	0	0	0	673	0	0	986	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	235	3	0	0	0	0	0	732	0	0	1188	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	584	337		527	337	0	263	1743	0	263	2504	0
Arrive On Green	0.18	0.18	0.00	0.00	0.00	0.00	0.00	0.49	0.00	0.00	0.49	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	472	3647	0	724	5274	0
Grp Volume(v), veh/h	235	3	0	0	0	0	0	732	0	0	1188	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1371	1870	0	472	1777	0	724	1702	0
Q Serve(g_s), s	3.4	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.2	0.0
Cycle Q Clear(g_c), s	3.4	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	4.2	0.0
Prop In Lane	1.00	0.0	1.00	1.00	0.0	0.00	1.00	0.0	0.00	1.00	1.2	0.00
Lane Grp Cap(c), veh/h	584	337	1.00	527	337	0	263	1743	0.00	263	2504	0.00
V/C Ratio(X)	0.40	0.01		0.00	0.00	0.00	0.00	0.42	0.00	0.00	0.47	0.00
Avail Cap(c_a), veh/h	1437	1232		1840	1232	0	429	2991	0.00	518	4298	0.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	10.6	9.2	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	4.6	0.0
Incr Delay (d2), s/veh	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.1	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
LnGrp Delay(d),s/veh	11.0	9.2	0.0	0.0	0.0	0.0	0.0	4.6	0.0	0.0	4.8	0.0
LnGrp LOS	В	Α.	0.0	Α	Α	Α	Α	4.0 A	Α	Α	4.0 A	Α
Approach Vol, veh/h	ט	238	А		0			732			1188	
		11.0	А		0.0			4.6			4.8	
Approach LOS					0.0							
Approach LOS		В						А			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		17.9		9.4		17.9		9.4				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		6.2		5.4		5.6		0.0				
Green Ext Time (p_c), s		7.2		0.5		4.3		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			5.4									
HCM 6th LOS			Α									
Notes												

Intersection												
Int Delay, s/veh	1.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7	ሻ	ħβ		ሻ	^	7
Traffic Vol, veh/h	0	0	47	0	0	0	11	983	0	0	1003	8
Future Vol, veh/h	0	0	47	0	0	0	11	983	0	0	1003	8
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	2,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	25	25	25	92	92	92	85	85	85	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	188	0	0	0	13	1156	0	0	1114	9
Major/Minor 1	Minor2		1	Minor1		ľ	Major1		N	Major2		
Conflicting Flow All	1718	2296	557	-	-	578	1123	0	0	1156	0	0
Stage 1	1114	1114	-	-	-	-	-	-	-	-	-	-
Stage 2	604	1182	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	58	38	474	0	0	459	618	-	-	600	-	-
Stage 1	222	282	-	0	0	-	-	-	-	-	-	-
Stage 2	452	262	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %						_		-	-		-	-
Mov Cap-1 Maneuver	57	37	474	-	-	459	618	-	-	600	-	-
Mov Cap-2 Maneuver	57	37	-	-	-	-	-	-	-	-	-	-
Stage 1	217	282	-	-	-	-	-	-	-	-	-	-
Stage 2	442	256	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	17.5			0			0.1			0		
HCM LOS	С			Α								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		618	-	-	474	-	600	_	_			
HCM Lane V/C Ratio		0.021	_		0.397	-	-	_	_			
HCM Control Delay (s)		10.9	-	-		0	0	-	-			
HCM Lane LOS		В	-	-	С	Ā	A	-	_			
HCM 95th %tile Q(veh))	0.1	-	-	1.9	-	0	-	-			

Intersection						
Int Delay, s/veh	7.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
		EBK	NDL			SBK
Lane Configurations	Y	45	15	<u>ન</u>	ન	٥
Traffic Vol, veh/h	0	45	15	4	2	0
Future Vol, veh/h	0	45	15	4	2	0
Conflicting Peds, #/hr	0	0	0	0	_ 0	_ 0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	49	16	4	2	0
Major/Minor	Minor2	1	Major1	N	/lajor2	
Conflicting Flow All	38	2	2	0	- najorz	0
Stage 1	2	-	-	-	_	-
Stage 2	36	_	_	_	_	_
Critical Hdwy	6.42	6.22	4.12	-		-
	5.42	0.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42		-	-	-	-
Critical Hdwy Stg 2		2 210	2 210	-	-	-
Follow-up Hdwy	3.518		2.218	-	-	-
Pot Cap-1 Maneuver	974	1082	1620	-	-	-
Stage 1	1021	-	-	-	-	-
Stage 2	986	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	964	1082	1620	-	-	-
Mov Cap-2 Maneuver	964	-	-	-	-	-
Stage 1	1011	-	-	-	-	-
Stage 2	986	-	-	-	-	-
Approach	EB		NB		SB	
	8.5		5.7		0	
HCM Control Delay, s			5.7		U	
HCM LOS	Α					
Minor Lane/Major Mvm	nt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)		1620	_	1082	-	_
HCM Lane V/C Ratio		0.01		0.045	-	_
HCM Control Delay (s)		7.2	0	8.5	-	-
HCM Lane LOS		A	A	A	_	_
HCM 95th %tile Q(veh)	0	-	0.1	_	_
115W 75W 70W Q(VCI)	1	U		0.1		

Intersection						
Int Delay, s/veh	0					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations		LDK	WDL		NDL W	MOR
Traffic Vol., veh/h	†	٥	٥	<u>ન</u>		٥
· ·	2	0	0	4	0	0
Future Vol, veh/h			0	4	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	2	0	0	4	0	0
Major/Minor M	ajor1	N	Major2	ı	Minor1	
Conflicting Flow All	0	0	2	0	6	2
Stage 1	-	U		-	2	-
Stage 2	-	-	-	-	4	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
J		-	4.12		5.42	0.22
Critical Hdwy Stg 1	-	-	-	-	5.42	
Critical Hdwy Stg 2	-	-	2 210	-		2 210
Follow-up Hdwy	-	-	2.218	-	3.518	
Pot Cap-1 Maneuver	-	-	1620	-	1015	1082
Stage 1	-	-	-	-	1021	-
Stage 2	-	-	-	-	1019	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1620	-	1015	1082
Mov Cap-2 Maneuver	-	-	-	-	1015	-
Stage 1	-	-	-	-	1021	-
Stage 2	-	-	-	-	1019	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		0		0	
HCM LOS					Α	
Minor Lane/Major Mvmt	1	VBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		-	-	-	1620	
HCM Lane V/C Ratio		_	_	_	-	_
HCM Control Delay (s)		0	_	_	0	_
HCM Lane LOS		A	_	_	A	_
HCM 95th %tile Q(veh)		-	-	-	0	_
How four four Q(veri)					U	

ntersection													
nt Delay, s/veh 21	.8												
Movement SI	EL S	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
ane Configurations	_	44	7		414	7		4			र्स	7	
Fraffic Vol, veh/h		378	216	0	942	453	0	0	0	145	0	100	
-uture Vol, veh/h	0 3	378	216	0	942	453	0	0	0	145	0	100	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control From	ee F	ree	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Free	-	-	Free	-	-	None	-		Yield	
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0	
/eh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Nymt Flow	0 4	420	240	0	1002	482	0	0	0	169	0	116	
Asiar/Minor Maio	1			//olor)			Ninor1			Ninar?			
Major/Minor Majo			N	Major2			/linor1	1400		Minor2	1400	F04	
Conflicting Flow All 10		0	-	420	0	0	921	1422	210	1212	1422	501	
Stage 1	-	-	-	-	-	-	420	420	-	1002	1002	-	
Stage 2	-	-	-	-	-	-	501	1002	-	210	420	-	
Critical Hdwy 4.		-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94	
Critical Hdwy Stg 1	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-	
Critical Hdwy Stg 2	-	-	-	-	-	-	6.54	5.54	-	6.54	5.54	-	
	22	-	-	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32	
	87	-	0	1136	-	0	225	135		~ 138	135	515	
Stage 1	-	-	0	-	-	0	581	588	-	260	318	-	
Stage 2	-	-	0	-	-	0	521	318	-	773	588	-	
Platoon blocked, %	07	-		1101	-		474	405	70/	100	405	E45	
	87	-	-	1136	-	-	174	135		~ 138	135	515	
Mov Cap-2 Maneuver	-	-	-	-	-	-	174	135		~ 138	135	-	
Stage 1	-	-	-	-	-	-	581	588	-	260	318	-	
Stage 2	-	-	-	-	-	-	403	318	-	773	588	-	
Approach S	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			130.4			
HCM LOS							A			F			
Minor Lanc/Major Mumt	NEI	l n1	NWL	NWT	SEL	CETC	WLn1S	:\\\\ n2					
Minor Lane/Major Mvmt	IVE					JE13							
Capacity (veh/h)		-	1136	-	687	-	138	515					
HCM Control Polov (c)		-	-	-	-		1.222						
HCM Control Delay (s)		0 A	0	-	0		210.7	14					
ICM Lang LOC		/\	Δ	-	Α	-	F	В					
HCM CEth (/tile O(yeh)			A										
HCM Lane LOS HCM 95th %tile Q(veh)		-	0	-	0	-	10.1	0.9					
						-							

	>	→	74	4	←	*_	\	*	4	+	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	7	^	77	ሻሻ	₽		7	∱ î≽		ሻ	ተተተ	
Traffic Volume (veh/h)	403	3	706	0	0	0	0	471	0	0	1157	0
Future Volume (veh/h)	403	3	706	0	0	0	0	471	0	0	1157	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	415	3	0	0	0	0	0	512	0	0	1300	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	724	544		412	544	0	206	1605	0	206	2306	0
Arrive On Green	0.29	0.29	0.00	0.00	0.00	0.00	0.00	0.45	0.00	0.00	0.45	0.00
Sat Flow, veh/h	1781	1870	2790	2743	1870	0	424	3647	0	888	5274	0
Grp Volume(v), veh/h	415	3	0	0	0	0	0	512	0	0	1300	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1371	1870	0	424	1777	0	888	1702	0
Q Serve(g_s), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.2	0.0	0.0	6.6	0.0
Cycle Q Clear(g_c), s	7.5	0.0	0.0	0.0	0.0	0.0	0.0	3.2	0.0	0.0	6.6	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	724	544		412	544	0	206	1605	0	206	2306	0
V/C Ratio(X)	0.57	0.01		0.00	0.00	0.00	0.00	0.32	0.00	0.00	0.56	0.00
Avail Cap(c_a), veh/h	1123	963		1025	963	0	293	2337	0	389	3358	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.5	8.8	0.0	0.0	0.0	0.0	0.0	6.1	0.0	0.0	7.1	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.9	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.1	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0
LnGrp Delay(d),s/veh	12.2	8.8	0.0	0.0	0.0	0.0	0.0	6.3	0.0	0.0	7.3	0.0
LnGrp LOS	В	A	0.0	A	A	A	A	A	A	A	A	A
Approach Vol, veh/h		418	А	-,,	0			512		,, <u> </u>	1300	
Approach Delay, s/veh		12.2	А		0.0			6.3			7.3	
Approach LOS		12.2			0.0			0.5 A			7.5 A	
•											A	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		20.3		14.7		20.3		14.7				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		8.6		9.5		5.2		0.0				
Green Ext Time (p_c), s		7.2		0.8		2.9		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			8.0									
HCM 6th LOS			А									
Notes												

Intersection												
Int Delay, s/veh	0.5											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDK	WDL	WDT	WBK	NDL	↑	אטוג	JDL N	<u>361</u>	JDK 7
Traffic Vol, veh/h	0	4	33	0	0	r 0	1 26	T № 1123	0	0	TT 1152	1 25
Future Vol, veh/h	0	0	33	0	0	0	26	1123	0	0	1152	25
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	Jiop -	- -	None	- -	Jiop -	None	-	-	None	-	-	None
Storage Length	-	-	-	_	-	0	80	_	-	200	_	0
Veh in Median Storage	e.# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	58	58	58	92	92	92	92	92	92	97	97	97
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	57	0	0	0	28	1221	0	0	1188	26
Major/Minor 1	Minor2		1	Minor1		N	Major1		N	Major2		
Conflicting Flow All	1855	2465	594	-	_	611	1214	0	0	1221	0	0
Stage 1	1188	1188	-	-	-	-	-	-	-	-	-	-
Stage 2	667	1277	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	46	30	448	0	0	437	570	-	-	567	-	-
Stage 1	200	260	-	0	0	-	-	-	-	-	-	-
Stage 2	414	236	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	44	29	448	-	-	437	570	-	-	567	-	-
Mov Cap-2 Maneuver	44	29	-	-	-	-	-	-	-	-	-	-
Stage 1	190	260	-	-	-	-	-	-	-	-	-	-
Stage 2	394	224	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	14.2			0			0.3			0		
HCM LOS	В			Α								
Minor Lane/Major Mvm	nt	NBL	NBT	NBR I	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		570	-	-		-	567	-	-			
HCM Lane V/C Ratio		0.05	_	_	0.127	-	-	_	-			
HCM Control Delay (s)		11.6	-	-		0	0	-	-			
HCM Lane LOS		В	-	-	В	A	A	-	-			
HCM 95th %tile Q(veh))	0.2	-	-	0.4	-	0	-	-			

Intersection						
Int Delay, s/veh	7.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	¥			4	♣	
Traffic Vol, veh/h	0	29	49	2	4	0
Future Vol, veh/h	0	29	49	2	4	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	_
Grade, %	0	_	_	0	0	_
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	0	32	53	2	4	0
WWW. TOW	J	02	00	_	•	U
				_		
	Minor2		Major1		/lajor2	
Conflicting Flow All	112	4	4	0	-	0
Stage 1	4	-	-	-	-	-
Stage 2	108	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	885	1080	1618	-	-	-
Stage 1	1019	-	-	-	-	-
Stage 2	916	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	856	1080	1618	-	-	-
Mov Cap-2 Maneuver	856	-	-	-	-	-
Stage 1	985	-	-	-	_	-
Stage 2	916	-	-	-	-	-
5 12 gt =						
			ND		0.0	
Approach	EB		NB		SB	
HCM Control Delay, s	8.4		7		0	
HCM LOS	Α					
Minor Lane/Major Mvm	nt	NBL	NRT I	EBLn1	SBT	SBR
Capacity (veh/h)		1618	-		-	ODIC
HCM Lane V/C Ratio		0.033		0.029	-	-
HCM Control Delay (s)		7.3	0	8.4	-	-
HCM Lane LOS		7.3 A	A	0.4 A	-	_
HCM 95th %tile Q(veh)	0.1	-	0.1		
110W 75W 70WE Q(VEH		U. I		0.1	•	_

Intersection						
Int Delay, s/veh	0					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1	LUK	VVDL	₩ <u>₩</u>	₩.	אטוז
Traffic Vol, veh/h	4	0	0	2	0	0
Future Vol, veh/h	4	0	0	2	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
ğ	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	0	0	2	0	0
N.A.;/N.A;	-!1		1-:		M:1	
	ajor1		Major2		Minor1	4
Conflicting Flow All	0	0	4	0	6	4
Stage 1	-	-	-	-	4	-
Stage 2	-	-	-	-	2	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	
Pot Cap-1 Maneuver	-	-	1618	-	1015	1080
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	1021	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1618	-	1015	1080
Mov Cap-2 Maneuver	-	-	-	-	1015	-
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	1021	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		0		0	
HCM LOS	U		U		A	
TIOM EGG					,,	
Minau Lana/Maiau Munat		IDI1	EDT	EDD	WDI	WDT
Minor Lane/Major Mvmt	ľ	VBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		-	-	-	1618	-
HCM Lane V/C Ratio		-	-	-	-	-
		0	_	-	0	-
HCM Control Delay (s)						
HCM Control Delay (s) HCM Lane LOS HCM 95th %tile Q(veh)		A	-	-	A 0	-

Intersection	
Int Delay, s/veh 12.8	
Movement SEL SET SER NWL NWT NWR NEL NET NER SWL SWT SW	SWR
Lane Configurations 4† † 4† † 4	7
	75
Future Vol, veh/h 0 605 493 0 451 592 0 0 0 174 0	75
Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0	0
	Stop
	Yield
Storage Length 480 900	0
Veh in Median Storage, #-000	-
Grade, % - 0 0 0	-
	76
Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2	2
Mvmt Flow 0 688 560 0 518 680 0 0 0 229 0	99
Major/Minor Major1 Major2 Minor1 Minor2	
Conflicting Flow All 518 0 - 688 0 0 947 1206 344 862 1206 2	259
Stage 1 688 688 - 518 518	-
Stage 2 259 518 - 344 688	-
	6.94
Critical Hdwy Stg 1 6.54 5.54 - 6.54 5.54	-
Critical Hdwy Stg 2 6.54 5.54 - 6.54 5.54	-
	3.32
	740
Stage 1 0 0 403 445 - 509 531	-
Stage 2 0 0 723 531 - 645 445	-
Platoon blocked, %	
Mov Cap-1 Maneuver 1044 902 187 182 652 249 182 7	740
Mov Cap-2 Maneuver 187 182 - 249 182	-
Stage 1 403 445 - 509 531	-
Stage 2 627 531 - 645 445	-
Approach SE NW NE SW	
HCM Control Delay, s 0 0 59.7	
HCM LOS A F	
non-250	
Minor Long/Major Mumt NEL p1 NIMI NIMI CEL CETCIMI p1CMI p2	
Minor Lane/Major Mvmt NELn1 NWL NWT SEL SETSWLn1SWLn2	
Capacity (veh/h) - 902 - 1044 - 249 740	
HCM Lane V/C Ratio 0.919 0.133	
HCM Control Delay (s) 0 0 - 0 - 80.8 10.6	
HCM Lane LOS A A - A - F B	
HCM 95th %tile Q(veh) - 0 - 8.1 0.5	

	>	→	-	4	←	*_	\	×	4	1	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	14.54	₽		ሻ	∱ }		ሻ	ተተተ	
Traffic Volume (veh/h)	190	1	360	0	0	0	0	703	0	0	1044	0
Future Volume (veh/h)	190	1	360	0	0	0	0	703	0	0	1044	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	244	1	0	0	0	0	0	764	0	0	1258	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	584	347		506	347	0	253	1771	0	253	2545	0
Arrive On Green	0.19	0.19	0.00	0.00	0.00	0.00	0.00	0.50	0.00	0.00	0.50	0.00
Sat Flow, veh/h	1781	1870	2790	2748	1870	0	441	3647	0	703	5274	0
Grp Volume(v), veh/h	244	1	0	0	0	0	0	764	0	0	1258	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1374	1870	0	441	1777	0	703	1702	0
Q Serve(g_s), s	3.7	0.0	0.0	0.0	0.0	0.0	0.0	3.9	0.0	0.0	4.7	0.0
Cycle Q Clear(g_c), s	3.7	0.0	0.0	0.0	0.0	0.0	0.0	3.9	0.0	0.0	4.7	0.0
Prop In Lane	1.00	0.0	1.00	1.00	0.0	0.00	1.00	0.7	0.00	1.00	•••	0.00
Lane Grp Cap(c), veh/h	584	347	1.00	506	347	0	253	1771	0	253	2545	0.00
V/C Ratio(X)	0.42	0.00		0.00	0.00	0.00	0.00	0.43	0.00	0.00	0.49	0.00
Avail Cap(c_a), veh/h	1378	1182		1732	1182	0	389	2870	0	470	4123	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	10.9	9.4	0.0	0.0	0.0	0.0	0.0	4.6	0.0	0.0	4.8	0.0
Incr Delay (d2), s/veh	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.1	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.3	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0
LnGrp Delay(d),s/veh	11.4	9.5	0.0	0.0	0.0	0.0	0.0	4.7	0.0	0.0	4.9	0.0
LnGrp LOS	В	A	0.0	A	A	A	A	Α	A	A	A	A
Approach Vol, veh/h		245	А		0			764			1258	
Approach Delay, s/veh		11.4	А		0.0			4.7			4.9	
Approach LOS		В			0.0			Α.			Α.	
											Д	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		18.7		9.8		18.7		9.8				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		6.7		5.7		5.9		0.0				
Green Ext Time (p_c), s		7.5		0.5		4.5		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			5.5									
HCM 6th LOS			Α									
Notes												_

Intersection												
Int Delay, s/veh	4.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LDL	4	LDIX	WDL	WDI	7	ሻ	†	NDIX	<u> </u>	^	7
Traffic Vol, veh/h	0	0	85	0	0	12	16	1041	0	0	1044	12
Future Vol, veh/h	0	0	85	0	0	12	16	1041	0	0	1044	12
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	25	25	25	92	92	92	85	85	85	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	340	0	0	13	19	1225	0	0	1160	13
Major/Minor N	Minor2		ľ	Minor1		N	Major1		N	/lajor2		
Conflicting Flow All	1811	2423	580			613	1173	0	0	1225	0	0
Stage 1	1160	1160	-	-	-	-	-	-	-	-	-	-
Stage 2	651	1263	_	_	_	_	_	_	_	_	_	_
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	49	32	458	0	0	435	591	-	-	565	-	-
Stage 1	208	268	-	0	0	-	-	-	-	-	-	-
Stage 2	424	239	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	46	31	458	-	-	435	591	-	-	565	-	-
Mov Cap-2 Maneuver	46	31	-	-	-	-	-	-	-	-	-	-
Stage 1	201	268	-	-	-	-	-	-	-	-	-	-
Stage 2	398	231	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	32.3			13.5			0.2			0		
HCM LOS	D			В								
Minor Lane/Major Mvm	nt	NBL	NBT	NRR I	EBLn1V	VBI n1	SBL	SBT	SBR			
Capacity (veh/h)		591	-	- NDICI	458	435	565	JD1 -	JDIN .			
HCM Lane V/C Ratio		0.032	-		0.742	0.03	505					
HCM Control Delay (s)		11.3	-	-	32.3	13.5	0	_	-			
HCM Lane LOS		11.3 B	-	-	52.5 D	13.3 B	A	-				
HCM 95th %tile Q(veh))	0.1	-	-	6.1	0.1	0	-	-			
HOW 75th 70the Q(Veh)		U. I			0.1	U. I	U					

Intersection						
Int Delay, s/veh	6.8					
		EDD	NIDI	NDT	CDT	CDD
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	7	75	17	વ	}	0
Traffic Vol, veh/h	0	75	17	11	10	0
Future Vol, veh/h	0	75	17	11	10	0
Conflicting Peds, #/hr	0	0	0	0	_ 0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	82	18	12	11	0
Major/Minor	Minor2		Major1	N	/lajor2	
Conflicting Flow All	59	11	11	0	-	0
Stage 1	11	-	-	-	_	-
Stage 2	48	_		_	_	_
Critical Hdwy	6.42	6.22	4.12	-	-	
Critical Hdwy Stg 1	5.42	0.22	4.12	-	-	-
Critical Hdwy Stg 2	5.42		-	-	-	-
Follow-up Hdwy	3.518	3.318	2.218	-	-	-
Pot Cap-1 Maneuver	948	1070	1608	-	-	-
	1012	1070	1000	-	-	-
Stage 1	974		-	-	-	-
Stage 2	9/4	-	-	-	-	-
Platoon blocked, %	020	1070	1/00	-	-	-
Mov Cap-1 Maneuver	938	1070	1608	-	-	-
Mov Cap-2 Maneuver	938	-	-	-	-	-
Stage 1	1001	-	-	-	-	-
Stage 2	974	-	-	-	-	-
Approach	EB		NB		SB	
HCM Control Delay, s	8.6		4.4		0	
HCM LOS	Α		т.т		U	
HOW EOS						
Minor Lane/Major Mvn	nt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)		1608	-	1070	-	-
HCM Lane V/C Ratio		0.011	-	0.076	-	-
HCM Control Delay (s)		7.3	0	8.6	-	-
HCM Lane LOS		Α	Α	Α	-	-
HCM 95th %tile Q(veh)	0	-	0.2	-	-

Intersection						
Int Delay, s/veh	5.6					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	^			4	¥	
Traffic Vol, veh/h	2	0	7	4	0	8
Future Vol, veh/h	2	0	7	4	0	8
Conflicting Peds, #/hr	0	0	0	0	0	0
· ·	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	2	0	8	4	0	9
Major/Minor Ma	ajor1	ı	Major2		Minor1	
						2
Conflicting Flow All	0	0	2	0	22	2
Stage 1	-	-	-	-	2	-
Stage 2	-	-	112	-	20	- ())
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	2 210	-	5.42	2 210
Follow-up Hdwy	-	-	2.218		3.518	
Pot Cap-1 Maneuver	-	-	1620	-	995	1082
Stage 1	-	-	-	-	1021	-
Stage 2	-	-	-	-	1003	-
Platoon blocked, %	-	-	1/00	-	000	1000
Mov Cap-1 Maneuver	-	-	1620	-	990	1082
Mov Cap-2 Maneuver	-	-	-	-	990	-
Stage 1	-	-	-	-	1021	-
Stage 2	-	-	-	-	998	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		4.6		8.4	
HCM LOS					Α	
NA'		JDI1	EDT	EDD	WDI	WDT
Minor Lane/Major Mvmt	ľ	VBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		1082	-		1620	-
HCM Lane V/C Ratio		0.008	-		0.005	-
HCM Control Delay (s)		8.4	-	-	7.2	0
11/:N/11 opo 1 ()C		Α	-	-	Α	Α
HCM Lane LOS HCM 95th %tile Q(veh)		0	-	_	0	-

Intersection													
Int Delay, s/veh	29.9												
J .		CET	CED	N IN A /I	NIVAZT	MMD	NIEL	NICT	NED	CMI	CMT	CMD	
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
Lane Configurations	0	41	224	0	41	471	0	- ♣	0	150	<u>ન</u>	104	
Fraffic Vol., veh/h	0	399 399	224	0	980	471	0	0	0	153	0	104 104	
Future Vol, veh/h Conflicting Peds, #/hr	0	399	224 0	0	980 0	471 0	0	0	0	153 0	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	1166	Free	-	-	Free	Stop -	Stop -	None	310p	Stop -	Yield	
Storage Length	_	_	480	_	_	900	_	_	-	_	_	0	
Veh in Median Storage		0	-	_	0	-	_	0	_	_	0	-	
Grade, %	-	0	_	_	0	_	_	0	_	_	0	_	
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Vivmt Flow	0	443	249	0	1043	501	0	0	0	178	0	121	
Major/Minor	Major1		N	Major2		ı	/linor1		N	/linor2			
Conflicting Flow All	1043	0	- I	443	0	0	965	1486	222	1265	1486	522	
Stage 1	1043	-	-	443	-	-	443	443	-	1043	1043	522	
Stage 2	_		_	_	_	_	522	1043	-	222	443	_	
Critical Hdwy	4.14	_	-	4.14	-	_	7.54	6.54	6.94	7.54	6.54	6.94	
ritical Hdwy Stg 1	-	_	_	-	_	_	6.54	5.54	-	6.54	5.54	-	
Critical Hdwy Stg 2	_	_	_	_	_	_	6.54	5.54	_	6.54	5.54	_	
Follow-up Hdwy	2.22	_	_	2.22	_	_	3.52	4.02	3.32	3.52	4.02	3.32	
Pot Cap-1 Maneuver	663	-	0	1113	-	0	209	123		~ 126	123	499	
Stage 1	-	-	0	-	-	0	564	574	-	245	305	-	
Stage 2	-	-	0	-	-	0	506	305	-	760	574	-	
Platoon blocked, %		-			-								
Mov Cap-1 Maneuver	663	-	-	1113	-	-	158	123	782	~ 126	123	499	
Nov Cap-2 Maneuver	-	-	-	-	-	-	158	123	-	~ 126	123	-	
Stage 1	-	-	-	-	-	-	564	574	-	245	305	-	
Stage 2	-	-	-	-	-	-	383	305	-	760	574	-	
Approach	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			178.4			
HCM LOS							Α			F			
Minor Lane/Major Mvm	nt N	VELn1	NWL	NWT	SEL	SETS	WLn1S	SWLn2					
Capacity (veh/h)			1113	-	663	-	126	499					
ICM Lane V/C Ratio		_	-	-	-	_	1.412						
ICM Control Delay (s)		0	0	-	0		289.8	14.5					
ICM Lane LOS		A	A	-	A	-	F	В					
HCM 95th %tile Q(veh)	-	0	-	0	-	12	0.9					
Votes													
: Volume exceeds ca	nacity	\$. Do	lay ove	eeds 3	nns	+: Com	nutation	Not D	ofinod	*· \ \	maiory	ıolumo i	n platoon
volunie exceeds ca	pacity	φ. D∈	iay exc	ccus 31	002	+. CUIII	pulaliul	ו ואטנ ט	enneu	. All	majui \	volume i	ii piatuuii

	>	→	-	•	←	*_	\	\mathbf{x}	4	•	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	*	†	77	ሻሻ	1>		7	↑ ↑		ሻ	^	
Traffic Volume (veh/h)	420	2	748	0	0	0	0	499	0	0	1216	0
Future Volume (veh/h)	420	2	748	0	0	0	0	499	0	0	1216	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	433	2	0	0	0	0	0	542	0	0	1366	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	729	559		394	559	0	197	1618	0	197	2324	0
Arrive On Green	0.30	0.30	0.00	0.00	0.00	0.00	0.00	0.46	0.00	0.00	0.46	0.00
Sat Flow, veh/h	1781	1870	2790	2745	1870	0	398	3647	0	864	5274	0
Grp Volume(v), veh/h	433	2	0	0	0	0	0	542	0	0	1366	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1373	1870	0	398	1777	0	864	1702	0
Q Serve(g_s), s	8.2	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	7.3	0.0
Cycle Q Clear(g_c), s	8.2	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.0	0.0	7.3	0.0
Prop In Lane	1.00	0.0	1.00	1.00	0.0	0.00	1.00	0.0	0.00	1.00	7.0	0.00
Lane Grp Cap(c), veh/h	729	559	1.00	394	559	0	197	1618	0	197	2324	0.00
V/C Ratio(X)	0.59	0.00		0.00	0.00	0.00	0.00	0.34	0.00	0.00	0.59	0.00
Avail Cap(c_a), veh/h	1073	920		924	920	0	266	2234	0	347	3210	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.9	9.0	0.0	0.0	0.0	0.0	0.0	6.4	0.0	0.0	7.4	0.0
Incr Delay (d2), s/veh	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	2.2	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	1.3	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0		0.0
LnGrp Delay(d),s/veh	12.7	9.0	0.0	0.0	0.0	0.0	0.0	6.5	0.0	0.0	7.7	0.0
LnGrp LOS	В	A	0.0	A	A	A	A	A	A	A	Α	A
Approach Vol, veh/h		435	А		0	- ,,	-,,	542		, , , 	1366	
Approach Delay, s/veh		12.6	7.		0.0			6.5			7.7	
Approach LOS		12.0 B			0.0			0.5 A			Α.	
		D						А			А	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		21.2		15.4		21.2		15.4				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+I1), s		9.3		10.2		5.6		0.0				
Green Ext Time (p_c), s		7.4		8.0		3.0		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			8.3									
HCM 6th LOS			Α									
Notes												

Intersection												
Int Delay, s/veh	0.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7		∱ }			^	7
Traffic Vol, veh/h	0	0	57	0	0	0	48	1180	0	0	1199	48
Future Vol, veh/h	0	0	57	0	0	0	48	1180	0	0	1199	48
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	.,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	58	58	58	92	92	92	92	92	92	97	97	97
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	98	0	0	0	52	1283	0	0	1236	49
Major/Minor N	Minor2		<u> </u>	Minor1		N	/lajor1		N	/lajor2		
Conflicting Flow All	1982	2623	618	-	-	642	1285	0	0	1283	0	0
Stage 1	1236	1236	-	-	-	-	-	-	-	-	-	-
Stage 2	746	1387	-	-	-	-	-	-	-	-	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	36	24	432	0	0	417	536	-	-	537	-	-
Stage 1	187	246	-	0	0	-	-	-	-	-	-	-
Stage 2	372	208	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver	33	22	432	-	-	417	536	-	-	537	-	-
Mov Cap-2 Maneuver	33	22	-	-	-	-	-	-	-	-	-	-
Stage 1	169	246	-	-	-	-	-	-	-	-	-	-
Stage 2	336	188	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	15.8			0			0.5			0		
HCM LOS	С			A								
Minor Lane/Major Mvm	ıt	NBL	NBT	NBR E	EBLn1V	VBLn1	SBL	SBT	SBR			
Capacity (veh/h)		536	-	-	432	-	537	-	-			
HCM Lane V/C Ratio		0.097	-	-	0.227	-	-	-	-			
HCM Control Delay (s)		12.4	-	-	15.8	0	0	-	-			
HCM Lane LOS		В	-	-	С	A	A	-	-			
HCM 95th %tile Q(veh)		0.3	-	-	0.9	-	0	-	-			
							_					

Intersection						
Int Delay, s/veh	6.7					
		EDD	NIDI	NDT	CDT	CDD
Movement Lang Configurations	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	7	40	0.4	<u>र्</u> च	4	٥
Traffic Vol, veh/h	0	48	84	12	9	0
Future Vol, veh/h	0	48	84	12	9	0
Conflicting Peds, #/hr	0	0	0	0	0	_ 0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	52	91	13	10	0
Major/Minor	Minor2	- 1	Major1	N	/lajor2	
Conflicting Flow All	205	10	10	0	- najoiz	0
Stage 1	10				-	-
Stage 2	195	-	-	-		-
			112	-		-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518			-	-	-
Pot Cap-1 Maneuver	783	1071	1610	-	-	-
Stage 1	1013	-	-	-	-	-
Stage 2	838	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	738	1071	1610	-	-	-
Mov Cap-2 Maneuver	738	-	-	-	-	-
Stage 1	955	-	-	-	-	-
Stage 2	838	-	-	-	-	-
Annroach	ED		ND		CD	
Approach	EB		NB		SB	
HCM Control Delay, s	8.5		6.4		0	
HCM LOS	Α					
Minor Lane/Major Mvn	nt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)		1610		1071		
HCM Lane V/C Ratio		0.057		0.049	_	_
HCM Control Delay (s)	1	7.4	0	8.5	_	_
HCM Lane LOS		Α.4	A	Α	_	_
HCM 95th %tile Q(veh)	0.2	- A	0.2	-	-
HOW FOUT MITTE Q(VEH)	0.2		0.2	-	-

Intersection						
Int Delay, s/veh	5.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	1	LUIN	1100	4	¥	HOR
Traffic Vol., veh/h	4	0	10	2	0	5
Future Vol, veh/h	4	0	10	2	0	5
Conflicting Peds, #/hr	0	0	0	0	0	0
•	Free	Free	Free	Free	Stop	Stop
RT Channelized	_	None	_	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	# 0	-	_	0	0	-
Grade, %	0	-	-	0	0	_
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	0	11	2	0	5
N.A.;/N.A;	-!1		1-:		\	
	ajor1		Major2		Minor1	
Conflicting Flow All	0	0	4	0	28	4
Stage 1	-	-	-	-	4	-
Stage 2	-	-	-	-	24	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	
Pot Cap-1 Maneuver	-	-	1618	-	987	1080
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	999	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1618	-	980	1080
Mov Cap-2 Maneuver	-	-	-	-	980	-
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	992	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		6		8.4	
HCM LOS	U		U		Α	
HOW EOS						
Minor Lane/Major Mvmt	N	VBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		1080	-		1618	-
		0.005	-	-	0.007	-
HCM Lane V/C Ratio						
HCM Control Delay (s)		8.4	-	-	7.2	0
			-	-	7.2 A 0	0 A

Intersection													
Int Delay, s/veh	25.1												
		CET	CED	N IN A /I	NINAIT	MMD	NIEL	NICT	NED	CMI	CMT	CMD	
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR	
Lane Configurations	٥	4↑	7	0	407	7	0	- ♣	0	100	4	7	
Fraffic Vol, veh/h uture Vol, veh/h	0	667 667	544 544	0	497 497	653 653	0	0	0	192 192	0	83 83	
Conflicting Peds, #/hr	0	007	0	0	497	003	0	0	0	192	0	0	
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	riee	Free	-	-	Free	310p -	Slup -	None	310p -	Stop -	Yield	
Storage Length	_		480	_	-	900	_	_	NOTIC -	_	_	0	
/eh in Median Storage		0	-	_	0	-	_	0	_	_	0	-	
Grade, %	-	0	_	_	0	_	_	0	_	_	0	_	
Peak Hour Factor	88	88	88	87	87	87	92	92	92	76	76	76	
leavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
/lvmt Flow	0	758	618	0	571	751	0	0	0	253	0	109	
Major/Minor I	Maior1		N	Major?		ı	/linor1		N	/linor2			
Conflicting Flow All	<u>Major1</u> 571	0	ľ	Major2 758	0	0	1044	1329	379	950	1329	286	
Stage 1	5/1	-	-	730	-	-	758	758	3/9	571	571	200	
Stage 2	_	_	_	_	_	_	286	571	_	379	758	_	
ritical Hdwy	4.14	_	_	4.14	-	_	7.54	6.54	6.94	7.54	6.54	6.94	
ritical Hdwy Stg 1	-	_	_	-	_	_	6.54	5.54	-	6.54	5.54	-	
ritical Hdwy Stg 2	_	_	_	_	_	_	6.54	5.54	_	6.54	5.54	_	
follow-up Hdwy	2.22	_	_	2.22		_	3.52	4.02	3.32	3.52	4.02	3.32	
Pot Cap-1 Maneuver	998	-	0	849	-	0	183	154		~ 215	154	711	
Stage 1	-	-	0	-	-	0	365	413	-	473	503	-	
Stage 2	-	-	0	-	-	0	697	503	-	615	413	-	
Platoon blocked, %		-			-								
Mov Cap-1 Maneuver	998	-	-	849	-	-	155	154		~ 215	154	711	
Nov Cap-2 Maneuver	-	-	-	-	-	-	155	154	-	~ 215	154	-	
Stage 1	-	-	-	-	-	-	365	413	-	473	503	-	
Stage 2	-	-	-	-	-	-	590	503	-	615	413	-	
pproach	SE			NW			NE			SW			
HCM Control Delay, s	0			0			0			117.2			
ICM LOS							Α			F			
/linor Lane/Major Mvm	nt N	VELn1	NWL	NWT	SEL	SETS	WLn1S	WLn2					
Capacity (veh/h)		-	849	-	998		215	711					
CM Lane V/C Ratio		-	-	-	-	-	1.175						
ICM Control Delay (s)		0	0	-	0		163.1	11					
ICM Lane LOS		Α	Α	-	Α	-	F	В					
HCM 95th %tile Q(veh))	-	0	-	0	-	12.4	0.5					
Votes													
: Volume exceeds cap	nacity	\$· Do	lav evo	eeds 3	00s	+: Com	nutation	Not D	efined	*· ∆II	maiory	ınluma i	in platoon
olullic exceeds ca	vacity	ψ. De	iay til	ccus s	003	T. CUIII	palaliul	ו ואטנ טי	cillicu	. All	major \	Joiume I	iii piatuuii

	>	→	-	4	←	*_	\	×	4	1	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	ሻ	†	77	14.54	₽		ሻ	∱ }		ሻ	ተተተ	
Traffic Volume (veh/h)	210	1	397	0	0	0	0	775	0	0	1148	0
Future Volume (veh/h)	210	1	397	0	0	0	0	775	0	0	1148	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	269	1	0	0	0	0	0	842	0	0	1383	0
Peak Hour Factor	0.78	0.78	0.78	0.92	0.92	0.92	0.92	0.92	0.92	0.83	0.83	0.83
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	593	378		466	378	0	233	1801	0	233	2587	0
Arrive On Green	0.20	0.20	0.00	0.00	0.00	0.00	0.00	0.51	0.00	0.00	0.51	0.00
Sat Flow, veh/h	1781	1870	2790	2748	1870	0	392	3647	0	653	5274	0
Grp Volume(v), veh/h	269	1	0	0	0	0	0	842	0	0	1383	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1374	1870	0	392	1777	0	653	1702	0
Q Serve(g_s), s	4.4	0.0	0.0	0.0	0.0	0.0	0.0	4.7	0.0	0.0	5.7	0.0
Cycle Q Clear(q_c), s	4.4	0.0	0.0	0.0	0.0	0.0	0.0	4.7	0.0	0.0	5.7	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	593	378		466	378	0	233	1801	0	233	2587	0
V/C Ratio(X)	0.45	0.00		0.00	0.00	0.00	0.00	0.47	0.00	0.00	0.53	0.00
Avail Cap(c_a), veh/h	1270	1089		1509	1089	0	326	2643	0	388	3798	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.6	9.8	0.0	0.0	0.0	0.0	0.0	4.9	0.0	0.0	5.2	0.0
Incr Delay (d2), s/veh	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.5	0.0
Unsig. Movement Delay, s/veh	1											
LnGrp Delay(d),s/veh	12.1	9.8	0.0	0.0	0.0	0.0	0.0	5.1	0.0	0.0	5.3	0.0
LnGrp LOS	В	Α		Α	Α	Α	Α	Α	Α	Α	Α	Α
Approach Vol, veh/h		270	Α		0			842			1383	
Approach Delay, s/veh		12.1			0.0			5.1			5.3	
Approach LOS		В						Α			Α	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		20.2		10.8		20.2		10.8				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (q_c+l1), s		7.7		6.4		6.7		0.0				
Green Ext Time (p_c), s		8.0		0.5		4.9		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			6.0									
HCM 6th LOS			Α									
Notes												

Intersection												
Int Delay, s/veh	4.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4				7		∱ ∱		ነ	^	7
Traffic Vol, veh/h	0	0	85	0	0	0	16	1145	0	0	1152	12
Future Vol, veh/h	0	0	85	0	0	0	16	1145	0	0	1152	12
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	25	25	25	92	92	92	85	85	85	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	340	0	0	0	19	1347	0	0	1280	13
Major/Minor	Minor2			Minor1			/lajor1		,	/lajor2		
		2475						0			0	0
Conflicting Flow All	1992	2665	640	-	-	674	1293	0		1347	0	0
Stage 1	1280	1280	-	-	-	-	-	-	-	-	-	-
Stage 2	712	1385	- / 04	-	-	- / 04	-	-	-	111	-	-
Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Follow-up Hdwy	3.52	4.02	3.32	-	-	3.32	2.22	-	-	2.22	-	-
Pot Cap-1 Maneuver	36	22	418	0	0	397	532	-	-	507	-	-
Stage 1	175	235	-	0	0	-	-	-	-	-	-	-
Stage 2	389	209	-	0	0	-	-	-	-	-	-	-
Platoon blocked, %								-	-		-	-
Mov Cap-1 Maneuver		21	418	-	-	397	532	-	-	507	-	-
Mov Cap-2 Maneuver	35	21	-	-	-	-	-	-	-	-	-	-
Stage 1	169	235	-	-	-	-	-	-	-	-	-	-
Stage 2	375	201	-	-	-	-	-	-	-	-	-	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	41.7			0			0.2			0		
HCM LOS	E			A								
	_			,,								
Minor Lane/Major Mvn	nt	NDI	NDT	NDD	DI 51V	VDI 51	CDI	CDT	CDD			
	iit	NBL	NBT	NDK	EBLn1V	VDLIII	SBL	SBT	SBR			
Capacity (veh/h)		532	-	-	418	-	507	-	-			
HCM Lane V/C Ratio	,	0.035	-	-	0.813	-	-	-	-			
HCM Control Delay (s))	12	-	-	41.7	0	0	-	-			
HCM Lane LOS	,	В	-	-	E	Α	A	-	-			
HCM 95th %tile Q(veh	1)	0.1	-	-	7.4	-	0	-	-			

Int Delay, s/veh 6.8
Movement
Lane Configurations Y ↓
Traffic Vol, veh/h 0 75 17 11 10 0 Future Vol, veh/h 0 75 17 11 10 0 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 - - 0 0 - Veh in Median Storage, # 0 - - 0 0 - Grade, % 0 - - 0 0 - Grade, % 0 - - 0 0 - Heavy Vehicles, % 2
Future Vol, veh/h Conflicting Peds, #/hr O Conflicting Free Conflicting Flow All Stage 2 Conflicting Flow All Conflicting Flow All Stage 2 Conflicting Flow All Stage 2 Conflicting Flow All Solution Stage 1 Conflicting Flow All Solution Stage 2 Conflicting Flow Stage 3 Conflicting Flow Stage 5 Conflicting Flow
Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 - - 0 0 - Veh in Median Storage, # 0 - - 0 0 - Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 92 Heavy Vehicles, % 2
Sign Control Stop Stop Free Free Free Free Free Free Free Free Ree Ree Ree Ree Ree Free Free Free Free Ree Ree Ree None None <th< td=""></th<>
RT Channelized - None - None - None Storage Length 0
Storage Length 0 -
Veh in Median Storage, # 0 - - 0 0 - Grade, % 0 - - 0 0 - Peak Hour Factor 92 92 92 92 92 92 Heavy Vehicles, % 2 <td< td=""></td<>
Grade, % 0 - - 0 0 - Peak Hour Factor 92
Peak Hour Factor 92 2 2 2 Conflicting Flow All 59 11 11 0 - 0 0 Stage 2 48 - - - - - - - -<
Major/Minor Minor2 Major1 Major2 Conflicting Flow All 59 11 11 0 Stage 1 11 - - - - Stage 2 48 - - - - - Critical Hdwy 6.42 6.22 4.12 - - - - Critical Hdwy Stg 1 5.42 - - - - - - Critical Hdwy Stg 2 5.42 - <td< td=""></td<>
Moment Flow 0 82 18 12 11 0 Major/Minor Minor2 Major1 Major2 Conflicting Flow All 59 11 11 0 - 0 Stage 1 11 - - - - - - Stage 2 48 - - - - - - Critical Hdwy 6.42 6.22 4.12 - - - - Critical Hdwy Stg 1 5.42 - - - - - - Critical Hdwy Stg 2 5.42 - - - - - - Follow-up Hdwy 3.518 3.318 2.218 - - - Pot Cap-1 Maneuver 948 1070 1608 - - - Stage 1 1012 - - - - - Stage 2 974 - - - -
Major/Minor Minor2 Major1 Major2 Conflicting Flow All 59 11 11 0 0 Stage 1 11 - - - - Stage 2 48 - - - - Critical Hdwy 6.42 6.22 4.12 - - - Critical Hdwy Stg 1 5.42 - - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 2.218 - - - Pot Cap-1 Maneuver 948 1070 1608 - - - Stage 1 1012 - - - - - Stage 2 974 - - - - - Platoon blocked, % - - - - - -
Conflicting Flow All 59 11 11 0 - 0 Stage 1 11
Conflicting Flow All 59 11 11 0 - 0 Stage 1 11
Conflicting Flow All 59 11 11 0 - 0 Stage 1 11
Stage 1 11 - - - - Stage 2 48 - - - - Critical Hdwy 6.42 6.22 4.12 - - - Critical Hdwy Stg 1 5.42 - - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 2.218 - - - Pot Cap-1 Maneuver 948 1070 1608 - - - Stage 1 1012 - - - - - Stage 2 974 - - - - - Platoon blocked, % - - - - - -
Stage 2 48 - - - - Critical Hdwy 6.42 6.22 4.12 - - - Critical Hdwy Stg 1 5.42 - - - - - Critical Hdwy Stg 2 5.42 - - - - - Follow-up Hdwy 3.518 3.318 2.218 - - - Pot Cap-1 Maneuver 948 1070 1608 - - - Stage 1 1012 - - - - - Stage 2 974 - - - - - Platoon blocked, % - - - - - -
Critical Hdwy Stg 1 5.42
Critical Hdwy Stg 1 5.42
Critical Hdwy Stg 2 5.42
Follow-up Hdwy 3.518 3.318 2.218
Pot Cap-1 Maneuver 948 1070 1608 Stage 1 1012
Stage 1 1012 - - - - Stage 2 974 - - - - Platoon blocked, % - - - -
Stage 2 974 Platoon blocked, %
Platoon blocked, %
Mov Cap-1 Maneuver 938 1070 1608
Mov Cap-1 Maneuver 938
•
Stage 2 974
Approach EB NB SB
HCM Control Delay, s 8.6 4.4 0
HCM LOS A
Minor Long/Major Muset NDI NDT FDI p1 CDT CDD
Minor Lane/Major Mvmt NBL NBT EBLn1 SBT SBR
Capacity (veh/h) 1608 - 1070
HCM Lane V/C Ratio 0.011 - 0.076
HCM Control Delay (s) 7.3 0 8.6
HCM Lane LOS A A A
HCM 95th %tile Q(veh) 0 - 0.2

Intersection						
Int Delay, s/veh	5.6					
		===	14.5	14/5-		NES
	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	Þ			4	Y	
Traffic Vol, veh/h	2	0	7	4	0	8
Future Vol, veh/h	2	0	7	4	0	8
Conflicting Peds, #/hr	0	0	0	0	0	0
	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	2	0	8	4	0	9
Maiau/Minau	.!4		A-lano		A!	
	ajor1		Major2		Minor1	
Conflicting Flow All	0	0	2	0	22	2
Stage 1	-	-	-	-	2	-
Stage 2	-	-	-	-	20	-
Critical Hdwy	-	-	4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	-	-	2.218	-	3.518	
Pot Cap-1 Maneuver	-	-	1620	-	995	1082
Stage 1	-	-	-	-	1021	-
Stage 2	-	-	-	-	1003	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1620	-	990	1082
Mov Cap-2 Maneuver	-	-	-	-	990	-
Stage 1	-	-	-	-	1021	-
Stage 2	_		_	_	998	
Jugo L					.,,	
Approach	EB		WB		NB	
HCM Control Delay, s	0		4.6		8.4	
HCM LOS					Α	
Minor Lane/Major Mvmt	N	NBLn1	EBT	EBR	WBL	WBT
	ı		LDI	LDIX		WDT
Capacity (veh/h)		1082	-	-	1620	-
HCM Control Doloy (c)		0.008	-		0.005	-
HCM Control Delay (s)		8.4	-	-	7.2	0
HCM Lane LOS		Α	-	-	Α	Α
HCM 95th %tile Q(veh)		0	_		0	-

Intersection												
Int Delay, s/veh	17											
Movement	SEL	SET	SER	NWL	NWT	NWR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4₽	7		41₽	7		4			र्स	7
Traffic Vol, veh/h	0	363	211	0	916	440	0	0	0	139	0	98
Future Vol, veh/h	0	363	211	0	916	440	0	0	0	139	0	98
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	Free	-	-	None	-	-	Yield
Storage Length	-	-	480	-	-	900	-	-	-	-	-	0
Veh in Median Storage	e,# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	94	94	94	92	92	92	86	86	86
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	403	234	0	974	468	0	0	0	162	0	114
Major/Minor	Major1		1	Major2		N	/linor1		ľ	Minor2		
Conflicting Flow All	974	0	-	403	0	0	890	1377	202	1176	1377	487
Stage 1	-	-	-		-	_	403	403		974	974	-
Stage 2	-		-	-	-	-	487	974		202	403	-
Critical Hdwy	4.14	-	-	4.14	-	-	7.54	6.54	6.94	7.54	6.54	6.94
Critical Hdwy Stg 1	-	-	_	-	-	-	6.54	5.54	-	6.54	5.54	-
Critical Hdwy Stg 2	-	-	_	_	_	-	6.54	5.54	_	6.54	5.54	-
Follow-up Hdwy	2.22	-	_	2.22	-	-	3.52	4.02	3.32	3.52	4.02	3.32
Pot Cap-1 Maneuver	704	-	0	1152	_	0	237	144		~ 147	144	526
Stage 1	-	-	0	-	-	0	595	598	-	270	328	-
Stage 2	-	-	0	-	-	0	531	328	-	781	598	-
Platoon blocked, %		-			-							
Mov Cap-1 Maneuver	704	-	-	1152	-	-	186	144	805	~ 147	144	526
Mov Cap-2 Maneuver	-	-	-	-	-	-	186	144	-	~ 147	144	-
Stage 1	-	-	-	-	-	-	595	598	-	270	328	-
Stage 2	-	-	-	-	-	-	416	328	-	781	598	-
Approach	SE			NW			NE			SW		
HCM Control Delay, s	0			0			0			102		
HCM LOS	- 0						A			F		
TOW LOO							, ,			•		
Minor Lane/Major Mvm	nt I	NELn1	NWL	NWT	SEL	SFTS	WLn1S	WI n2				
Capacity (veh/h)	π 1	*LLIII	1152	14001	704	JLIJ	147	526				
HCM Lane V/C Ratio		-		-	704	-		0.217				
HCM Control Delay (s)		0	0	-	0	-	164.2	13.7				
HCM Lane LOS		A	A	-	A	-	104.2 F	13.7 B				
HCM 95th %tile Q(veh)	A -	0	-	0	-	8.8	0.8				
)		U		U		0.0	0.0				
Notes												
~: Volume exceeds ca	pacity	\$: D€	elay exc	eeds 3	00s	+: Com	putation	Not D	efined	*: All	major	volume

	>	→	74	•	←	*_	\	×	4	*	×	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	SEL	SET	SER	NWL	NWT	NWR
Lane Configurations	7	↑	77	ሻሻ	₽		7	ተ ኈ		ሻ	^	
Traffic Volume (veh/h)	395	2	678	0	0	0	0	452	0	0	1121	0
Future Volume (veh/h)	395	2	678	0	0	0	0	452	0	0	1121	0
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Work Zone On Approach		No			No			No			No	
Adj Sat Flow, veh/h/ln	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	1870	0
Adj Flow Rate, veh/h	407	2	0	0	0	0	0	491	0	0	1260	0
Peak Hour Factor	0.97	0.97	0.97	0.92	0.92	0.92	0.92	0.92	0.92	0.89	0.89	0.89
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	0
Cap, veh/h	723	538		422	538	0	211	1594	0	211	2290	0
Arrive On Green	0.29	0.29	0.00	0.00	0.00	0.00	0.00	0.45	0.00	0.00	0.45	0.00
Sat Flow, veh/h	1781	1870	2790	2745	1870	0	440	3647	0	906	5274	0
Grp Volume(v), veh/h	407	2	0	0	0	0	0	491	0	0	1260	0
Grp Sat Flow(s), veh/h/ln	1781	1870	1395	1373	1870	0	440	1777	0	906	1702	0
Q Serve(g_s), s	7.2	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	6.2	0.0
Cycle Q Clear(g_c), s	7.2	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	6.2	0.0
Prop In Lane	1.00		1.00	1.00		0.00	1.00		0.00	1.00		0.00
Lane Grp Cap(c), veh/h	723	538		422	538	0	211	1594	0	211	2290	0
V/C Ratio(X)	0.56	0.00		0.00	0.00	0.00	0.00	0.31	0.00	0.00	0.55	0.00
Avail Cap(c_a), veh/h	1151	987		1082	987	0	311	2397	0	416	3444	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	11.2	8.7	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	6.9	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.2	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	1.8	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.0	0.0
Unsig. Movement Delay, s/veh		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	0.0
LnGrp Delay(d),s/veh	11.9	8.7	0.0	0.0	0.0	0.0	0.0	6.1	0.0	0.0	7.1	0.0
LnGrp LOS	В	Α	0.0	A	A	A	A	A	Α	Α	Α	Α
Approach Vol, veh/h		409	А		0			491			1260	
Approach Delay, s/veh		11.9	٨		0.0			6.1			7.1	
Approach LOS		11.9 B			0.0			Α			7.1 A	
Approach LOS		D						А			А	
Timer - Assigned Phs		2		4		6		8				
Phs Duration (G+Y+Rc), s		19.8		14.3		19.8		14.3				
Change Period (Y+Rc), s		4.5		4.5		4.5		4.5				
Max Green Setting (Gmax), s		23.0		18.0		23.0		18.0				
Max Q Clear Time (g_c+l1), s		8.2		9.2		5.0		0.0				
Green Ext Time (p_c), s		7.1		0.8		2.7		0.0				
Intersection Summary												
HCM 6th Ctrl Delay			7.8									
HCM 6th LOS			A									
Notes												

Int Delay, S/veh	Intersection												
Traffic Vol, veh/h		0.9											
Traffic Vol, veh/h	Movement	EBI	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Traffic Vol, veh/h													
Future Vol, veh/h		0		57	0	0				0			
Conflicting Peds, #/hr													
Sign Control Stop Stop Stop Stop Stop Stop Stop Stop Tree Free Free Free Free Free Tree RT Channelized - - None - None None - None None Storage Length - - - None - None Non	· · · · · · · · · · · · · · · · · · ·	0	0										
RT Channelized		Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
Veh in Median Storage, # - 0		-	-		•	•	None	-	-	None	-	-	None
Grade, % - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 9 97 90 Major/Licing Flow All 204 261<	Storage Length	-	-	-	-	-	0	80	-	-	200	-	0
Peak Hour Factor	Veh in Median Storage	2,# -	0	-	-	0	-	-	0	-	-	0	-
Heavy Vehicles, % 2 2 2 2 2 2 2 2 2	Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Mymit Flow 0 0 98 0 0 0 70 1255 0 0 1236 33 Major/Minor Minor2 Minor1 Major1 Major2 Major2 Conflicting Flow All 2004 2631 618 - - 628 1269 0 0 1255 0 0 Stage 1 1236 1236 - <td>Peak Hour Factor</td> <td>58</td> <td>58</td> <td>58</td> <td>92</td> <td>92</td> <td>92</td> <td>92</td> <td>92</td> <td>92</td> <td>97</td> <td>97</td> <td>97</td>	Peak Hour Factor	58	58	58	92	92	92	92	92	92	97	97	97
Major/Minor Minor2 Minor1 Major1 Major2 Conflicting Flow All 2004 2631 618 628 1269 0 0 1255 0 0 Stage 1 1236 1236	Heavy Vehicles, %	2	2	2	2	2	2	2		2	2		
Conflicting Flow All 2004 2631 618 - - 628 1269 0 0 1255 0 0 Stage 1 1236 1236 - - - - - - - - -	Mvmt Flow	0	0	98	0	0	0	70	1255	0	0	1236	33
Conflicting Flow All 2004 2631 618 - - 628 1269 0 0 1255 0 0 Stage 1 1236 1236 - - - - - - - - -													
Conflicting Flow All 2004 2631 618 -	Major/Minor I	Minor2		ľ	Minor1		N	/lajor1		N	/lajor2		
Stage 1 1236	Conflicting Flow All	2004	2631	618	-	-	628	1269	0	0	1255	0	0
Critical Hdwy 7.54 6.54 6.94 - - 6.94 4.14 - 4.14 - 4.14 -		1236	1236	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 1 6.54 5.54 -<		768	1395	-	-	-	-	-	-	-	-	-	-
Critical Hdwy Stg 2 6.54 5.54 -	Critical Hdwy	7.54	6.54	6.94	-	-	6.94	4.14	-	-	4.14	-	-
Follow-up Hdwy 3.52 4.02 3.32 3.32 2.22 2.22 2.7 Pot Cap-1 Maneuver 35 23 432 0 0 426 543 550 Stage 1 187 246 - 0 0	Critical Hdwy Stg 1	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Pot Cap-1 Maneuver 35 23 432 0 0 426 543 - - 550 - - Stage 1	Critical Hdwy Stg 2	6.54	5.54	-	-	-	-	-	-	-	-	-	-
Stage 1					-	-			-	-		-	-
Stage 2 360 207 - 0 0	Pot Cap-1 Maneuver			432	0	0	426	543	-	-	550	-	-
Platoon blocked, %				-	0	0	-	-	-	-	-	-	-
Mov Cap-1 Maneuver 32 20 432 - 426 543 - 550 - - Mov Cap-2 Maneuver 32 20 -		360	207	-	0	0	-	-	-	-	-	-	-
Mov Cap-2 Maneuver 32 20 -									-	-		-	-
Stage 1 163 246 - <th< td=""><td></td><td></td><td></td><td>432</td><td>-</td><td>-</td><td>426</td><td>543</td><td>-</td><td>-</td><td>550</td><td>-</td><td>-</td></th<>				432	-	-	426	543	-	-	550	-	-
Stage 2 314 180 - <th< td=""><td>•</td><td></td><td></td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td></th<>	•			-	-	-	-	-	-	-	-	-	-
Approach EB WB NB SB HCM Control Delay, s 15.8 0 0.7 0 HCM LOS C A Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 543 - - 432 - 550 - - HCM Lane V/C Ratio 0.128 - - 0.227 - - - HCM Control Delay (s) 12.6 - - 15.8 0 0 - - HCM Lane LOS B - C A A - -	· ·			-	-	-	-	-	-	-	-	-	-
HCM Control Delay, s 15.8	Stage 2	314	180	-	-	-	-	-	-	-	-	-	-
HCM Control Delay, s 15.8													
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 543 - - 432 - 550 - - HCM Lane V/C Ratio 0.128 - - 0.227 - - - HCM Control Delay (s) 12.6 - - 15.8 0 0 - - HCM Lane LOS B - C A A - -	Approach	EB			WB			NB			SB		
Minor Lane/Major Mvmt NBL NBT NBR EBLn1WBLn1 SBL SBT SBR Capacity (veh/h) 543 - - 432 - 550 - - HCM Lane V/C Ratio 0.128 - - 0.227 - - - - HCM Control Delay (s) 12.6 - - 15.8 0 0 - - HCM Lane LOS B - C A A - -	HCM Control Delay, s	15.8			0			0.7			0		
Capacity (veh/h) 543 432 - 550 HCM Lane V/C Ratio 0.128 0.227 HCM Control Delay (s) 12.6 15.8 0 0 HCM Lane LOS B - C A A		С			Α								
Capacity (veh/h) 543 432 - 550 HCM Lane V/C Ratio 0.128 0.227 HCM Control Delay (s) 12.6 - 15.8 0 0 HCM Lane LOS B - C A A													
HCM Lane V/C Ratio 0.128 - - 0.227 - - - HCM Control Delay (s) 12.6 - - 15.8 0 0 - - HCM Lane LOS B - C A A - -	Minor Lane/Major Mvm	nt _	NBL	NBT	NBR I	EBL _{n1} V	VBL _{n1}	SBL	SBT	SBR			
HCM Lane V/C Ratio 0.128 - - 0.227 - - - - HCM Control Delay (s) 12.6 - - 15.8 0 0 - - HCM Lane LOS B - C A A - -	Capacity (veh/h)		543	-	-	432	-	550	-	-			
HCM Lane LOS B C A A			0.128	-	-	0.227	-		-	-			
HCM Lane LOS B C A A	HCM Control Delay (s)		12.6	-	-	15.8	0	0	-	-			
HCM 95th %tile Q(veh) 0.4 0.9 - 0			В	-	-	С	Α	Α	-	-			
	HCM 95th %tile Q(veh))	0.4	-	-	0.9	-	0	-	-			

Intersection						
Int Delay, s/veh	6.7					
		EDD	NIDI	NDT	CDT	CDD
Movement Lang Configurations	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	7	40	0.4	<u>र्</u> च	4	٥
Traffic Vol, veh/h	0	48	84	12	9	0
Future Vol, veh/h	0	48	84	12	9	0
Conflicting Peds, #/hr	0	0	0	0	0	_ 0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-		-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	52	91	13	10	0
Major/Minor	Minor2	-	Major1	N	/lajor2	
Conflicting Flow All	205	10	10	0	- najoiz	0
Stage 1	10				-	-
Stage 2	195	-	-	-		-
			112	-		-
Critical Hdwy	6.42	6.22	4.12	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518			-	-	-
Pot Cap-1 Maneuver	783	1071	1610	-	-	-
Stage 1	1013	-	-	-	-	-
Stage 2	838	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	738	1071	1610	-	-	-
Mov Cap-2 Maneuver	738	-	-	-	-	-
Stage 1	955	-	-	-	-	-
Stage 2	838	-	-	-	-	-
Annroach	ED		ND		CD	
Approach	EB		NB		SB	
HCM Control Delay, s	8.5		6.4		0	
HCM LOS	Α					
Minor Lane/Major Mvn	nt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)		1610		1071		
HCM Lane V/C Ratio		0.057		0.049	_	_
HCM Control Delay (s)	1	7.4	0	8.5	_	_
HCM Lane LOS		Α.4	A	Α	_	_
HCM 95th %tile Q(veh)	0.2	- A	0.2	-	-
HOW FOUT MITTE Q(VEH)	0.2		0.2	-	-

Intersection						
Int Delay, s/veh	5.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
		EBR	WDL			INDK
Lane Configurations	-	٥	10	<u>ન</u>	¥	Е
Traffic Vol, veh/h	4	0	10	2	0	5
Future Vol, veh/h	4	0	10	2	0	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,		-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	92	92	92	92	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	0	11	2	0	5
Major/Minor N	lajor1	N	Major2		Minor1	
Conflicting Flow All	0	0	4	0	28	4
Stage 1	-	-	-	-	4	-
Stage 2	_	_	_	_	24	_
Critical Hdwy	-		4.12	-	6.42	6.22
Critical Hdwy Stg 1	-	_	4.12	_	5.42	0.22
Critical Hdwy Stg 2	-	-	_	_	5.42	-
		-	2 210			3.318
Follow-up Hdwy	-	-	2.218	-		
Pot Cap-1 Maneuver	-	-	1618	-	987	1080
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	999	-
Platoon blocked, %	-	-		-		
Mov Cap-1 Maneuver	-	-	1618	-	980	1080
Mov Cap-2 Maneuver	-	-	-	-	980	-
Stage 1	-	-	-	-	1019	-
Stage 2	-	-	-	-	992	-
Approach	EB		WB		NB	
HCM Control Delay, s	0		6		8.4	
HCM LOS	U		U		0.4 A	
TIGIVI EUS					А	
Minor Lane/Major Mvmt	<u> </u>	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)		1080	-	-	1618	-
HCM Lane V/C Ratio		0.005	-		0.007	-
HCM Control Delay (s)		8.4	-	-	7.2	0
HCM Lane LOS		Α	-	-	Α	A
HCM 95th %tile Q(veh)		0	-	-	0	-

APPENDIX G TRAFFIC COUNT DATA



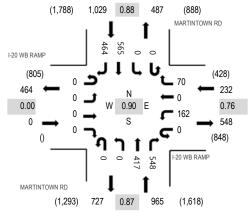


Location: 1 MARTINTOWN RD & I-20 WB RAMP AM

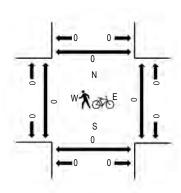
Date: Tuesday, March 22, 2022 **Peak Hour:** 07:15 AM - 08:15 AM

Peak 15-Minutes: 07:30 AM - 07:45 AM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

Interval	I-	20 WB Eastb	RAMF ound)	1-3	20 WB Westb			MA	RTINT(Northb		D		RTINT South	OWN Foound	RD		Rollina	Ped	lestriar	n Crossi	ings
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
7:00 AM	0	0	0	0	0	27	0	7	0	0	70	64	0	0	120	80	368	2,078	0	0	0	0
7:15 AM	0	0	0	0	0	39	0	14	0	0	85	114	0	0	147	116	515	2,226	0	0	0	0
7:30 AM	0	0	0	0	0	30	0	18	0	0	114	163	0	0	147	145	617	2,203	0	0	0	0
7:45 AM	0	0	0	0	0	52	0	24	0	0	105	141	0	0	138	118	578	1,978	0	0	0	0
8:00 AM	0	0	0	0	0	41	0	14	0	0	113	130	0	0	133	85	516	1,756	0	0	0	0
8:15 AM	0	0	0	0	0	68	1	21	0	0	125	62	0	0	122	93	492		0	0	0	0
8:30 AM	0	0	0	0	0	36	3	14	0	0	89	94	0	0	80	76	392		0	0	0	0
8:45 AM	0	0	0	0	0	13	0	6	0	0	69	80	0	0	100	88	356		0	0	0	0

		East	bound			West	oound			Northb	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	2	0	1	0	0	2	3	0	0	8	1	17
Lights	0	0	0	0	0	160	0	68	0	0	413	545	0	0	555	460	2,201
Mediums	0	0	0	0	0	0	0	1	0	0	2	0	0	0	2	3	8
Total	0	0	0	0	0	162	0	70	0	0	417	548	0	0	565	464	2,226

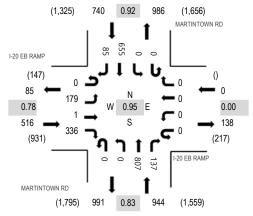


Location: 2 MARTINTOWN RD & I-20 EB RAMP AM

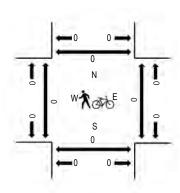
Date: Tuesday, March 22, 2022 **Peak Hour:** 07:15 AM - 08:15 AM

Peak 15-Minutes: 07:45 AM - 08:00 AM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	Į.	-20 EB	RAMP	1	1-2	20 EB I	RAMP		MA	RTINT	NWC	RD	MA	RTINT	OWN F	RD						
Interval		Eastb	ound			Westb	ound			Northb	ound			Southl	oound			Rolling	Ped	estriar	n Crossi	ngs
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
7:00 AM	0	35	0	53	0	0	0	0	0	0	103	24	0	0	131	22	368	2,026	0	0	0	0
7:15 AM	0	38	0	69	0	0	0	0	0	0	178	31	0	0	176	20	512	2,200	0	0	0	0
7:30 AM	0	37	0	73	0	0	0	0	0	0	238	47	0	0	146	26	567	2,177	0	0	0	0
7:45 AM	0	56	1	109	0	0	0	0	0	0	191	30	0	0	168	24	579	1,995	0	0	0	0
8:00 AM	0	48	0	85	0	0	0	0	0	0	200	29	0	0	165	15	542	1,789	0	0	0	0
8:15 AM	0	30	0	68	0	0	0	0	0	0	165	22	0	0	183	21	489		0	0	0	0
8:30 AM	0	34	0	73	0	0	0	0	0	0	152	13	1	0	104	8	385		0	0	0	0
8:45 AM	0	34	0	88	0	0	0	0	0	0	116	20	0	0	104	11	373		0	0	0	0

		East	bound			West	ound			Northb	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	1	0	5	0	0	0	0	0	0	5	1	0	0	6	5	23
Lights	0	178	1	331	0	0	0	0	0	0	800	136	0	0	648	80	2,174
Mediums	0	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0	3
Total	0	179	1	336	0	0	0	0	0	0	807	137	0	0	655	85	2,200

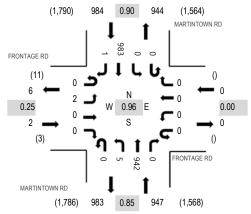


Location: 3 MARTINTOWN RD & FRONTAGE RD AM

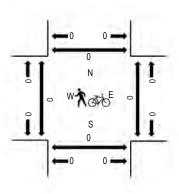
Date: Tuesday, March 22, 2022 **Peak Hour:** 07:15 AM - 08:15 AM

Peak 15-Minutes: 07:45 AM - 08:00 AM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

		FI	RONTA	AGE RI)	FR	ONTA	GE RE)	MA	RTINT	OWN R	D	MA	RTINT	OWN F	RD						
	Interval		Eastb	ound			Westb	ound			Northb	ound			South	ound			Rolling	Ped	estriar	n Crossii	ngs
_	Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
	7:00 AM	0	0	0	0	0	0	0	0	0	0	126	0	0	0	184	0	310	1,767	0	0	0	0
	7:15 AM	0	0	0	0	0	0	0	0	0	2	219	0	0	0	235	0	456	1,933	0	0	0	0
	7:30 AM	0	2	0	0	0	0	0	0	0	0	277	0	0	0	221	0	500	1,915	0	0	0	0
	7:45 AM	0	0	0	0	0	0	0	0	0	2	220	0	0	0	278	1	501	1,760	0	0	0	0
	8:00 AM	0	0	0	0	0	0	0	0	0	1	226	0	0	0	249	0	476	1,594	0	0	0	0
	8:15 AM	0	0	0	0	0	0	0	0	0	0	186	0	0	0	252	0	438		0	0	0	0
	8:30 AM	0	0	0	1	0	0	0	0	0	1	165	0	0	0	175	3	345		0	0	0	0
	8:45 AM	0	0	0	0	0	0	0	0	0	0	143	0	0	0	191	1	335		0	0	0	0

		East	bound			West	oound			North	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	5	0	0	0	11	0	16
Lights	0	2	0	0	0	0	0	0	0	5	934	0	0	0	971	1	1,913
Mediums	0	0	0	0	0	0	0	0	0	0	3	0	0	0	1	0	4
Total	0	2	0	0	0	0	0	0	0	5	942	0	0	0	983	1	1,933

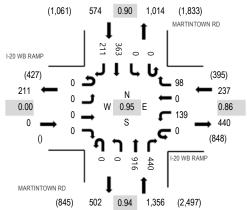


Location: 1 MARTINTOWN RD & I-20 WB RAMP PM

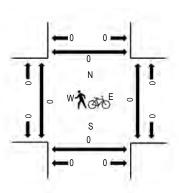
Date: Tuesday, March 22, 2022 **Peak Hour:** 04:45 PM - 05:45 PM

Peak 15-Minutes: 05:00 PM - 05:15 PM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	I-		RAMF)		20 WB			MA	RTINTO		D	MA		OWN F	RD						
Interval		Eastb	ound			Westb	ound			Northb	ound			South	ound			Rolling	Ped	lestriar	n Crossii	ngs
Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru f	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
4:00 PM	0	0	0	0	0	21	0	22	0	0	177	103	0	0	81	52	456	1,823	0	0	0	0
4:15 PM	0	0	0	0	0	14	0	30	0	0	180	102	0	0	65	51	442	1,939	0	0	0	0
4:30 PM	0	0	0	0	0	17	0	17	0	0	173	97	0	0	61	60	425	2,024	0	0	0	0
4:45 PM	0	0	0	0	0	30	0	22	0	0	225	87	0	0	79	57	500	2,167	0	0	0	0
5:00 PM	0	0	0	0	0	35	0	18	0	0	225	135	0	0	103	56	572	2,130	0	0	0	0
5:15 PM	0	0	0	0	0	36	0	33	0	0	230	100	0	0	87	41	527		0	0	0	0
5:30 PM	0	0	0	0	0	38	0	25	0	0	236	118	0	0	94	57	568		0	0	0	0
5:45 PM	0	0	0	0	0	20	0	17	0	0	203	106	0	0	64	53	463		0	0	0	0

		East	bound			Westk	ound			Northb	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	2	0	1	0	0	2	5	0	0	2	0	12
Lights	0	0	0	0	0	135	0	97	0	0	911	434	0	0	361	210	2,148
Mediums	0	0	0	0	0	2	0	0	0	0	3	1	0	0	0	1	7
Total	0	0	0	0	0	139	0	98	0	0	916	440	0	0	363	211	2,167

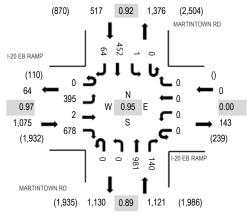


Location: 2 MARTINTOWN RD & I-20 EB RAMP PM

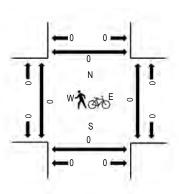
Date: Tuesday, March 22, 2022 **Peak Hour:** 04:45 PM - 05:45 PM

Peak 15-Minutes: 05:30 PM - 05:45 PM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

		Į-		RAMP			20 EB F			MA	RTINTO		D	MA		OWN F	RD			-			
	Interval		Eastb				Westb				Northb				South	oound			Rolling			Crossi	
_	Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru F	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
	4:00 PM	0	79	1	100	0	0	0	0	0	0	190	19	0	0	91	16	496	2,129	0	0	0	0
	4:15 PM	0	100	0	136	0	0	0	0	0	0	181	27	0	0	68	10	522	2,335	0	0	0	0
	4:30 PM	0	74	0	128	0	0	0	0	0	0	200	22	0	0	69	10	503	2,499	0	0	0	0
	4:45 PM	0	108	0	160	0	0	0	0	0	0	200	28	0	1	98	13	608	2,713	0	0	0	0
	5:00 PM	0	90	1	178	0	0	0	0	0	0	265	34	0	0	115	19	702	2,659	0	0	0	0
	5:15 PM	0	106	1	171	0	0	0	0	0	0	236	42	0	0	118	12	686		0	0	0	0
	5:30 PM	0	91	0	169	0	0	0	0	0	0	280	36	0	0	121	20	717		0	0	0	0
	5:45 PM	0	105	0	134	0	0	0	0	0	0	199	27	0	0	79	10	554		0	0	0	0

		East	bound			West	oound			North	ound			South	bound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	3	0	2	0	0	0	0	0	0	5	0	0	0	2	2	14
Lights	0	389	2	676	0	0	0	0	0	0	974	140	0	1	450	61	2,693
Mediums	0	3	0	0	0	0	0	0	0	0	2	0	0	0	0	1	6
Total	0	395	2	678	0	0	0	0	0	0	981	140	0	1	452	64	2,713

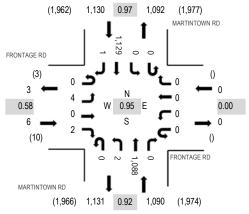


Location: 3 MARTINTOWN RD & FRONTAGE RD PM

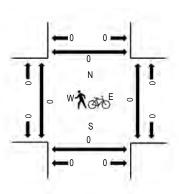
Date: Tuesday, March 22, 2022 **Peak Hour:** 04:45 PM - 05:45 PM

Peak 15-Minutes: 05:00 PM - 05:15 PM

Peak Hour - Motorized Vehicles



Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

Traffic Counts - Motorized Vehicles

	Interval	FI	RONTA Eastb	AGE RI ound)		ONTA Westb	GE RD ound		MA	RTINT(Northb		D	MA	RTINT Southl	OWN Foound	RD		Rolling	Ped	lestriar	ı Crossii	ngs
	Start Time	U-Turn	Left	Thru	Right	U-Turn	Left	Thru F	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total	Hour	West	East	South	North
_	4:00 PM	0	0	0	0	0	0	0	0	0	0	222	0	0	0	199	0	421	1,759	0	0	0	0
	4:15 PM	0	1	0	0	0	0	0	0	0	0	215	0	0	0	210	0	426	1,926	0	0	0	0
	4:30 PM	0	0	0	1	0	0	0	0	0	0	218	0	0	0	206	0	425	2,072	0	0	0	0
	4:45 PM	0	2	0	1	0	0	0	0	0	0	221	0	0	0	263	0	487	2,226	0	0	0	0
	5:00 PM	0	1	0	0	0	0	0	0	0	0	298	0	0	0	289	0	588	2,187	0	0	0	0
	5:15 PM	0	1	0	1	0	0	0	0	0	0	284	0	0	0	285	1	572		0	0	0	0
	5:30 PM	0	0	0	0	0	0	0	0	0	2	285	0	0	0	292	0	579		0	0	0	0
	5:45 PM	0	0	0	2	0	0	0	0	0	0	229	0	0	0	217	0	448		0	0	0	0

		East	bound			West	oound			North	bound			Sout	hbound		
Vehicle Type	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	Total
Articulated Trucks	0	0	0	0	0	0	0	0	0	0	5	0	0	0	4	0	9
Lights	0	4	0	2	0	0	0	0	0	2	1,080	0	0	0	1,120	1	2,209
Mediums	0	0	0	0	0	0	0	0	0	0	3	0	0	0	5	0	8
Total	0	4	0	2	0	0	0	0	0	2	1,088	0	0	0	1,129	1	2,226

DEPARTMENT OF PLANNING AND DEVELOPMENT

TOMMY PARADISE DIRECTOR

MONTHLY REPORT FOR August 2022

City of North Augusta

Department of Planning and Development Monthly Report for August 2022

Item	This M	onth	Year To	Date	Same Mor Yea		Last Year	To Date
Administrative	Incoming	Outgoing	Incoming	Outgoing	Incoming	Outgoing	Incoming	Outgoing
Total Phone Calls					462	303	3,982	2,516
Development Applications	Received	Approved	Received	Approved	Received	Approved	Received	Approved
Subdivisions								
Major Subdivision Plans (PP)	1	0	6	1	0	0	9	3
Planned Acres	25.85	0.00	111.96	8.00	0.00	0.00	256.60	32.48
Planned Lots	56	0	184	79	0	0	0	104
Minor Subdivision Plats	1	1	13	9	2	2	17	16
Platted New Lots	2	2	46	45	5	5	22	22
Major Subdivision Plats	1	1	5	4	0	1	2	2
Platted Acres	39.78	39.78	236.64	230.89	0.00	18.92	1.00	21.97
Platted Lots	4	4	244	244	0	50	82	82
					<u> </u>			
Site Plans								
Minor Site Plans (MSP)	2	0	9	7	3	2	12	5
Major Site Plans (SP)	0	0	3	1	0	0	3	2
SITE PIAN IVIODITICATION	0	0	0	0	0	1	2	2
Total Site Plan Acres	1.88	0.00	58.76	19.92	0.00	1.09	191.51	77.29
Planned Developments								
PD Gen Dev Plans/Major Mod. (PD)	0	0	1	0	0	0	0	0
PD Acres	0	0	68.73	0	0	0	0	0
Development Plan Modification (PDM)	0	0	2	0	0	0	2	0
, ,								
Annexations								
Annexation Agreements Received	0	0	0	0	0	0	0	0
Annexation Cases (ANX)	0	0	2	1	0	0	3	0
Approved by City Council	0	0	1	1	0	0	0	1
Parcels	0	0	1	0	0	0	0	1
Acres	0	0	45	43.90	0	0	0	0.23

City of North Augusta ment of Planning and Developme

Department of Planning and Development <u>Monthly Report for August 2022</u>

ltem	This M	onth	Year To	Date	Same Mo Yea		Last Year	To Date
	Received	Approved	Received	Approved	Received	Approved	Received	Approved
Zoning/Text Amendments								
Rezoning (RZM)	0	0	2	1	3	0	5	2
Parcels	0	0	1	1	5	0	3	1
Acres	0	0.00	15.64	4.39	56.54	0.00	124.26	51.20
Conditional Zoning (RZC)	0	0	0	0	0	0	0	0
Parcels	0	0	0	0	0	0	0	0
Acres	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Text Amendments (RZT)	0	0	1	1	0	0	0	0
Other								
Certificates of Zoning Compliance (CZC)	13	13	101	99	17	17	86	87
Zoning Confirmation Letters (LZC)	1	1	9	9	7	7	20	17
Residential Site Reviews	15	15	259	259	34	34	238	240
Sign Permits (SN)	9	9	38	38	3	3	29	29
Right of way waming	0	1	2	2	0	0	0	0
Right of Way Abandonment	0	0	0	0	0	0	0	0
Planning Projects (PROJ)	0	0	0	0	0	0	3	2
Communications Towers (CT)	0	0	0	0	0	0	0	0
Conditional Use Permits (CU)	0	0	5	5	0	0	7	6
Item	This M	onth	Year To	Date	Same Mo Yea		Last Year	To Date
Appeals	Received	Approved	Received	Approved	Received	Approved	Received	Approved
Variances	0	1	13	10	2	2	8	3
Special Exceptions	0	0	0	0	0	0	0	0
Administrative Decisions	0	0	0	0	0	0	0	0
Waivers	0	0	1	1	1	0	1	2

City of North Augusta Department of Planning and Development Monthly Report for August 2022

Item	This Month	Year To Date	Same Month Last Year	Last Year To Date
Fees Collected				
Development Applications	\$2,298.46	\$31,546.91	\$2,540.00	\$28,181.51
Appeals	\$0.00	\$3,257.77	\$500.00	\$2,257.77
Maps/Publications	\$0.00	\$0.00	\$0.00	\$0.00
Special Review Fees	\$0.00	\$0.00	\$0.00	\$0.00
Total Fees	\$2,298.46	\$34,804.68	\$3,040.00	\$30,439.28

^{*} Not yet recorded

Item	This Mo	onth	Year To	Date	Same Mont Year	•	Last Year	Γο Date
Code Enforcement	Case Received or Investigated	Case Closed						
Property Maintenance	11	12	130	112	26	21	125	133
Property Leins/Contractor Mitigation	0	0	0	0	0	0	2	2
Swimming Pools	5	5	11	6	1	0	3	1
Recreational Vehicles/RV/Boat/Utility Trailers	6	5	26	23	4	6	33	26
Illegal Vehicles	8	8	32	35	12	4	74	43
Commercial Vehicles/Equipment	0	0	1	2	1	1	1	1
Temporary Signs	84	84	641	641	37	37	451	451
Landscape Inspections	13	13	145	145	21	21	118	118
Structure Demolitions	0	0	0	0	0	0	2	2
Citation/Summons Issued	0	0	1	0	1	0	1	0

City of North Augusta Department of Planning and Development

North Augusta Planning Department

August 2022 Staff Approvals

Residential Site Plans

Application Number	Tax Parcel Number	Applicant	Legal Description	Zone	Approval Date	Structure
B22-0563	010 11 09 016	Winchester Commercial Group	4279 Candleberry Garden	PD	8/3/2022	New Residential Construction
B22-0564	010 11 09 017	Winchester Commercial Group	4285 Candleberrry Garden	PD	8/3/2022	New Residential Construction
B22-0565	010 11 09 018	Winchester Commercial Group	4289 Candleberry Garden	PD	8/3/2022	New Residential Construction
B22-0566	012 17 03 040	Park Ridge Builders	1570 Womrath Rd	R-7	8/3/2022	New Residential Construction
B22-0568	007 12 13 001	Robert Methvin	907 Laurens St	R-10	8/3/2022	Storage Building 16X12
B22-0579	006 16 12 024	ParkRidge Builders	324 Whitlaws Rd	R-7	8/8/2022	New Residential Construction
B22-0580	006 16 12 026	ParkRidge Builders	322 Whitlaws Rd	R-7	8/8/2022	New Residential Construction
B22-0581	006 09 06 013	JS and More LLC	1810 Robinson Dr	R-14	8/11/2022	Adding lean to
B22-0589	003 08 06 005	Vintson Construction Co	615 Stanton Dr	R-14	8/10/2022	add master bedroom/bath/laundry room
B22-0624	007 11 03 005	Prescott & Sons Construction	909 East Ave	R-7	8/24/2022	Adding Master bedroom/bath/laundry
B22-0630	007 11 05 077	Green & Green Construction	811 East Ave	R-7	8/26/2022	New Residential Construction
B22-0631	006 13 04 012	Christian Mercado	1975 Bolin Rd	R-14	8/29/2022	Build Attached lean to over Patio
B22-0642	001 12 16 001	Bill Beazley Homes	214 Bonhill St	PD	8/30/2022	New Residential Construction
SP22-0019	002 11 02 102	BEC Custom Pools	203 Seton Circle	R-14	8/8/2022	Swimming Pool
SP22-0020	014 00 02 033	Peach Tree Pools & Spa	328 Rivernorth Dr	PD	8/24/2022	Swimming Pool

City of North Augusta Department of Planning and Development

Sign	Perm	nite

5.8. · 5. · · · · · · · · · · · · · · · · ·						
Application Number	Tax Parcel Number	Applicant	Legal Description	Zone	Approval Date	Use
SN22-030	007 14 04 012	Julie McNeely	McNeely Place	D	8/2/2022	
SN22-031	007 06 24 006	Fast Signs	Woodward & Associates	OC	8/11/2022	
SN22-032	007 14 03 002	Keen Signs and Graphics	Orange Otter Toys	D	8/18/2022	
SN22-033	006 12 05 001	Keen Signs and Graphics	Community Choice Finance	GC	8/19/2022	
SN22-034	006 18 07 043	Summer Trullo/Apollo Signs	Athletico Physical Therapy	GC	8/25/2022	
SN22-035	012 17 03 035	Glynn Bruker	Spring Grove Village-Sign	R-7	8/24/2022	
SN22-036	007 11 05 048	AAA Sign Co	T Mobile	GC	8/22/2022	
SN22-037	007 11 05 047	Finuf Sign Company INC	Beall's Outlet	GC	8/23/2022	
SN22-038	010 14 13 001	AAA Sign Co	Piedmont Prompt Care	GC	8/29/2022	

Certificate of Zoning Compliance Approvals

Application Number	Tax Parcel Number	Applicant	Legal Description	Zone	Approval Date	Use
CZC22-088	013 19 02 001	Terry Lambert	gusta, Inc. Dba terry Lambert H	TC	8/1/2022	
CZC22-089	006 15 03 002	William Manning	North Augusta Consulting	R-7	8/1/2022	
CZC22-090	013 17 14 001	Theyartis Edwards	Hannibal International Imports	TC	8/2/2022	
CZC22-091	006 16 14 003	Dorothy Spaulding	Watchman Broadcasting	GC	8/4/2022	
CZC22-092	007 14 03 002	Denice Golden	ane's Income Tax & Bookeeping	D	8/10/2022	
CZC22-093	007 10 27 007	Africa Thomas	Booze Pops CSRA Food Truck	D	8/10/2022	
CZC22-094	106 00 07 018	James Neal	Frontline Irrigation Service	R-10	8/11/2022	
CZC22-095	005 08 07 013	David Hall	Southern Sudds	R-7	8/15/2022	
CZC22-096	006 16 14 001	Jessica Veerapen	aylor's Barber & Beauty Acaden	GC	8/18/2022	
CZC22-097	007 09 17 028	Jesus Mercado	Mercado Landscaping LLC	R-5	8/18/2022	
CZC22-098	007 16 02 008	Ho Yong Lee	BJ Country Buffet	TC	8/22/2022	
CZC22-099	001 16 07 040	Pedro Ryan Ufret	CSRA Pressure Pros	PD	8/25/2022	
CZC22-100	007 07 06 007	Jo Barton	America's Rubbish Removal	R-14	8/29/2022	

City of North Augusta Department of Planning and Development